

ANNEXE C

Étude des effets hydrologiques de l'urbanisation du
bassin ruisseau des Fées à Hull (février 1989)

Étude du bassin du ruisseau des Fées (octobre 1993).

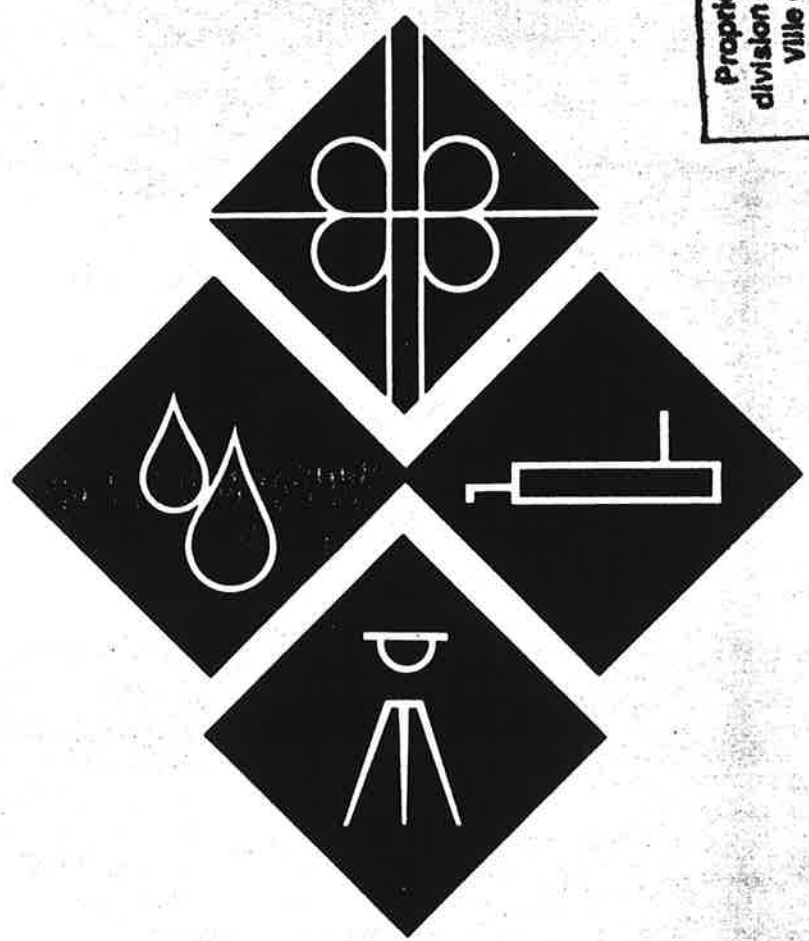
Pink

6 001739-000-030-R-011

classer C-05-54
(Poquette)

Propriété du
Service d'ingénierie
Ville de Gatineau

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Ville de Hull



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Ville de Hull

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Ville de Gatineau

VILLE DE HULL

LES DÉVELOPPEMENTS IMMOBILIERS GAMELIN LTÉE

ÉTUDE DU BASSIN DU RUISSEAU DES FÉES

NOTRE DOSSIER: 368-013

Ville de Hull
Service du génie
Reçu le
8 OCT 1993

AH/dp
Révisé le 04 octobre 1993

INTRODUCTION:

Notre firme a été mandatée par la compagnie Les Développements Immobiliers Gamelin Ltée afin de poursuivre notre étude préliminaire du bassin du ruisseau des Fées. Cette étude préliminaire préparée en 1989, rappelons-le, avait pour but de déterminer l'influence du développement urbain prévu dans ce bassin sur le débit des eaux de ruissellement et d'esquiver différents scénarios d'interventions possibles.

La présente étude a donc pour but de raffiner les interventions suggérées et de préciser dans quelles mesures le débit des eaux de ruissellement sera affecté. Ceci sera fait en tenant compte des données recueillies initialement ainsi que de nouveaux facteurs tels que des modifications apportées aux limites des sous-bassins considérés, ainsi que les développements domiciliaires en cours et projetés.

SOMMAIRE:

Le présent rapport d'étude comporte quatre (4) étapes principales. La première étape consiste en une description et une caractérisation des sous-bassins actuels de la portion du bassin du ruisseau des Fées en amont du chemin de la Montagne.

La seconde étape comporte une description du modèle informatique utilisé ainsi que les résultats de la modélisation des eaux de ruissellement générées par le bassin du ruisseau dans les conditions actuelles.

Les résultats issus de la modélisation en fonction de l'urbanisation prévue du bassin constitue la troisième étape de la présente étude.

La quatrième étape du rapport comporte une analyse des résultats de modélisation en fonction du bassin urbanisé à l'intérieur duquel on aurait aménagé des volumes de rétention additionnels, ainsi que quelques commentaires sur la localisation et répartition de ces ouvrages de rétention des eaux de ruissellement.

LISTE DES PLANS ET CROQUIS:

Plan numéro 368-013-100 Bassin du Ruisseau des Fées-
Conditions avant urbanisation

Plan numéro 368-013-101 Bassin du Ruisseau
Conditions urbanisées

Croquis #368-013-1: Schéma du modèle - conditions avant urbanisation

Croquis #368-013-2: Schéma du modèle - conditions urbanisées non contrôlées

Croquis #368-013-3: Schéma du modèle - conditions urbanisées contrôlées

Croquis #4: Débit de pointe pour les différentes orages -
conditions urbanisées contrôlées

1. DESCRIPTION DES SOUS-BASSINS

SOUS-BASSIN 1 (63.0 ha)

Le sous-bassin 1 est limité au sud par le chemin de la Montagne, à l'ouest et au nord par la limite de partage des eaux formées par des collines de la Gatineau et à l'est également par la ligne de partage des eaux qui correspond approximativement à un prolongement théorique de l'axe du chemin Vanier. Ce sous-bassin est fortement boisé et le sol en surface se compose d'une bonne épaisseur de matière organique et de débris forestiers.

SOUS-BASSIN 1 AB (141.0 ha)

Le sous-bassin 1 AB est situé immédiatement à l'est du sous-bassin 1 et est limité au nord par la ligne de partage des eaux, à l'est par une ligne imaginaire passant à l'est de la rue Skyridge et au sud par le chemin Cook. Mise à part les quelques résidences en bordure des chemins Skyridge et Notch, la partie du présent sous-bassin située au nord du chemin de la Montagne, présente les mêmes caractéristiques topographiques et pédologiques que le sous-bassin 1. La partie méridionale du sous-bassin 1 AB, qui est sise dans le triangle formé par les chemins Cook, de la Montagne et Vanier, est caractérisée par une topographie relativement plate et une répartition à peu près égale au niveau de l'occupation du sol entre les zones boisées et marécageuses. Ces zones basses de pair avec une sablière abandonnée constituent un immense volume de rétention naturelle. La majorité de ces terrains sont présentement zonés agricole. Nous avons pris comme hypothèse de calcul qu'ils le demeureraient. Advenant un changement de zonage et une urbanisation subséquente de ces terrains, il serait nécessaire alors d'aménager un réservoir permettant de compenser à la fois pour le volume naturel de rétention ainsi perdu et pour le volume d'eau généré par l'urbanisation de ce territoire.

SOUS-BASSIN 2 (248.0 ha)

Le sous-bassin 2 est situé au sud du sous-bassin 1 et est limité du côté ouest et sud par la ligne naturelle de partage des eaux. La limite est du sous-bassin, quant à elle, est formée par la ligne de partage des eaux joignant le chemin Cook au chemin Vanier et passant par l'exutoire du présent sous-bassin (noté par la lettre "A" sur le plan numéro 368-013-100).

Zoné agricole, le sous-bassin 2 est partiellement boisé et on y retrouve un bon nombre de zones marécageuses, dont un pourcentage appréciable est concentré le long des berges du ruisseau des Fées.

SOUS-BASSIN 3 (205.0 ha)

Compris à l'intérieur des limites du parc de la Gatineau, le sous-bassin numéro 3 est adjacent au sous-bassin 1 AB et est limité au nord par la ligne de partage des eaux, au sud par le chemin de la Montagne et à l'est, tel qu'indiqué au plan.

Ce sous-bassin présente les mêmes caractéristiques topographiques et pédologiques que le sous-bassin 1 et la portion septentrionale du sous-bassin 1 AB. De plus, la forêt mature et son sol riche en terre organique et débris végétaux sont protégés par la Commission de la Capitale Nationale.

SOUS-BASSIN 4 (357.0 ha)

Le sous-bassin numéro 4 est limité à l'ouest par le sous-bassin numéro 2, au nord par le sous-bassin numéro 3, à l'est par le sous-bassin numéro 5 (tel qu'indiqué au plan) et au sud par le chemin Pink.

Ce sous-bassin se caractérise par une topographie peu accidentée et un sol qui est en majeure partie fermé d'une couche de surface, d'une épaisseur appréciable de matériau sablonneux. Les quantités de ce matériau sont à ce point appréciables qu'elles justifieraient facilement l'exploitation d'une carrière. Le couvert végétal de ce sous-bassin se divise à part égale entre des champs autrefois cultivés et des forêts à différents stades de croissance.

SOUS-BASSIN 5 (31.0 ha)

Ce sous-bassin dont les principales caractéristiques sont similaires à celles du sous-bassin numéro 4, est limité à l'ouest par ce dernier, au nord-est par le chemin de la Montagne et au sud par le chemin Pink.

SOUS-BASSIN 6A (142.0 ha)

Situé au sud du chemin Pink, le sous-bassin numéro 6A est limité du côté sud-ouest par la ligne de partage des eaux et du côté est par la limite de la zone habitée le long de la rue des Pommiers (telle qu'indiquée au plan).

Le terrain est en général relativement plat, peu boisé et constitué en grande partie de champs abandonnés et de marécages. Le type de sol varie de sableux-silteux par endroits à argileux en d'autres endroits.

SOUS-BASSIN 6B (51.0 ha)

Le sous-bassin numéro 6B se trouve à l'est du sous-bassin numéro 6A et est limité par l'ancien tracé du chemin de la Montagne et la ligne de partage des eaux au sud.

Le territoire compris à l'intérieur de ce sous-bassin est partiellement urbanisé par un développement de très faible densité regroupé dans le secteur des chemins de la

Montagne et des rues des Pommiers et des Peupliers.

Le sol y est de nature silteuse et la topographie existante permet d'assurer un bon drainage de surface.

2. **MODÉLISATION EN FONCTION DES CONDITIONS AVANT URBANISATION PLANIFIÉE:**

Notre analyse hydrologique du bassin du ruisseau des Fées a été réalisée à l'aide du logiciel OTTHYMO (version interhymo 1989 b) distribué par le centre INTERHYMO d'Ottawa. Le croquis 368-013-1 démontre le schéma de modélisation utilisé pour simuler le réseau de drainage du bassin du ruisseau des Fées. Les caractéristiques hydrologiques du bassin actuel ont été consignées au tableau suivant:

TABLEAU NUMÉRO 1
LES CARACTÉRISTIQUES DES SOUS-BASSINS ACTUELS

Sous-bassin	Superficie (ha)	Occupation	CN*	. Tp (hres)	Surface imperméable
1 AB	141.0	rural	63	1.4	----
1	63.0	rural	68	1.57	----
2	248.0	rural	55	2.0	----
3	205.0	rural	68	1.58	----
4	357.0	rural	55	0.79	----
5	31.0	rural	55	0.39	----
6 A	142.0	rural	55	0.88	----
6 B	51.0	urbain	--	----	15%

Les résultats obtenus au moyen de notre simulation informatique pour le bassin actuel aux points de contrôles A, C et D' pour des événements correspondant à une pluie de fréquence de une fois dans 2 ans, 5 ans et 100 ans sont présentés au tableau 1.1 et les résultats détaillés ont été consignés en annexe.

TABLEAU NUMÉRO 1.1

DÉBIT DE POINTE

Point	Pluie 2 ans	Pluie 5 ans	Pluie 100 ans
A	0.9m ³ /s	2.1m ³ /s	4.4m ³ /s
C	2.7m ³ /s	6.5m ³ /s	14.4m ³ /s
D'	3.0m ³ /s	7.6m ³ /s	15.3m ³ /s

3. MODÉLISATION EN FONCTION DES CONDITIONS HYDROLOGIQUES DU BASSIN URBANISÉ:

L'urbanisation du bassin ainsi que la construction de grands axes routiers auront un impact important, non seulement sur les débits des eaux de ruissellement générés, mais aussi sur les limites futures des sous-bassins.

Conscients de ces phénomènes, nous avons modifié les limites des sous-bassins de notre modèle urbanisé (voir plan 368-013-101-01) afin de tenir compte des facteurs mentionnés précédemment à la lumière des informations présentement disponibles. Certaines de ces informations, comme les parcours de l'autoroute 50 et de l'autoroute Deschênes, ainsi que l'implantation du parc industriel de la rue Vernon, peuvent être considérées comme définitives.

Le parcours des rues et des axes routiers secondaires ainsi que le cheminement du drainage qui y sont associés pourraient toutefois facilement subir des modifications substantielles sans que les impacts sur les débits aux points importants soient modifiés visiblement.

La numérotation des sous-bassins urbanisés correspond approximativement à la numérotation des sous-bassin actuels et les principales caractéristiques hydrologiques de ces sous-bassins sont consignées au tableau suivant:

TABLEAU NUMÉRO 2
LES CARACTÉRISTIQUES DES SOUS-BASSINS FUTURES APRÈS URBANISATION

Sous-bassin	Superficie (ha)	Occupation	CN*	Tp (hres)	Surface imperméable
1 AB	268	rural	65	2.0	----
2	247	rural	55	1.07	----
3	204	rural	68	1.58	----
5	136	urbain	--	----	45
6	167	urbain	--	----	35
4	220	urbain	--	----	75

Le croquis numéro 368-13-2 démontre la modélisation utilisée lors de notre simulation du réseau de drainage du bassin urbanisé du ruisseau des Fées. Afin de faciliter la comparaison des débits des eaux de ruissellement générées, le bassin dans son état actuel versus par le bassin après urbanisation, nous avons repris les tableaux 1 et 2 et formé le tableau 2.1.

TABLEAU NUMÉRO 2.1

DÉBIT DE POINTE (M³/SEC)

Point	Pluie de 2 ans (non urbanisé)	Pluie de 2 ans (urbanisé)	Pluie de 5 ans (non urbanisé)	Pluie de 5 ans (urbanisé)	Pluie de 100 ans (non urbanisé)	Pluie de 100 ans (urbanisé)
A	0.9	0.9	2.1	2.1	4.4	5.0
B	---	15.5	---	25.3	---	43.1
C	2.7	---	6.5	---	14.4	---
C'	---	13.9	---	20.3	---	34.1
D	---	14.0	---	19.8	---	32.9
D'	3.0	---	7.6	---	15.3	---

Les débits obtenus nous permettent de constater la nécessité d'aménager à l'intérieur du bassin du ruisseau des Fées des ouvrages de rétention.

4. MODÉLISATION EN FONCTION DES CONDITIONS HYDROLOGIQUES DU BASSIN URBANISÉ AVEC OUVRAGES DE CONTRÔLE:

Le croquis numéro 368-13-3 montre un schéma du modèle utilisé pour simuler le réseau de drainage du bassin urbanisé avec la localisation relative de tous les ouvrages de rétention qu'ils soient du type naturel ou artificiel existant ou projeté.

Nous avons modifié notre modèle de façon à prendre en considération les facteurs énumérés précédemment et les caractéristiques hydrologiques de ces sous-bassins ont été consignées au tableau 2.2.

TABLEAU NUMÉRO 2.2

Sous-bassin	Superficie (ha)	Occupation	CN*	 Tp (hres)	Surface imperméable
1 AB	268	rural	65	2.0	-----
2	247	rural	55	1.07	-----
3	204	rural	68	1.58	-----
5	136	urbain	--	----	45
6	167	urbain	--	----	35
4 A	90	urbain	--	----	75
4 B	130	urbain	--	----	75

Les résultats obtenus confirment la nécessité d'aménager un volume additionnel de rétention de 5.4 ha.m en amont du point C'. Le point C' correspond à l'intersection projetée du boulevard des Grives et du ruisseau des Fées. Nous sommes d'avis qu'il est relativement facile d'aménager 3.5 ha.m entre le chemin Pink et le boulevard des Grives. Le volume additionnel 2.0 ha.m devra être implanté à l'intérieur des limites du sous-bassin numéro 5 au nord du chemin Pink.

Le volume de 1.5 ha.m indiqué au point "D", point qui correspond à l'intersection du chemin de la Montagne et du ruisseau des Fées, sera aménagé lors de l'excavation du canal en amont du point "D".

Le débit obtenu par nos simulations confirme le contenu des conclusions. Le croquis numéro 368-13-4, quant à lui, montre les volumes maximaux utilisables, ainsi que les débits de pointe aux endroits importants, soit les points A, B, C' et D.

Enfin, le tableau numéro 3 résume les débits calculés aux points importants. Pour les trois (3) cas que nous avons étudiés, soit le bassin actuel, le bassin après urbanisation et le bassin après urbanisation avec structure de contrôle et ce, en fonction d'évènements simulants une pluie de fréquence de une fois dans 2 ans, 5 ans et 100 ans.

TABLEAU NUMÉRO 3
DÉBIT DE POINTE (M³/SEC)

PLUIE 2 ANS

Endroit	Non urbanisé	Urbanisé non contrôlé	Urbanisé contrôlé
A	0.9	0.9	0.9
B		15.5	2.4
C	2.7		
C'		13.9	3.3
D		14.0	4.9
D'	3.0		



TABLEAU NUMÉRO 3
DÉBIT DE POINTE (M³/SEC)
PLUIE 5 ANS

Endroit	Non urbanisé	Urbanisé non contrôlé	Urbanisé contrôlé
A	2.1	2.2	2.7
B		25.3	4.0
C	6.5		
C'		20.3	6.1
D		19.8	8.3
D'	7.6		

TABLEAU NUMÉRO 3
DÉBIT DE POINTE (M³/SEC)
PLUIE 100 ANS

Endroit	Pluie 100 ans	Non urbanisé	Urbanisé non contrôlé	Urbanisé contrôlé
A		4.4	5.0	5.7
B			43.1	6.6
C		14.4		
C'			34.1	10.5
D			32.9	15.3
D'		15.8		

De notre rapport préliminaire à l'effet qu'il faudrait augmenter la capacité, des ponceaux sous l'ancien et le nouveau tracé du chemin de la Montagne, de façon à pouvoir accepter un débit de plus de $15.3\text{m}^3/\text{s}$, sans toutefois augmenter le niveau du gradient hydraulique du réseau d'égout pluvial.

Alexandre Hotovec, ing. M. SCQUEBEC

AH/dp

le 1^{er} juin 1992

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=====
      OOO      TTTTT  TTTTT  H   H   Y   Y   M   M   OOO      I N T E R H Y M O
      O   O    T     T    H   H   Y   Y   M M M M  O   O    * * * 1989b * * *
      O   O    T     T    H H H H   Y   M M M   O   O
      O   O    T     T    H   H   Y   M   M   O   O
      OOO      T     T    H   H   Y   M   M   OOO      bK-915981900004
=====

```

istributed by the INTERHYMO Centre. Copyright (c), 1989. Paul Wisner & Assoc.

Input filename: B:OTFC.FEE
Output filename: B:OUFC.FEE
Summary filename: B:SUF.C.FEE

ATE: 01-16-1991 TIME: 17:23:13

```

<=== comment ===>-----
<=== comment ===>-----
<=== comment ===>-----

```

```

*****
** SIMULATION NUMBER: 1 **
*****

```

```

#=====
# DOSSIER OTFC.FEE |
#=====
# PROJET RUISSEAU DES FEES GPD
#=====
# CONDITIONE FUTURE SIMULATION FINALE (CN* = VARIABLE)
#=====
# -CONTROLEE-
#=====
# ORAGE DE 100-ANS
#=====

```

```

-----
READ STORM      Filename: b:100.ANS
Ptotal= 72.30 mm Comments: 100 YEAR STORM (DE FEES)
-----

```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	4.92	.83	78.42	1.58	12.65	2.33	5.89
.17	4.92	.92	107.19	1.67	12.65	2.42	5.20
.25	6.35	1.00	107.19	1.75	9.85	2.50	5.20
.33	6.35	1.08	99.64	1.83	9.85	2.58	4.65
.42	8.95	1.17	99.64	1.92	8.05	2.67	4.65
.50	8.95	1.25	31.10	2.00	8.05	2.75	4.21
.58	18.54	1.33	31.10	2.08	6.81	2.83	4.21
.67	18.54	1.42	17.51	2.17	6.81	2.92	3.85
.75	78.42	1.50	17.51	2.25	5.89	3.00	3.85

```

#=====
# SOUS-BASSIN -1AB- |
#=====

```

```

-----
CALIB
NASHYD (0111) | Area (ha)= 268.00 Curve Number (CN)= 65.0
ID= 1 DT= 5.0 min | Ia (mm)= 2.50 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= 2.00

```

```

Unit Hyd Qpeak (cms)= 5.12
PEAK FLOW (cms)= 4.40 (i)
TIME TO PEAK (hrs)= 3.33
RUNOFF VOLUME (mm)= 23.58
TOTAL RAINFALL (mm)= 72.30
RUNOFF COEFFICIENT = .33

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0201)
 IN= 1---> OUT= 2
 DT= 5.0 min

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.000	.000	.500	50.000
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)
INFLOW : ID= 1 (0111)		268.00	4.40	3.33
OUTFLOW: ID= 2 (0201)		268.00	.06	10.83
				R.V. (mm)
				23.58
				5.84
				PEAK FLOW REDUCTION [Qout/Qin](%)= 1.40
				TIME SHIFT OF PEAK FLOW (min)=450.00
				MAXIMUM STORAGE USED (ha.m.)= 6.15

#=====||
 # SOUS-BASSIN -2- ||
 #=====||

CALIB
 NASHYD (0200)
 ID= 1 DT= 5.0 min

Area (ha)=	247.00	Curve Number (CN)=	55.0
Ia (mm)=	2.50	# of Linear Res.(N)=	3.00
U.H. Tp(hrs)=	1.07		

Unit Hyd Qpeak (cms)= 8.82

PEAK FLOW (cms)= 4.95 (i)
 TIME TO PEAK (hrs)= 2.33
 RUNOFF VOLUME (mm)= 17.55
 TOTAL RAINFALL (mm)= 72.30
 RUNOFF COEFFICIENT = .24

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

#=====||
 # POINT -A- ||
 #=====||

ADD HYD (0321)
 2 + 1 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 2 (0201):	268.00	.06	10.83	5.84
+ ID2= 1 (0200):	247.00	4.95	2.33	17.55
ID = 3 (0321):	515.00	4.96	2.33	11.45

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

#=====||
 # SOUS-BASSIN -4A- Urbain ||
 #=====||

DESIGN
 STANDHYD (0401)
 ID= 1 DT= 5.0 min

Area (ha)=	90.00	Dir. Conn.(%)=	75.00
Total Imp(%)=	75.00		

	IMPERVIOUS (ha)	PERVIOUS (i)
Surface Area	67.50	22.50
Dep. Storage	.80	1.50
Average Slope (%)	1.00	1.00
Length (m)	774.00	40.00
Mannings n	.013	.250
Max.eff.Inten.(mm/hr)=	107.19	29.97
over (min)	10.00	25.00
Storage Coeff. (min)=	8.48 (ii)	22.55 (ii)
Unit Hyd. Tpeak (min)=	10.00	25.00
Unit Hyd. peak (cms)=	.12	.05

PEAK FLOW (cms)= 18.06
 TIME TO PEAK (hrs)= 1.17

TOTALS
 18.65 (iii)
 1.17

RUNOFF VOLUME (mm) = 71.50 17.99 58.12
 TOTAL RAINFALL (mm) = 72.30 72.30 72.30
 RUNOFF COEFFICIENT = .99 .25 .80

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 55.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

COMPUTE VOLUME
 ID= 1 (0401)

	DISCHARGE (cms)	TIME (hrs)
START CONTROLLING AT	.03	.17
INFLOW HYD. PEAKS AT	18.65	1.17
STOP CONTROLLING AT	1.50	2.39

REQUIRED STORAGE VOLUME (ha.m.) = 4.2844
 TOTAL HYDROGRAPH VOLUME (ha.m.) = 5.2307
 % OF HYDROGRAPH TO STORE = 81.9083

NOTE: Storage was computed to reduce the Inflow
 peak to 1.50 (cms).

=====||
 # RESERVOIR NATURELE ||
 #=====||

RESERVOIR (0201)
 IN= 1---> OUT= 4
 DT= 5.0 min

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.000	.000	1.500	10.000

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 1 (0401)	90.00	18.65	1.17	58.12
OUTFLOW: ID= 4 (0201)	90.00	.71	3.08	57.42

PEAK FLOW REDUCTION [Qout/Qin](%) = 3.78
 TIME SHIFT OF PEAK FLOW (min) = 115.00
 MAXIMUM STORAGE USED (ha.m.) = 4.71

ADD HYD (0321)
 3 + 4 = 5

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 3 (0321):	515.00	4.96	2.33	11.45
+ ID2= 4 (0201):	90.00	.71	3.08	57.42
=====	=====	=====	=====	=====
ID = 5 (0321):	605.00	5.65	2.33	18.29

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

=====||
 # DE POINT "A" A POINT "B" ||
 #=====||

ROUTE (0110)
 CHANNEL #SEG= 3
 IN= 5---> OUT= 3

Routing time step (min) = 6.00
 Slopes (%), CHANNEL= .40 FLOODPLAIN= .40
 LENGTH = 1600.00 (m)

<----- DATA FOR SECTION (1.0) ----->

Distance	Elevation	Manning	
.00	104.24	.0500	
100.00	101.79	.0500	
110.00	101.17	.0500	
113.00	101.17	.0500 / .0300	Main Channel
113.80	100.57	.0300	Main Channel
116.50	100.57	.0300	Main Channel
117.00	101.30	.0300 / .0500	Main Channel
120.00	101.52	.0500	
126.00	102.40	.0500	

←----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV. TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.12	100.69	.542E+03	.2	.49	54.71
.24	100.81	.113E+04	.5	.74	36.00
.36	100.93	.176E+04	1.0	.93	28.53
.48	101.05	.245E+04	1.7	1.10	24.35
.60	101.17	.317E+04	2.4	1.23	21.60
.73	101.30	.483E+04	3.7	1.21	22.04
.86	101.43	.710E+04	5.4	1.21	22.10
.99	101.56	.102E+05	7.6	1.20	22.26
1.12	101.69	.139E+05	10.5	1.21	22.04
1.25	101.82	.182E+05	14.0	1.22	21.77
1.38	101.95	.237E+05	17.9	1.21	21.97
1.51	102.08	.303E+05	23.0	1.21	21.95
1.63	102.20	.383E+05	29.3	1.23	21.77
1.76	102.33	.475E+05	37.0	1.24	21.44
1.89	102.46	.586E+05	44.1	1.20	22.16
2.02	102.59	.747E+05	54.4	1.16	22.91
2.15	102.72	.966E+05	68.6	1.14	23.45
2.28	102.85	.124E+06	87.2	1.12	23.74
2.41	102.98	.157E+06	110.5	1.12	23.74

	AREA	<---- hydrograph ---->			<---- channel ---->	
	(ha)	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
		(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 5 (0321)	605.00	5.65	2.33	18.29	.88	1.21
OUTFLOW: ID= 3 (0110)	605.00	5.27	2.75	18.26	.85	1.21

```

=====
# SOUS-BASSIN -4B- Urbain |
=====

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-----
DESIGN
STANDHYD (0402) | Area (ha)= 130.00
ID= 1 DT= 5.0 min | Total Imp(%)= 75.00 Dir. Conn.(%)= 75.00
-----

```

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	97.50	32.50	
Dep. Storage (mm)=	.80	1.50	
Average Slope (%)=	1.00	1.00	
Length (m)=	930.00	40.00	
Mannings n =	.013	.250	
Max. eff. Inten. (mm/hr)=	107.19	29.97	
over (min)	10.00	25.00	
Storage Coeff. (min)=	9.47 (ii)	23.54 (ii)	
Unit Hyd. Tpeak (min)=	10.00	25.00	
Unit Hyd. peak (cms)=	.12	.05	
PEAK FLOW (cms)=	25.64	1.41	*TOTALS*
TIME TO PEAK (hrs)=	1.17	1.50	26.46 (iii)
RUNOFF VOLUME (mm)=	71.50	17.99	1.17
TOTAL RAINFALL (mm)=	72.30	72.30	58.12
RUNOFF COEFFICIENT =	.99	.25	72.30
			.80

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 55.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

=====
# POINT -B- |
=====

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-----
ADD HYD (0231) |
  3 + 1 = 2 |
-----

```

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 3 (0110):	605.00	5.27	2.75	18.26
+ ID2= 1 (0402):	130.00	26.46	1.17	58.12
ID = 2 (0231):	735.00	26.69	1.17	25.31

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

COMPUTE VOLUME
ID= 2 (0231)

	DISCHARGE	TIME
	(cms)	(hrs)
START CONTROLLING AT	2.73	.60
INFLOW HYD. PEAKS AT	26.69	1.17
STOP CONTROLLING AT	13.00	1.49

REQUIRED STORAGE VOLUME (ha.m.) = 2.8944
TOTAL HYDROGRAPH VOLUME (ha.m.) = 18.6039
% OF HYDROGRAPH TO STORE = 15.5583

NOTE: Storage was computed to reduce the Inflow peak to 13.00 (cms).

=====

RESERVOIR #1+ #2 ||

=====

RESERVOIR (0201)
IN= 2---> OUT= 3
DT= 5.0 min

OUTFLOW	STORAGE	OUTFLOW	STORAGE
(cms)	(ha.m.)	(cms)	(ha.m.)
.000	.000	7.000	5.800

	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0231)	735.00	26.69	1.17	25.31
OUTFLOW: ID= 3 (0201)	735.00	6.62	2.92	25.24

PEAK FLOW REDUCTION [Qout/Qin] (%) = 24.80
TIME SHIFT OF PEAK FLOW (min) = 105.00
MAXIMUM STORAGE USED (ha.m.) = 5.48

=====

DE POINT "B" A POINT "C" ||

=====

ROUTE (0110)
CHANNEL #SEG= 3
IN= 3---> OUT= 2

Routing time step (min) = 6.00
Slopes (%), CHANNEL= .40 FLOODPLAIN= .40
LENGTH = 1800.00 (m)

<----- DATA FOR SECTION (1.0) ----->

Distance	Elevation	Manning	
.00	104.24	.0500	
100.00	101.79	.0500	
110.00	101.17	.0500	
113.00	101.17	.0500 / .0300	Main Channel
113.80	100.57	.0300	Main Channel
116.50	100.57	.0300	Main Channel
117.00	101.30	.0300 / .0500	Main Channel
120.00	101.52	.0500	
126.00	102.40	.0500	
226.00	102.98	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.12	100.69	.609E+03	.2	.49	61.55
.24	100.81	.127E+04	.5	.74	40.50
.36	100.93	.199E+04	1.0	.93	32.10
.48	101.05	.275E+04	1.7	1.10	27.39
.60	101.17	.357E+04	2.4	1.23	24.30
.73	101.30	.543E+04	3.7	1.21	24.79
.86	101.43	.799E+04	5.4	1.21	24.86
.99	101.56	.114E+05	7.6	1.20	25.04
1.12	101.69	.156E+05	10.5	1.21	24.79
1.25	101.82	.205E+05	14.0	1.22	24.49
1.38	101.95	.266E+05	17.9	1.21	24.71
1.51	102.08	.341E+05	23.0	1.21	24.70
1.63	102.20	.431E+05	29.3	1.23	24.49
1.76	102.33	.535E+05	37.0	1.24	24.12
1.89	102.46	.659E+05	44.1	1.20	24.93
2.02	102.59	.841E+05	54.4	1.16	25.78
2.15	102.72	.109E+06	68.6	1.14	26.38
2.28	102.85	.140E+06	87.2	1.12	26.71
2.41	102.98	.177E+06	110.5	1.12	26.71

			<---- hydrograph ---->			<---- channel ---->	
	AREA		QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
	(ha)		(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW :	ID= 3 (0201)	735.00	6.62	2.92	25.24	.93	1.20
OUTFLOW:	ID= 2 (0110)	735.00	6.52	3.25	25.21	.92	1.20

```

=====
# DE POINT "C" A POINT "C'"
=====

```

ROUTE (0110)	Routing time step (min) = 6.00
CHANNEL #SEG= 3	
IN= 2--> OUT= 3	Slopes (%), CHANNEL= .35 FLOODPLAIN= .35
	LENGTH = 800.00 (m)

<----- DATA FOR SECTION (1.0) ----->		
Distance	Elevation	Manning
.00	97.89	.0500
100.00	95.77	.0500
102.50	95.57	.0500 / .0300
103.50	94.48	.0300
106.50	94.48	.0300
107.50	95.39	.0300 / .0500
110.00	95.78	.0500
210.00	96.54	.0500

<----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.10	94.58	.251E+03	.1	.41	32.38
.20	94.68	.518E+03	.4	.63	21.11
.30	94.78	.802E+03	.8	.80	16.61
.40	94.88	.110E+04	1.3	.95	14.10
.51	94.99	.142E+04	1.9	1.07	12.46
.61	95.09	.175E+04	2.6	1.18	11.28
.71	95.19	.210E+04	3.4	1.28	10.40
.81	95.29	.247E+04	4.2	1.38	9.69
.91	95.39	.285E+04	5.2	1.46	9.12
1.03	95.51	.334E+04	6.5	1.57	8.50
1.14	95.62	.391E+04	8.1	1.65	8.06
1.25	95.74	.466E+04	9.9	1.70	7.84
1.37	95.85	.595E+04	11.9	1.60	8.31
1.48	95.96	.901E+04	15.0	1.33	10.04
1.60	96.08	.140E+05	19.5	1.12	11.94
1.71	96.19	.208E+05	26.0	1.00	13.33
1.83	96.31	.295E+05	34.9	.95	14.10
1.94	96.42	.402E+05	46.6	.93	14.37
2.06	96.54	.527E+05	61.4	.93	14.31

			<---- hydrograph ---->			<---- channel ---->	
	AREA		QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
	(ha)		(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW :	ID= 2 (0110)	735.00	6.52	3.25	25.21	1.02	1.57
OUTFLOW:	ID= 3 (0110)	735.00	6.51	3.42	25.20	1.02	1.57

```

=====
# SOUS-BASSIN -3-
=====

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CALIB			
NASHYD (0300)	Area (ha) = 204.00	Curve Number (CN) = 68.0	
ID= 1 DT= 5.0 min	Ia (mm) = 2.50	# of Linear Res. (N) = 3.00	
	U.H. Tp (hrs) = 1.58		

Unit Hyd Qpeak	(cms) = 4.93
PEAK FLOW	(cms) = 4.44 (i)
TIME TO PEAK	(hrs) = 2.92
RUNOFF VOLUME	(mm) = 25.73
TOTAL RAINFALL	(mm) = 72.30
RUNOFF COEFFICIENT	= .36

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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#
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SOUS-BASSIN -5- Urbain|
#=====

DESIGN STANDHYD (0500) ID= 2 DT= 5.0 min	Area (ha)= 136.00 Total Imp(%)= 45.00	Dir. Conn.(%)= 45.00
--	--	----------------------

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	61.20	74.80	
Dep. Storage (mm)=	.80	1.50	
Average Slope (%)=	1.00	1.00	
Length (m)=	952.00	40.00	
Mannings n =	.013	.250	
Max.eff.Inten.(mm/hr)=	107.19	29.97	
over (min)	10.00	25.00	
Storage Coeff. (min)=	9.60 (ii)	23.67 (ii)	
Unit Hyd. Tpeak (min)=	10.00	25.00	
Unit Hyd. peak (cms)=	.11	.05	
PEAK FLOW (cms)=	16.05	3.23	*TOTALS*
TIME TO PEAK (hrs)=	1.17	1.50	17.94 (iii)
RUNOFF VOLUME (mm)=	71.50	17.99	1.17
TOTAL RAINFALL (mm)=	72.30	72.30	42.07
RUNOFF COEFFICIENT =	.99	.25	72.30
			.58

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 55.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0412) 1 + 2 = 4	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0300):	204.00	4.44	2.92	25.73
+ ID2= 2 (0500):	136.00	17.94	1.17	42.07
=====	=====	=====	=====	=====
ID = 4 (0412):	340.00	18.33	1.17	32.26

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

#=====

# POINT -C'-		
--------------	--	--

#=====

ADD HYD (0143) 4 + 3 = 1	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 4 (0412):	340.00	18.33	1.17	32.26
+ ID2= 3 (0110):	735.00	6.51	3.42	25.20
=====	=====	=====	=====	=====
ID = 1 (0143):	1075.00	18.80	1.17	27.43

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

COMPUTE VOLUME ID= 1 (0143)	DISCHARGE (cms)	TIME (hrs)
START CONTROLLING AT	2.40	.67
INFLOW HYD. PEAKS AT	18.80	1.17
STOP CONTROLLING AT	15.00	1.39
REQUIRED STORAGE VOLUME (ha.m.)=		1.1543
TOTAL HYDROGRAPH VOLUME (ha.m.)=		29.4907
% OF HYDROGRAPH TO STORE =		3.9143

NOTE: Storage was computed to reduce the Inflow peak to 15.00 (cms).

```

=====
# RESERVOIR #3
=====

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```

RESERVOIR (0201)
IN= 1---> OUT= 4
DT= 5.0 min

```

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.000	.000	11.000	5.600
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)
INFLOW : ID= 1 (0143)	1075.00	1075.00	18.80	1.17
OUTFLOW: ID= 4 (0201)	1075.00	1075.00	10.50	3.67
				R.V. (mm)
				27.43
				27.40
				PEAK FLOW REDUCTION [Qout/Qin](%)= 55.84
				TIME SHIFT OF PEAK FLOW (min)=150.00
				MAXIMUM STORAGE USED (ha.m.)= 5.35

```

=====
# DE POINT "C" A POINT "D"
=====

```

```

ROUTE (0110)
CHANNEL #SEG= 3
IN= 4---> OUT= 1

```

```

Routing time step (min) = 6.00
Slopes (%), CHANNEL= .35 FLOODPLAIN= .35
LENGTH = 2050.00 (m)

```

```

<----- DATA FOR SECTION ( 1.0) ----->

```

Distance	Elevation	Manning	
.00	97.89	.0500	
100.00	95.77	.0500	
102.50	95.57	.0500 / .0300	Main Channel
103.50	94.48	.0300	Main Channel
106.50	94.48	.0300	Main Channel
107.50	95.39	.0300 / .0500	Main Channel
110.00	95.78	.0500	
210.00	96.54	.0500	

```

<----- TRAVEL TIME TABLE ----->

```

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.10	94.58	.643E+03	.1	.41	82.98
.20	94.68	.133E+04	.4	.63	54.10
.30	94.78	.206E+04	.8	.80	42.57
.40	94.88	.283E+04	1.3	.95	36.12
.51	94.99	.364E+04	1.9	1.07	31.92
.61	95.09	.449E+04	2.6	1.18	28.92
.71	95.19	.539E+04	3.4	1.28	26.64
.81	95.29	.633E+04	4.2	1.38	24.84
.91	95.39	.731E+04	5.2	1.46	23.38
1.03	95.51	.855E+04	6.5	1.57	21.79
1.14	95.62	.100E+05	8.1	1.65	20.67
1.25	95.74	.119E+05	9.9	1.70	20.09
1.37	95.85	.152E+05	11.9	1.60	21.29
1.48	95.96	.231E+05	15.0	1.33	25.73
1.60	96.08	.358E+05	19.5	1.12	30.59
1.71	96.19	.533E+05	26.0	1.00	34.16
1.83	96.31	.757E+05	34.9	.95	36.13
1.94	96.42	.103E+06	46.6	.93	36.82
2.06	96.54	.135E+06	61.4	.93	36.66

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 4 (0201)	1075.00	10.50	3.67	27.40	1.29	1.67
OUTFLOW: ID= 1 (0110)	1075.00	10.38	4.08	27.37	1.28	1.68

```

=====
# SOUS-BASSIN -6-Urbain
=====

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```

DESIGN
STANDHYD (0600)
ID= 2 DT= 5.0 min

```

	Area (ha)=	167.00		
	Total Imp(%)=	35.00	Dir. Conn.(%)=	35.00
Surface Area	(ha)=	58.45	IMPERVIOUS	PERVIOUS (i)
Dep. Storage	(mm)=	.80		108.55
				1.50

Average Slope (%) =	1.00	1.00	
Length (m) =	1055.00	40.00	
Mannings n =	.013	.250	
Max. eff. Inten. (mm/hr) =	104.67	29.97	
over (min)	10.00	25.00	
Storage Coeff. (min) =	10.31 (ii)	24.38 (ii)	
Unit Hyd. Tpeak (min) =	10.00	25.00	
Unit Hyd. peak (cms) =	.11	.05	
			TOTALS
PEAK FLOW (cms) =	15.12	4.63	17.81 (iii)
TIME TO PEAK (hrs) =	1.17	1.50	1.17
RUNOFF VOLUME (mm) =	71.50	17.99	36.72
TOTAL RAINFALL (mm) =	72.30	72.30	72.30
RUNOFF COEFFICIENT =	.99	.25	.51

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 55.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

=====
# POINT -D -
=====

```

ADD HYD (0312)				
1 + 2 = 3				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0110):	1075.00	10.38	4.08	27.37
+ ID2= 2 (0600):	167.00	17.81	1.17	36.72

ID = 3 (0312):	1242.00	19.05	1.25	28.63

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0201)				
IN= 3---> OUT= 2				
DT= 5.0 min				
	OUTFLOW	STORAGE	OUTFLOW	STORAGE
	(cms)	(ha.m.)	(cms)	(ha.m.)
	.000	.000	16.000	1.500
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 3 (0312)	1242.00	19.05	1.25	28.63
OUTFLOW: ID= 2 (0201)	1242.00	15.30	1.42	28.63
	PEAK FLOW REDUCTION [Qout/Qin](%) =	80.31		
	TIME SHIFT OF PEAK FLOW (min) =	10.00		
	MAXIMUM STORAGE USED (ha.m.) =	1.45		

```

=====
# ORAGE DE 5-ANS
=====

```

READ STORM	Filename: b:5.ANS						
Ptotal= 48.36 mm	Comments: 5 YEAR STORM (DE FEES)						
TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	4.23	.83	45.05	1.58	9.50	2.33	4.94
.17	4.23	.92	72.96	1.67	9.50	2.42	4.44
.25	5.27	1.00	72.96	1.75	7.67	2.50	4.44
.33	5.27	1.08	62.52	1.83	7.67	2.58	4.03
.42	7.07	1.17	62.52	1.92	6.46	2.67	4.03
.50	7.07	1.25	19.19	2.00	6.46	2.75	3.70
.58	11.52	1.33	19.19	2.08	5.59	2.83	3.70
.67	11.52	1.42	12.59	2.17	5.59	2.92	3.42
.75	45.05	1.50	12.59	2.25	4.94	3.00	3.42

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=====
# SOUS-BASSIN -1AB- ||
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-----
CALIB
NASHYD (0111) Area (ha) = 268.00 Curve Number (CN) = 65.0
ID= 1 DT= 5.0 min Ia (mm) = 2.50 # of Linear Res.(N) = 3.00
U.H. Tp(hrs) = 2.00
-----

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```

Unit Hyd Qpeak (cms) = 5.12

PEAK FLOW (cms) = 2.12 (i)
TIME TO PEAK (hrs) = 3.50
RUNOFF VOLUME (mm) = 11.51
TOTAL RAINFALL (mm) = 48.36
RUNOFF COEFFICIENT = .24

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
RESERVOIR (0201)
IN= 1---> OUT= 2
DT= 5.0 min
-----

```

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.000	.000	.500	50.000
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)
INFLOW : ID= 1 (0111)		268.00	2.12	3.50
OUTFLOW: ID= 2 (0201)		268.00	.03	10.92
				R.V. (mm)
				11.51
				2.85
		PEAK FLOW REDUCTION [Qout/Qin](%)	= 1.41	
		TIME SHIFT OF PEAK FLOW (min)	= 445.00	
		MAXIMUM STORAGE USED (ha.m.)	= 3.00	

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=====
# SOUS-BASSIN -2- ||
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-----
CALIB
NASHYD (0200) Area (ha) = 247.00 Curve Number (CN) = 55.0
ID= 1 DT= 5.0 min Ia (mm) = 2.50 # of Linear Res.(N) = 3.00
U.H. Tp(hrs) = 1.07
-----

```

```

Unit Hyd Qpeak (cms) = 8.82

PEAK FLOW (cms) = 2.23 (i)
TIME TO PEAK (hrs) = 2.42
RUNOFF VOLUME (mm) = 8.29
TOTAL RAINFALL (mm) = 48.36
RUNOFF COEFFICIENT = .17

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

=====
# POINT -A- ||
=====

```

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-----
ADD HYD (0321)
2 + 1 = 3
-----

```

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 2 (0201):	268.00	.03	10.92	2.85
+ ID2= 1 (0200):	247.00	2.23	2.42	8.29
-----	-----	-----	-----	-----
ID = 3 (0321):	515.00	2.24	2.42	5.46

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

=====
# SOUS-BASSIN -4A- Urbain |
=====

```


DESIGN
 STANDHYD (0401)
 ID= 1 DT= 5.0 min

Area (ha)= 90.00
 Total Imp(%)= 75.00 Dir. Conn.(%)= 75.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	67.50	22.50	
Dep. Storage (mm)=	.80	1.50	
Average Slope (%)=	1.00	1.00	
Length (m)=	774.00	40.00	
Mannings n =	.013	.250	
Max. eff. Inten. (mm/hr)=	72.96	10.77	
over (min)	10.00	35.00	
Storage Coeff. (min)=	9.89 (ii)	31.08 (ii)	
Unit Hyd. Tpeak (min)=	10.00	35.00	
Unit Hyd. peak (cms)=	.11	.03	
PEAK FLOW (cms)=	11.30	.36	*TOTALS*
TIME TO PEAK (hrs)=	1.17	1.67	11.44 (iii)
RUNOFF VOLUME (mm)=	47.56	8.62	1.17
TOTAL RAINFALL (mm)=	48.36	48.36	37.82
RUNOFF COEFFICIENT =	.98	.18	48.36
			.78

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 55.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

COMPUTE VOLUME
 ID= 1 (0401)

	DISCHARGE (cms)	TIME (hrs)
START CONTROLLING AT	.01	.18
INFLOW HYD. PEAKS AT	11.44	1.17
STOP CONTROLLING AT	1.50	2.16

REQUIRED STORAGE VOLUME (ha.m.)= 2.4552
 TOTAL HYDROGRAPH VOLUME (ha.m.)= 3.4041
 % OF HYDROGRAPH TO STORE = 72.1254

NOTE: Storage was computed to reduce the Inflow peak to 1.50 (cms).

=====

RESERVOIR NATURELE ||

=====

RESERVOIR (0201)
 IN= 1---> OUT= 4
 DT= 5.0 min

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.000	.000	1.500	10.000
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)
INFLOW : ID= 1 (0401)		90.00	11.44	1.17
OUTFLOW: ID= 4 (0201)		90.00	.46	3.17
				R.V. (mm)
				37.82
				37.37

PEAK FLOW REDUCTION [Qout/Qin](%)= 4.00
 TIME SHIFT OF PEAK FLOW (min)=120.00
 MAXIMUM STORAGE USED (ha.m.)= 3.05

ADD HYD (0321)
 3 + 4 = 5

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 3 (0321):	515.00	2.24	2.42	5.46
+ ID2= 4 (0201):	90.00	.46	3.17	37.37
=====	=====	=====	=====	=====
ID = 5 (0321):	605.00	2.68	2.42	10.20

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

=====

DE POINT "A" A POINT "B" ||

ROUTE (0110)
 CHANNEL #SEG= 3
 IN= 5--> OUT= 3

Routing time step (min) = 6.00
 Slopes (%), CHANNEL= .40 FLOODPLAIN= .40
 LENGTH = 1600.00 (m)

<----- DATA FOR SECTION (1.0) ----->

Distance	Elevation	Manning	
.00	104.24	.0500	
100.00	101.79	.0500	
110.00	101.17	.0500	
113.00	101.17	.0500 / .0300	Main Channel
113.80	100.57	.0300	Main Channel
116.50	100.57	.0300	Main Channel
117.00	101.30	.0300 / .0500	Main Channel
120.00	101.52	.0500	
126.00	102.40	.0500	
226.00	102.98	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.12	100.69	.542E+03	.2	.49	54.71
.24	100.81	.113E+04	.5	.74	36.00
.36	100.93	.176E+04	1.0	.93	28.53
.48	101.05	.245E+04	1.7	1.10	24.35
.60	101.17	.317E+04	2.4	1.23	21.60
.73	101.30	.483E+04	3.7	1.21	22.04
.86	101.43	.710E+04	5.4	1.21	22.10
.99	101.56	.102E+05	7.6	1.20	22.26
1.12	101.69	.139E+05	10.5	1.21	22.04
1.25	101.82	.182E+05	14.0	1.22	21.77
1.38	101.95	.237E+05	17.9	1.21	21.97
1.51	102.08	.303E+05	23.0	1.21	21.95
1.63	102.20	.383E+05	29.3	1.23	21.77
1.76	102.33	.475E+05	37.0	1.24	21.44
1.89	102.46	.586E+05	44.1	1.20	22.16
2.02	102.59	.747E+05	54.4	1.16	22.91
2.15	102.72	.966E+05	68.6	1.14	23.45
2.28	102.85	.124E+06	87.2	1.12	23.74
2.41	102.98	.157E+06	110.5	1.12	23.74

<---- hydrograph ----> <---- channel ---->

	AREA (ha)	OPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 5 (0321)	605.00	2.68	2.42	10.20	.62	1.23
OUTFLOW: ID= 3 (0110)	605.00	2.56	2.75	10.19	.61	1.23

#=====
 # SOUS-BASSIN -4B- Urbain
 #=====

DESIGN
 STANDHYD (0402)
 ID= 1 DT= 5.0 min

Area (ha)= 130.00
 Total Imp(%)= 75.00 Dir. Conn.(%)= 75.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	97.50	32.50
Dep. Storage (mm)=	.80	1.50
Average Slope (%)=	1.00	1.00
Length (m)=	930.00	40.00
Mannings n =	.013	.250
Max. eff. Inten. (mm/hr)=	69.48	10.77
over (min)	10.00	35.00
Storage Coeff. (min)=	11.26 (ii)	32.45 (ii)
Unit Hyd. Tpeak (min)=	10.00	35.00
Unit Hyd. peak (cms)=	.10	.03
PEAK FLOW (cms)=	15.88	.51
TIME TO PEAK (hrs)=	1.17	1.67
RUNOFF VOLUME (mm)=	47.56	8.62
TOTAL RAINFALL (mm)=	48.36	48.36
RUNOFF COEFFICIENT =	.98	.18

TOTALS
 16.07 (iii)
 1.17
 37.82
 48.36
 .78

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 55.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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=====
# POINT -B-
#
=====

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ADD HYD	(0231)	AREA	QPEAK	TPEAK	R.V.
3 + 1 =	2	(ha)	(cms)	(hrs)	(mm)
ID1= 3	(0110):	605.00	2.56	2.75	10.19
+ ID2= 1	(0402):	130.00	16.07	1.17	37.82
ID = 2 (0231):		735.00	16.16	1.17	15.08

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

COMPUTE VOLUME	DISCHARGE	TIME
ID= 2 (0231)	(cms)	(hrs)
START CONTROLLING AT	2.34	.67
INFLOW HYD. PEAKS AT	16.16	1.17
STOP CONTROLLING AT	13.00	1.30
REQUIRED STORAGE VOLUME (ha.m.)=		.7700
TOTAL HYDROGRAPH VOLUME (ha.m.)=		11.0812
% OF HYDROGRAPH TO STORE		= 6.9486

NOTE: Storage was computed to reduce the Inflow peak to 13.00 (cms).

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=====
# RESERVOIR #1+ #2
#
=====

```

RESERVOIR (0201)	OUTFLOW	STORAGE	OUTFLOW	STORAGE	
IN= 2---> OUT= 3	(cms)	(ha.m.)	(cms)	(ha.m.)	
DT= 5.0 min	.000	.000	7.000	5.800	
		AREA	QPEAK	TPEAK	R.V.
INFLOW : ID= 2 (0231)		(ha)	(cms)	(hrs)	(mm)
OUTFLOW: ID= 3 (0201)		735.00	16.16	1.17	15.08
		735.00	3.98	2.67	15.04
PEAK FLOW REDUCTION [Qout/Qin](%)=					24.65
TIME SHIFT OF PEAK FLOW					(min)= 90.00
MAXIMUM STORAGE USED					(ha.m.)= 3.30

```

=====
# DE POINT "B" A POINT "C"
#
=====

```

ROUTE (0110)	Routing time step (min) =	6.00
CHANNEL #SEG= 3	Slopes (%), CHANNEL=	.40 FLOODPLAIN= .40
IN= 3---> OUT= 2	LENGTH =	1800.00 (m)

Distance	Elevation	Manning	
.00	104.24	.0500	
100.00	101.79	.0500	
110.00	101.17	.0500	
113.00	101.17	.0500 / .0300	Main Channel
113.80	100.57	.0300	Main Channel
116.50	100.57	.0300	Main Channel
117.00	101.30	.0300 / .0500	Main Channel
120.00	101.52	.0500	
126.00	102.40	.0500	
226.00	102.98	.0500	

←----- TRAVEL TIME TABLE ----->
 DEPTH ELEV VOLUME FLOW RATE VELOCITY TRAV.TIME

(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.12	100.69	.609E+03	.2	.49	61.55
.24	100.81	.127E+04	.5	.74	40.50
.36	100.93	.199E+04	1.0	.93	32.10
.48	101.05	.275E+04	1.7	1.10	27.39
.60	101.17	.357E+04	2.4	1.23	24.30
.73	101.30	.543E+04	3.7	1.21	24.79
.86	101.43	.799E+04	5.4	1.21	24.86
.99	101.56	.114E+05	7.6	1.20	25.04
1.12	101.69	.156E+05	10.5	1.21	24.79
1.25	101.82	.205E+05	14.0	1.22	24.49
1.38	101.95	.266E+05	17.9	1.21	24.71
1.51	102.08	.341E+05	23.0	1.21	24.70
1.63	102.20	.431E+05	29.3	1.23	24.49
1.76	102.33	.535E+05	37.0	1.24	24.12
1.89	102.46	.659E+05	44.1	1.20	24.93
2.02	102.59	.841E+05	54.4	1.16	25.78
2.15	102.72	.109E+06	68.6	1.14	26.38
2.28	102.85	.140E+06	87.2	1.12	26.71
2.41	102.98	.177E+06	110.5	1.12	26.71

	AREA (ha)	<--- hydrograph --->			<--- channel --->	
		QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 3 (0201)	735.00	3.98	2.67	15.04	.75	1.21
OUTFLOW: ID= 2 (0110)	735.00	3.92	3.17	15.03	.75	1.21

```

=====
# DE POINT "C" A POINT "C'"
#=====

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ROUTE (0110) Routing time step (min) = 6.00
CHANNEL #SEG= 3
IN= 2---> OUT= 3 Slopes (%), CHANNEL= .35 FLOODPLAIN= .35
LENGTH = 800.00 (m)

```

<----- DATA FOR SECTION (1.0) ----->

Distance	Elevation	Manning	
100.00	97.89	.0500	
102.50	95.77	.0500	
103.50	94.48	.0300	Main Channel
106.50	94.48	.0300	Main Channel
107.50	95.39	.0300 / .0500	Main Channel
110.00	95.78	.0500	
210.00	96.54	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.10	94.58	.251E+03	.1	.41	32.38
.20	94.68	.518E+03	.4	.63	21.11
.30	94.78	.802E+03	.8	.80	16.61
.40	94.88	.110E+04	1.3	.95	14.10
.51	94.99	.142E+04	1.9	1.07	12.46
.61	95.09	.175E+04	2.6	1.18	11.28
.71	95.19	.210E+04	3.4	1.28	10.40
.81	95.29	.247E+04	4.2	1.38	9.69
.91	95.39	.285E+04	5.2	1.46	9.12
1.03	95.51	.334E+04	6.5	1.57	8.50
1.14	95.62	.391E+04	8.1	1.65	8.06
1.25	95.74	.466E+04	9.9	1.70	7.84
1.37	95.85	.595E+04	11.9	1.60	8.31
1.48	95.96	.901E+04	15.0	1.33	10.04
1.60	96.08	.140E+05	19.5	1.12	11.94
1.71	96.19	.208E+05	26.0	1.00	13.33
1.83	96.31	.295E+05	34.9	.95	14.10
1.94	96.42	.402E+05	46.6	.93	14.37
2.06	96.54	.527E+05	61.4	.93	14.31

	AREA (ha)	<--- hydrograph --->			<--- channel --->	
		QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 2 (0110)	735.00	3.92	3.17	15.03	.77	1.34
OUTFLOW: ID= 3 (0110)	735.00	3.91	3.33	15.02	.77	1.34

```

=====
# SOUS-BASSIN -3-
#=====

```

 CALIB
 NASHYD (0300)
 ID= 1 DT= 5.0 min

Area (ha) = 204.00 Curve Number (CN) = 68.0
 Ia (mm) = 2.50 # of Linear Res. (N) = 3.00
 U.H. Tp(hrs) = 1.58

Unit Hyd Qpeak (cms) = 4.93
 PEAK FLOW (cms) = 2.14 (i)
 TIME TO PEAK (hrs) = 3.00
 RUNOFF VOLUME (mm) = 12.71
 TOTAL RAINFALL (mm) = 48.36
 RUNOFF COEFFICIENT = .26

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 # SOUS-BASSIN -5- Urbain |
 #####

 DESIGN
 STANDHYD (0500)
 ID= 2 DT= 5.0 min

Area (ha) = 136.00
 Total Imp(%) = 45.00 Dir. Conn.(%) = 45.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha) =	61.20	74.80
Dep. Storage (mm) =	.80	1.50
Average Slope (%) =	1.00	1.00
Length (m) =	952.00	40.00
Mannings n =	.013	.250
Max.eff.Inten.(mm/hr) =	69.48	10.77
over (min) =	10.00	35.00
Storage Coeff. (min) =	11.42 (ii)	32.61 (ii)
Unit Hyd. Tpeak (min) =	10.00	35.00
Unit Hyd. peak (cms) =	.10	.03
PEAK FLOW (cms) =	9.93	1.17
TIME TO PEAK (hrs) =	1.17	1.67
RUNOFF VOLUME (mm) =	47.56	8.62
TOTAL RAINFALL (mm) =	48.36	48.36
RUNOFF COEFFICIENT =	.98	.18

TOTALS
 10.37 (iii)
 1.17
 26.14
 48.36
 .54

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 55.0 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 ADD HYD (0412) |
 1 + 2 = 4

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0300):	204.00	2.14	3.00	12.71
+ ID2= 2 (0500):	136.00	10.37	1.17	26.14
=====				
ID = 4 (0412):	340.00	10.53	1.17	18.09

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

 # POINT -C'- | |
 #####

 ADD HYD (0143) |
 4 + 3 = 1

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 4 (0412):	340.00	10.53	1.17	18.09
+ ID2= 3 (0110):	735.00	3.91	3.33	15.02
=====				
ID = 1 (0143):	1075.00	10.72	1.17	15.99

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

COMPUTE VOLUME
ID= 1 (0143)

DISCHARGE TIME
(cms) (hrs)

**** WARNING: NO STORAGE REQUIRED, RELEASE > INFLOW PEAK

=====

RESERVOIR #3 ||

=====

RESERVOIR (0201)
IN= 1---> OUT= 4
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.000	.000	11.000	5.600

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 1 (0143)	1075.00	10.72	1.17	15.99
OUTFLOW: ID= 4 (0201)	1075.00	6.08	3.58	15.97

PEAK FLOW REDUCTION [Qout/Qin] (%) = 56.68
TIME SHIFT OF PEAK FLOW (min) = 145.00
MAXIMUM STORAGE USED (ha.m.) = 3.09

=====

DE POINT "C" A POINT "D " ||

=====

ROUTE (0110)
CHANNEL #SEG= 3
IN= 4---> OUT= 1

Routing time step (min) = 6.00
Slopes (%), CHANNEL= .35 FLOODPLAIN= .35
LENGTH = 2050.00 (m)

<----- DATA FOR SECTION (1.0) ----->

Distance	Elevation	Manning	
.00	97.89	.0500	
100.00	95.77	.0500	
102.50	95.57	.0500 / .0300	Main Channel
103.50	94.48	.0300	Main Channel
106.50	94.48	.0300	Main Channel
107.50	95.39	.0300 / .0500	Main Channel
110.00	95.78	.0500	
210.00	96.54	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.10	94.58	.643E+03	.1	.41	82.98
.20	94.68	.133E+04	.4	.63	54.10
.30	94.78	.206E+04	.8	.80	42.57
.40	94.88	.283E+04	1.3	.95	36.12
.51	94.99	.364E+04	1.9	1.07	31.92
.61	95.09	.449E+04	2.6	1.18	28.92
.71	95.19	.539E+04	3.4	1.28	26.64
.81	95.29	.633E+04	4.2	1.38	24.84
.91	95.39	.731E+04	5.2	1.46	23.38
1.03	95.51	.855E+04	6.5	1.57	21.79
1.14	95.62	.100E+05	8.1	1.65	20.67
1.25	95.74	.119E+05	9.9	1.70	20.09
1.37	95.85	.152E+05	11.9	1.60	21.29
1.48	95.96	.231E+05	15.0	1.33	25.73
1.60	96.08	.358E+05	19.5	1.12	30.59
1.71	96.19	.533E+05	26.0	1.00	34.16
1.83	96.31	.757E+05	34.9	.95	36.13
1.94	96.42	.103E+06	46.6	.93	36.82
2.06	96.54	.135E+06	61.4	.93	36.66

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 4 (0201)	1075.00	6.08	3.58	15.97	.99	1.53
OUTFLOW: ID= 1 (0110)	1075.00	6.02	3.92	15.96	.98	1.52

=====

SOUS-BASSIN -6-Urbain |
#=====

DESIGN
STANDHYD (0600)
ID= 2 DT= 5.0 min

Area (ha)= 167.00
Total Imp(%)= 35.00 Dir. Conn.(%)= 35.00

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	58.45	108.55	
Dep. Storage	(mm)=	.80	1.50	
Average Slope	(%)=	1.00	1.00	
Length	(m)=	1055.00	40.00	
Mannings n	=	.013	.250	
Max.eff.Inten.(mm/hr)=		69.48	10.77	
over (min)		10.00	35.00	
Storage Coeff. (min)=		12.15 (ii)	33.34 (ii)	
Unit Hyd. Tpeak (min)=		10.00	35.00	
Unit Hyd. peak (cms)=		.10	.03	
				TOTALS
PEAK FLOW (cms)=		9.34	1.68	9.96 (iii)
TIME TO PEAK (hrs)=		1.17	1.67	1.17
RUNOFF VOLUME (mm)=		47.56	8.62	22.25
TOTAL RAINFALL (mm)=		48.36	48.36	48.36
RUNOFF COEFFICIENT =		.98	.18	.46

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 55.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

#=====

POINT -D -

ADD HYD (0312)
1 + 2 = 3

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0110):	1075.00	6.02	3.92	15.96
+ ID2= 2 (0600):	167.00	9.96	1.17	22.25
=====	=====	=====	=====	=====
ID = 3 (0312):	1242.00	10.50	1.17	16.80

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

RESERVOIR (0201)
IN= 3---> OUT= 2
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.000	.000	16.000	1.500

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 3 (0312)	1242.00	10.50	1.17	16.80
OUTFLOW: ID= 2 (0201)	1242.00	8.33	1.42	16.80

PEAK FLOW REDUCTION [Qout/Qin](%)= 79.38
TIME SHIFT OF PEAK FLOW (min)= 15.00
MAXIMUM STORAGE USED (ha.m.)= .79

#=====

ORAGE DE 2-ANS

READ STORM
Ptotal= 30.61 mm

Filename: b:2.ANS
Comments: 2 YEAR STORM (DE FEES)

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	2.08	.83	33.20	1.58	5.36	2.33	2.49
.17	2.08	.92	45.38	1.67	5.36	2.42	2.20
.25	2.69	1.00	45.38	1.75	4.17	2.50	2.20

.33	2.69	1.08	42.19	1.83	4.17	2.58	1.97
.42	3.79	1.17	42.19	1.92	3.41	2.67	1.97
.50	3.79	1.25	13.17	2.00	3.41	2.75	1.78
.58	7.85	1.33	13.17	2.08	2.88	2.83	1.78
.67	7.85	1.42	7.41	2.17	2.88	2.92	1.63
.75	33.20	1.50	7.41	2.25	2.49	3.00	1.63

#=====

SOUS-BASSIN -1AB- ||

CALIB
 NASHYD (0111) | Area (ha)= 268.00 Curve Number (CN)= 65.0
 ID= 1 DT= 5.0 min | Ia (mm)= 2.50 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 2.00

Unit Hyd Qpeak (cms)= 5.12
 PEAK FLOW (cms)= .89 (i)
 TIME TO PEAK (hrs)= 3.42
 RUNOFF VOLUME (mm)= 4.79
 TOTAL RAINFALL (mm)= 30.61
 RUNOFF COEFFICIENT = .16

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

RESERVOIR (0201)
 IN= 1---> OUT= 2
 DT= 5.0 min

	OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
	.000	.000	.500	50.000
		AREA (ha)	QPEAK (cms)	TPEAK (hrs)
INFLOW : ID= 1 (0111)		268.00	.89	3.42
OUTFLOW: ID= 2 (0201)		268.00	.01	10.92

PEAK FLOW REDUCTION [Qout/Qin](%)= 1.40
 TIME SHIFT OF PEAK FLOW (min)=450.00
 MAXIMUM STORAGE USED (ha.m.)= 1.25

SOUS-BASSIN -2- ||

CALIB
 NASHYD (0200) | Area (ha)= 247.00 Curve Number (CN)= 55.0
 ID= 1 DT= 5.0 min | Ia (mm)= 2.50 # of Linear Res.(N)= 3.00
 U.H. Tp(hrs)= 1.07

Unit Hyd Qpeak (cms)= 8.82
 PEAK FLOW (cms)= .93 (i)
 TIME TO PEAK (hrs)= 2.33
 RUNOFF VOLUME (mm)= 3.35
 TOTAL RAINFALL (mm)= 30.61
 RUNOFF COEFFICIENT = .11

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

POINT -A- ||

ADD HYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
2 + 1 = 3				
+ ID1= 2 (0201):	268.00	.01	10.92	1.19
+ ID2= 1 (0200):	247.00	.93	2.33	3.35

	(ha)	(cms)	(hrs)	(mm)
ID1= 3 (0321):	515.00	.94	2.33	2.22
+ ID2= 4 (0201):	90.00	.28	3.17	22.97

ID = 5 (0321):	605.00	1.21	2.33	5.31

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

=====

DE POINT "A" A POINT "B" ||

=====

ROUTE (0110) Routing time step (min) = 6.00
 CHANNEL #SEG= 3
 IN= 5----> OUT= 3 Slopes (%), CHANNEL= .40 FLOODPLAIN= .40
 LENGTH = 1600.00 (m)

<----- DATA FOR SECTION (1.0) ----->

Distance	Elevation	Manning	
.00	104.24	.0500	
100.00	101.79	.0500	
110.00	101.17	.0500	
113.00	101.17	.0500 / .0300	Main Channel
113.80	100.57	.0300	Main Channel
116.50	100.57	.0300	Main Channel
117.00	101.30	.0300 / .0500	Main Channel
120.00	101.52	.0500	
126.00	102.40	.0500	
226.00	102.98	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.12	100.69	.542E+03	.2	.49	54.71
.24	100.81	.113E+04	.5	.74	36.00
.36	100.93	.176E+04	1.0	.93	28.53
.48	101.05	.245E+04	1.7	1.10	24.35
.60	101.17	.317E+04	2.4	1.23	21.60
.73	101.30	.483E+04	3.7	1.21	22.04
.86	101.43	.710E+04	5.4	1.21	22.10
.99	101.56	.102E+05	7.6	1.20	22.26
1.12	101.69	.139E+05	10.5	1.21	22.04
1.25	101.82	.182E+05	14.0	1.22	21.77
1.38	101.95	.237E+05	17.9	1.21	21.97
1.51	102.08	.303E+05	23.0	1.21	21.95
1.63	102.20	.383E+05	29.3	1.23	21.77
1.76	102.33	.475E+05	37.0	1.24	21.44
1.89	102.46	.586E+05	44.1	1.20	22.16
2.02	102.59	.747E+05	54.4	1.16	22.91
2.15	102.72	.966E+05	68.6	1.14	23.45
2.28	102.85	.124E+06	87.2	1.12	23.74
2.41	102.98	.157E+06	110.5	1.12	23.74

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 5 (0321)	605.00	1.21	2.33	5.31	.39	.97
OUTFLOW: ID= 3 (0110)	605.00	1.12	2.83	5.30	.38	.95

=====

SOUS-BASSIN -4B- Urbain |

=====

DESIGN STANDHYD (0402)
 ID= 1 DT= 5.0 min

Area (ha)= 130.00
 Total Imp(%)= 75.00 Dir. Conn.(%)= 75.00

	IMPERVIOUS (ha)	PERVIOUS (i)
Surface Area	97.50	32.50
Dep. Storage	.80	1.50
Average Slope	1.00	1.00
Length	930.00	40.00
Mannings n	.013	.250
Max.eff.Inten.(mm/hr)=	44.32	3.98
over (min)	15.00	50.00
Storage Coeff. (min)=	13.48 (ii)	45.03 (ii)
Unit Hyd. Tpeak (min)=	15.00	50.00
Unit Hyd. peak (cms)=	.08	.02
PEAK FLOW (cms)=	9.57	.18

TOTALS
 9.61 (iii)

TIME TO PEAK	(hrs) =	1.17	1.92	1.17
RUNOFF VOLUME	(mm) =	29.81	3.58	23.25
TOTAL RAINFALL	(mm) =	30.61	30.61	30.61
RUNOFF COEFFICIENT	=	.97	.12	.76

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 55.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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=====
# POINT -B-
=====

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ADD HYD (0231)	AREA	QPEAK	TPEAK	R.V.
3 + 1 = 2	(ha)	(cms)	(hrs)	(mm)
ID1= 3 (0110):	605.00	1.12	2.83	5.30
+ ID2= 1 (0402):	130.00	9.61	1.17	23.25
=====				
ID = 2 (0231):	735.00	9.65	1.25	8.48

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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=====
COMPUTE VOLUME
ID= 2 (0231)
DISCHARGE TIME
(cms) (hrs)
**** WARNING: NO STORAGE REQUIRED, RELEASE > INFLOW PEAK
=====

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=====
# RESERVOIR #1+ #2
=====

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RESERVOIR (0201)	OUTFLOW	STORAGE	OUTFLOW	STORAGE
IN= 2---> OUT= 3	(cms)	(ha.m.)	(cms)	(ha.m.)
DT= 5.0 min	.000	.000	7.000	5.800
=====				
	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW : ID= 2 (0231)	735.00	9.65	1.25	8.48
OUTFLOW: ID= 3 (0201)	735.00	2.40	2.08	8.46
=====				
PEAK FLOW REDUCTION [Qout/Qin](%)	= 24.87			
TIME SHIFT OF PEAK FLOW (min)	= 50.00			
MAXIMUM STORAGE USED (ha.m.)	= 1.99			

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=====
# DE POINT "B" A POINT "C"
=====

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ROUTE (0110)	Routing time step (min) =	6.00
CHANNEL #SEG= 3	Slopes (%), CHANNEL=	.40 FLOODPLAIN= .40
IN= 3---> OUT= 2	LENGTH =	1800.00 (m)

<----- DATA FOR SECTION (1.0) ----->

Distance	Elevation	Manning	
.00	104.24	.0500	
100.00	101.79	.0500	
110.00	101.17	.0500	
113.00	101.17	.0500 / .0300	Main Channel
113.80	100.57	.0300	Main Channel
116.50	100.57	.0300	Main Channel
117.00	101.30	.0300 / .0500	Main Channel
120.00	101.52	.0500	
126.00	102.40	.0500	
226.00	102.98	.0500	

----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.12	100.69	.609E+03	.2	.49	61.55
.24	100.81	.127E+04	.5	.74	40.50
.36	100.93	.199E+04	1.0	.93	32.10
.48	101.05	.275E+04	1.7	1.10	27.39
.60	101.17	.357E+04	2.4	1.23	24.30
.73	101.30	.543E+04	3.7	1.21	24.79
.86	101.43	.799E+04	5.4	1.21	24.86
.99	101.56	.114E+05	7.6	1.20	25.04
1.12	101.69	.156E+05	10.5	1.21	24.79
1.25	101.82	.205E+05	14.0	1.22	24.49
1.38	101.95	.266E+05	17.9	1.21	24.71
1.51	102.08	.341E+05	23.0	1.21	24.70
1.63	102.20	.431E+05	29.3	1.23	24.49
1.76	102.33	.535E+05	37.0	1.24	24.12
1.89	102.46	.659E+05	44.1	1.20	24.93
2.02	102.59	.841E+05	54.4	1.16	25.78
2.15	102.72	.109E+06	68.6	1.14	26.38
2.28	102.85	.140E+06	87.2	1.12	26.71
2.41	102.98	.177E+06	110.5	1.12	26.71

	AREA	<---- hydrograph ---->			<---- channel ---->	
	(ha)	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
		(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 3 (0201)	735.00	2.40	2.08	8.46	.59	1.22
OUTFLOW: ID= 2 (0110)	735.00	2.31	2.67	8.45	.58	1.21

```

=====
# DE POINT "C" A POINT "C'" ||
=====

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ROUTE (0110) Routing time step (min) = 6.00
CHANNEL #SEG= 3
IN= 2----> OUT= 3 Slopes (%), CHANNEL= .35 FLOODPLAIN= .35
LENGTH = 800.00 (m)

```

<----- DATA FOR SECTION (1.0) ----->					
Distance	Elevation	Manning			
.00	97.89	.0500			
100.00	95.77	.0500			
102.50	95.57	.0500 / .0300	Main Channel		
103.50	94.48	.0300	Main Channel		
106.50	94.48	.0300	Main Channel		
107.50	95.39	.0300 / .0500	Main Channel		
110.00	95.78	.0500			
210.00	96.54	.0500			

----- TRAVEL TIME TABLE ----->					
DEPTH	ELEV	VOLUME	FLOW RATE	VELOCITY	TRAV.TIME
(m)	(m)	(cu.m.)	(cms)	(m/s)	(min)
.10	94.58	.251E+03	.1	.41	32.38
.20	94.68	.518E+03	.4	.63	21.11
.30	94.78	.802E+03	.8	.80	16.61
.40	94.88	.110E+04	1.3	.95	14.10
.51	94.99	.142E+04	1.9	1.07	12.46
.61	95.09	.175E+04	2.6	1.18	11.28
.71	95.19	.210E+04	3.4	1.28	10.40
.81	95.29	.247E+04	4.2	1.38	9.69
.91	95.39	.285E+04	5.2	1.46	9.12
1.03	95.51	.334E+04	6.5	1.57	8.50
1.14	95.62	.391E+04	8.1	1.65	8.06
1.25	95.74	.466E+04	9.9	1.70	7.84
1.37	95.85	.595E+04	11.9	1.60	8.31
1.48	95.96	.901E+04	15.0	1.33	10.04
1.60	96.08	.140E+05	19.5	1.12	11.94
1.71	96.19	.208E+05	26.0	1.00	13.33
1.83	96.31	.295E+05	34.9	.95	14.10
1.94	96.42	.402E+05	46.6	.93	14.37
2.06	96.54	.527E+05	61.4	.93	14.31

	AREA	<---- hydrograph ---->			<---- channel ---->	
	(ha)	QPEAK	TPEAK	R.V.	MAX DEPTH	MAX VEL
		(cms)	(hrs)	(mm)	(m)	(m/s)
INFLOW : ID= 2 (0110)	735.00	2.31	2.67	8.45	.57	1.13
OUTFLOW: ID= 3 (0110)	735.00	2.30	2.92	8.45	.56	1.13

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=====
# SOUS-BASSIN -3- ||
=====

```

#=====

CALIB
NASHYD (0300)
ID= 1 DT= 5.0 min

Area (ha)= 204.00
Ia (mm)= 2.50
U.H. Tp(hrs)= 1.58

Curve Number (CN)= 68.0
of Linear Res.(N)= 3.00

Unit Hyd Qpeak (cms)= 4.93
PEAK FLOW (cms)= .92 (i)
TIME TO PEAK (hrs)= 3.00
RUNOFF VOLUME (mm)= 5.35
TOTAL RAINFALL (mm)= 30.61
RUNOFF COEFFICIENT = .17

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

#=====
SOUS-BASSIN -5- Urbain
#=====

DESIGN
STANDHYD (0500)
ID= 2 DT= 5.0 min

Area (ha)= 136.00
Total Imp(%)= 45.00 Dir. Conn.(%)= 45.00

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 61.20 74.80
Dep. Storage (mm)= .80 1.50
Average Slope (%)= 1.00 1.00
Length (m)= 952.00 40.00
Mannings n = .013 .250

Max.eff.Inten.(mm/hr)= 44.32 3.98
over (min) 15.00 50.00
Storage Coeff. (min)= 13.67 (ii) 45.22 (ii)
Unit Hyd. Tpeak (min)= 15.00 50.00
Unit Hyd. peak (cms)= .08 .02

PEAK FLOW (cms)= 5.98 .41 *TOTALS*
TIME TO PEAK (hrs)= 1.17 1.92 6.09 (iii)
RUNOFF VOLUME (mm)= 29.81 3.58 1.25
TOTAL RAINFALL (mm)= 30.61 30.61 15.38
RUNOFF COEFFICIENT = .97 .12 .50

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 55.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

ADD HYD (0412)
1 + 2 = 4

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 1 (0300):	204.00	.92	3.00	5.35
+ ID2= 2 (0500):	136.00	6.09	1.25	15.38
ID = 4 (0412):	340.00	6.19	1.25	9.36

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

#=====
POINT -C'-
#=====

ADD HYD (0143)
4 + 3 = 1

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
ID1= 4 (0412):	340.00	6.19	1.25	9.36
+ ID2= 3 (0110):	735.00	2.30	2.92	8.45
ID = 1 (0143):	1075.00	6.29	1.25	8.74

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

COMPUTE VOLUME
ID= 1 (0143)

DISCHARGE (cms) TIME (hrs)

**** WARNING: NO STORAGE REQUIRED, RELEASE > INFLOW PEAK

=====||
RESERVOIR #3 ||
#=====||

RESERVOIR (0201)
IN= 1---> OUT= 4
DT= 5.0 min

OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.000	.000	11.000	5.600

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW : ID= 1 (0143)	1075.00	6.29	1.25	8.74
OUTFLOW: ID= 4 (0201)	1075.00	3.32	3.42	8.73

PEAK FLOW REDUCTION [Qout/Qin](%) = 52.84
TIME SHIFT OF PEAK FLOW (min) = 130.00
MAXIMUM STORAGE USED (ha.m.) = 1.69

=====||
DE POINT "C" A POINT "D " ||
#=====||

ROUTE (0110)
CHANNEL #SEG= 3
IN= 4---> OUT= 1

Routing time step (min) = 6.00
Slopes (%), CHANNEL= .35 FLOODPLAIN= .35
LENGTH = 2050.00 (m)

<----- DATA FOR SECTION (1.0) ----->

Distance	Elevation	Manning	
.00	97.89	.0500	
100.00	95.77	.0500	
102.50	95.57	.0500 / .0300	Main Channel
103.50	94.48	.0300	Main Channel
106.50	94.48	.0300	Main Channel
107.50	95.39	.0300 / .0500	Main Channel
110.00	95.78	.0500	
210.00	96.54	.0500	

<----- TRAVEL TIME TABLE ----->

DEPTH (m)	ELEV (m)	VOLUME (cu.m.)	FLOW RATE (cms)	VELOCITY (m/s)	TRAV.TIME (min)
.10	94.58	.643E+03	.1	.41	82.98
.20	94.68	.133E+04	.4	.63	54.10
.30	94.78	.206E+04	.8	.80	42.57
.40	94.88	.283E+04	1.3	.95	36.12
.51	94.99	.364E+04	1.9	1.07	31.92
.61	95.09	.449E+04	2.6	1.18	28.92
.71	95.19	.539E+04	3.4	1.28	26.64
.81	95.29	.633E+04	4.2	1.38	24.84
.91	95.39	.731E+04	5.2	1.46	23.38
1.03	95.51	.855E+04	6.5	1.57	21.79
1.14	95.62	.100E+05	8.1	1.65	20.67
1.25	95.74	.119E+05	9.9	1.70	20.09
1.37	95.85	.152E+05	11.9	1.60	21.29
1.48	95.96	.231E+05	15.0	1.33	25.73
1.60	96.08	.358E+05	19.5	1.12	30.59
1.71	96.19	.533E+05	26.0	1.00	34.16
1.83	96.31	.757E+05	34.9	.95	36.13
1.94	96.42	.103E+06	46.6	.93	36.82
2.06	96.54	.135E+06	61.4	.93	36.66

	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	MAX DEPTH (m)	MAX VEL (m/s)
INFLOW : ID= 4 (0201)	1075.00	3.32	3.42	8.73	.70	1.28
OUTFLOW: ID= 1 (0110)	1075.00	3.27	3.75	8.72	.70	1.27

=====

SOUS-BASSIN -6-Urbain |

=====

DESIGN

STANDHYD (0600)

ID= 2 DT= 5.0 min

Area (ha)= 167.00

Total Imp(%)= 35.00

Dir. Conn.(%)= 35.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	58.45	108.55	
Dep. Storage (mm)=	.80	1.50	
Average Slope (%)=	1.00	1.00	
Length (m)=	1055.00	40.00	
Mannings n =	.013	.250	
Max. eff. Inten. (mm/hr)=	44.32	3.98	
over (min)	15.00	50.00	
Storage Coeff. (min)=	14.54 (ii)	46.09 (ii)	
Unit Hyd. Tpeak (min)=	15.00	50.00	
Unit Hyd. peak (cms)=	.08	.02	
PEAK FLOW (cms)=	5.60	.59	*TOTALS* 5.78 (iii)
TIME TO PEAK (hrs)=	1.25	1.92	1.25
RUNOFF VOLUME (mm)=	29.81	3.58	12.76
TOTAL RAINFALL (mm)=	30.61	30.61	30.61
RUNOFF COEFFICIENT =	.97	.12	.42

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 55.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

=====

POINT -D -

=====

ADD HYD (0312)	AREA	QPEAK	TPEAK	R.V.
1 + 2 = 3	(ha)	(cms)	(hrs)	(mm)
ID1= 1 (0110):	1075.00	3.27	3.75	8.72
+ ID2= 2 (0600):	167.00	5.78	1.25	12.76
ID = 3 (0312):	1242.00	6.07	1.25	9.26

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

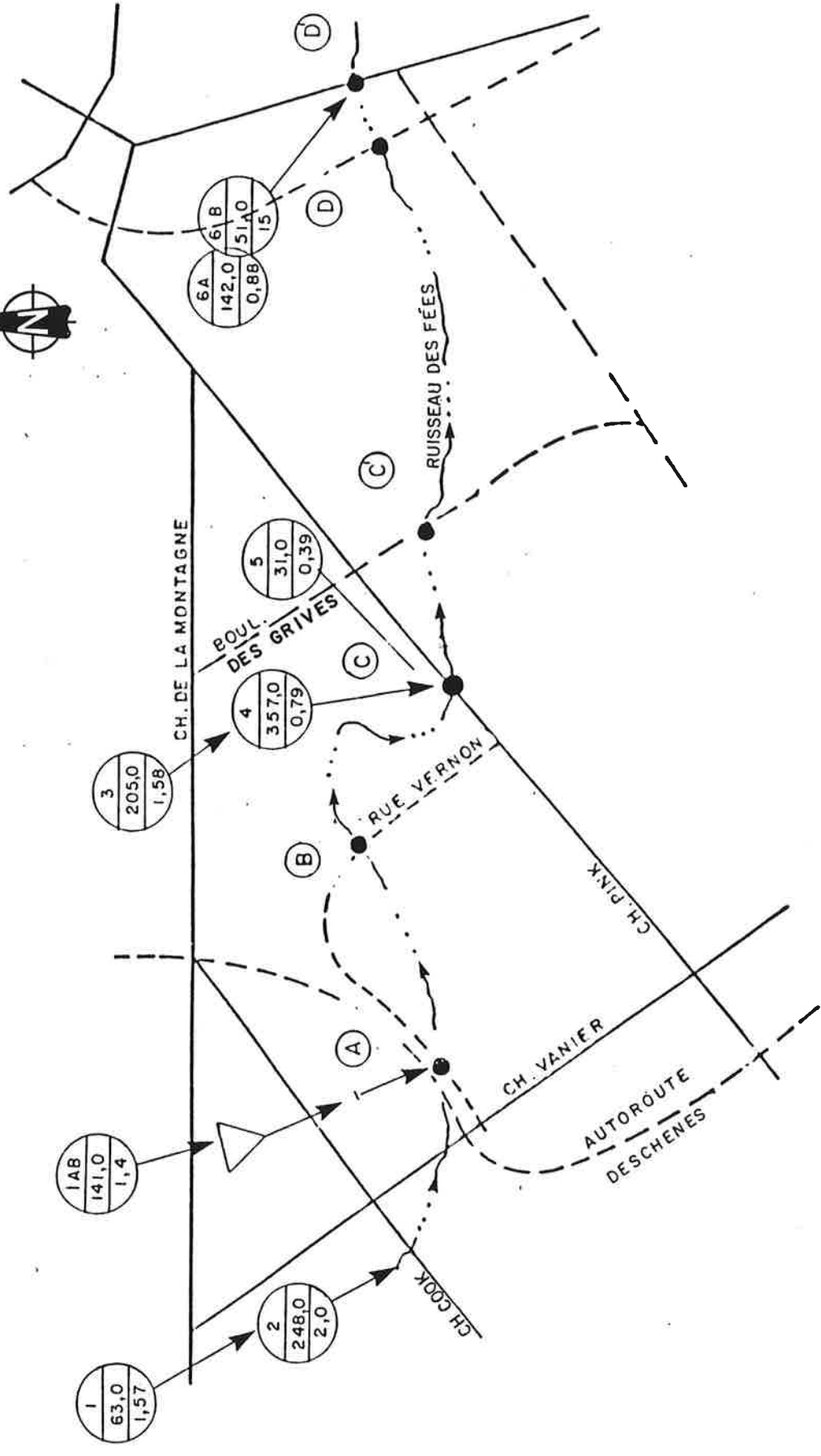
RESERVOIR (0201)	OUTFLOW	STORAGE	OUTFLOW	STORAGE
IN= 3---> OUT= 2	(cms)	(ha.m.)	(cms)	(ha.m.)
DT= 5.0 min				
	.000	.000	16.000	1.500
		AREA	TPEAK	R.V.
		(ha)	(hrs)	(mm)
INFLOW : ID= 3 (0312)		1242.00	1.25	9.26
OUTFLOW: ID= 2 (0201)		1242.00	1.50	9.26
		QPEAK	TPEAK	R.V.
		(cms)	(hrs)	(mm)
		6.07	1.25	9.26
		4.89	1.50	9.26
		PEAK FLOW REDUCTION [Qout/Qin](%)=	80.58	
		TIME SHIFT OF PEAK FLOW (min)=	15.00	
		MAXIMUM STORAGE USED (ha.m.)=	.47	

=====





FINISH

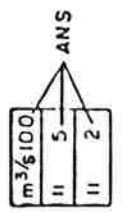
=====

**SCHEMA DU MODELE OTTHYMO
CONDITIONS NON - URBANISEES**



LÉGENDE

- 
 RÉSERVOIR DE RETENTION SUGGÉRÉ
- 
 NO DU SOUS-BASSIN SUPERFICIE (Ha)
Tp. (hrs) ou imp (%)
- 
 RÉSERVOIR DE RETENTION EN AMONT DU PONCEAU
- 
 NO DU SOUS-BASSIN SUPERFICIE (Ha)
Tp. (hrs) ou imp (%)

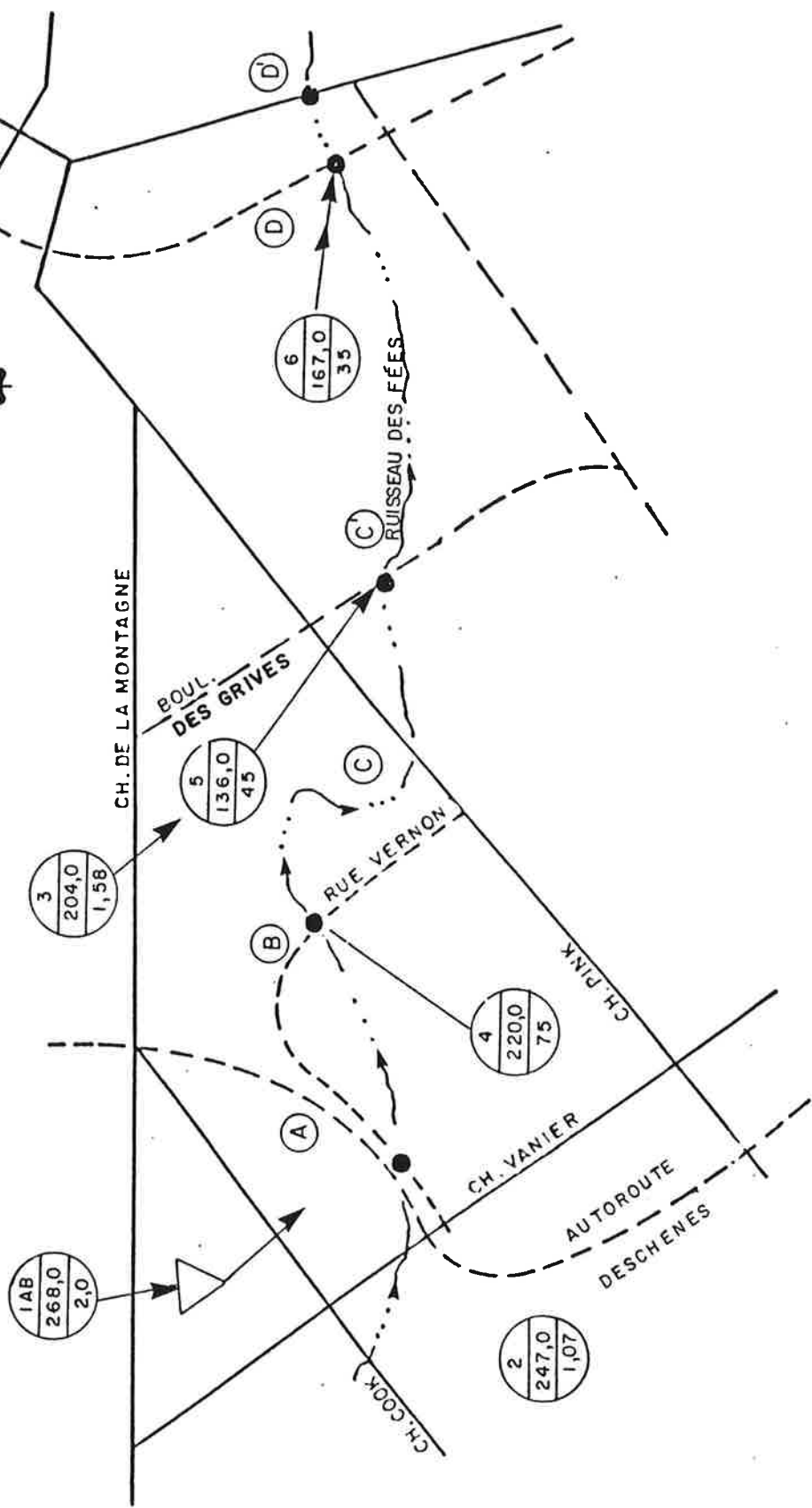


DESSINÉ PAR : C.V.
 PRÉPARÉ PAR : *[Signature]*


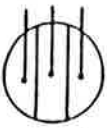

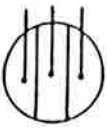
LES CONSULTANTS DE L'OUTAOUAIS INC.
 EXPERTS - CONSEILS
 MODÈLE OTTHYMO

DATE : 11 / 05 / 92
 ÉCHELLE : _____
 368-013-1

**SCHEMA DU MODELE OTTHYMO
CONDITIONS URBANISEES
NON-CONTROLEES**



LÉGENDE

- 
RÉSERVOIR DE RETENTION SUGGÉRÉ
- 
RÉSERVOIR DE RETENTION EN AMONT DU PONCEAU
- 
RÉSERVOIR DE RETENTION NATUREL
- 
NO DU SOUS-BASSIN SUPERFICIE (Mo) Tp, (hrs) OU imp (%)

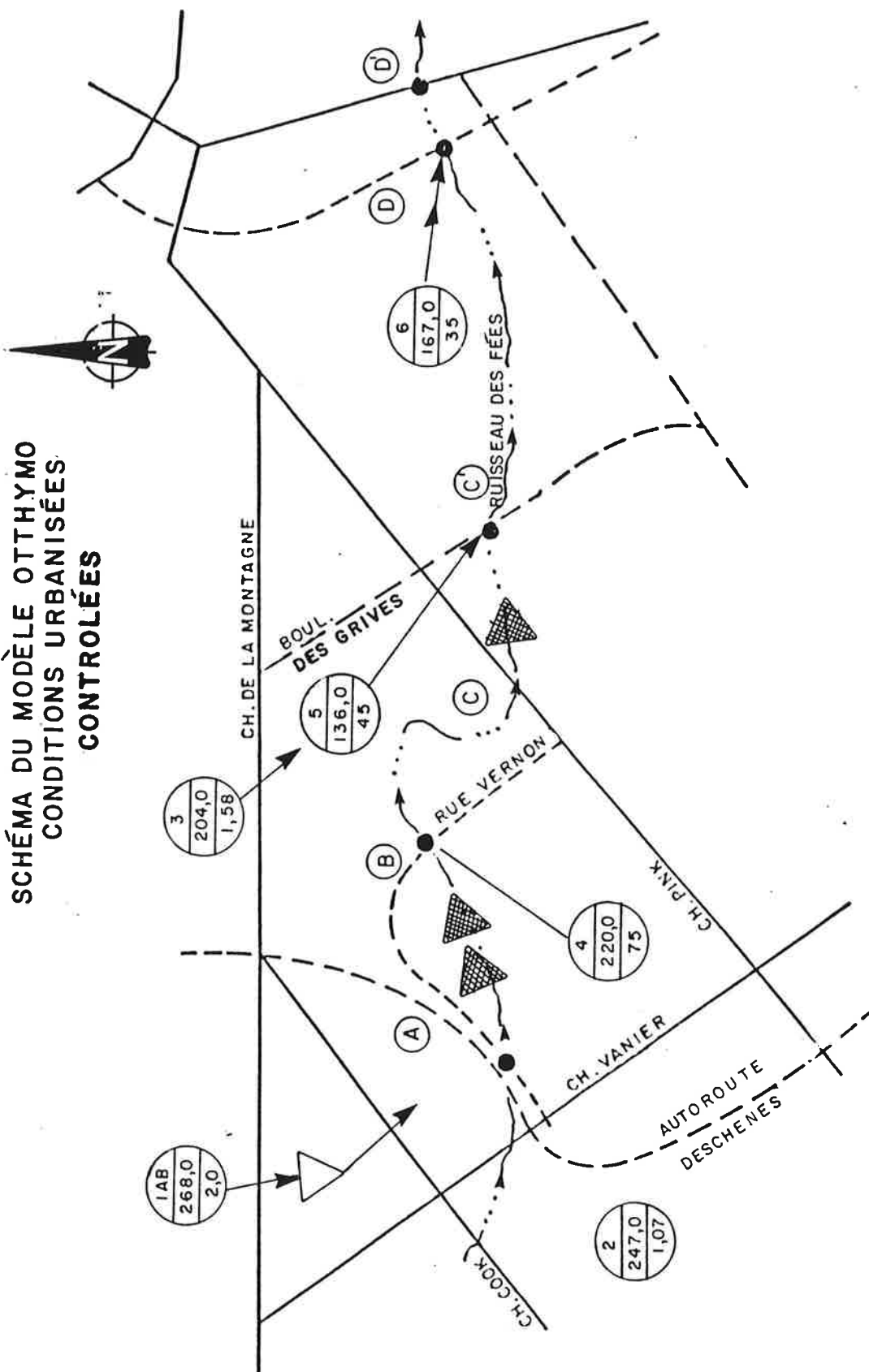
m ³ /s 100		
11	5	ANS
11	2	

DESSINÉ PAR: C, V.
PRÉPARÉ PAR: *[Signature]*

LES CONSULTANTS DE L'OUTAOUAIS INC.
EXPERTS - CONSEILS
MODELE OTTHYMO

DATE: 11 / 05 / 92
ÉCHELLE:
368-013-2

**SCHEMA DU MODELE OTTHYMO
CONDITIONS URBANISEES
CONTROLEES**



LÉGENDE

- RÉSERVOIR DE RETENTION SUGGÉRÉ
- NO DU SOUS-BASSIN SUPERFICIE (Mo) Tp, (hrs) ou imp (%)
- RÉSERVOIR DE RETENTION NATUREL
- RÉSERVOIR DE RETENTION EN AMONT DU PONCEAU

m ³ /s100	ANS
11	5
11	2

ESSINÉ PAR: C, V.	LES CONSULTANTS DE L'OUTAOUAIS INC. EXPERTS-CONSEILS	DATE: 11 / 05 / 92
RÉPARÉ PAR: 		ÉCHELLE:
	MODÈLE OTTHYMO	368-013-3

DÉBIT DE POINTE POUR LES DIFFÉRENTES ORAGES CONDITIONS URBANISÉES CONTRÔLÉES



CH. DE LA MONTAGNE

BOUL. DES GRIVES

RUISSEAU DES FÉES

RUE VERNON

CH. PINK

CH. VANIER

AUTOROUTE DESCHENES

CH. COOK

VOLUME MAX. UTILISÉ
V = 6,2 ha/m

VOLUME MAX. UTILISÉ
V = 5,5 ha/m

VOLUME MAX. UTILISÉ
V = 4,7 ha/m

VOLUME MAX. UTILISÉ
V = 5,4 ha/m

VOLUME MAX. UTILISÉ
V = 1,5 ha/m

15,3
8,3
4,9

10,5
6,1
3,3

6,6
4,0
2,4

5,7
2,7
0,9

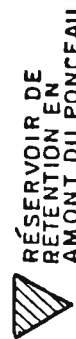
LÉGENDE



RÉSERVOIR DE RETENTION SUGGÉRÉ.



RÉSERVOIR DE RETENTION NATUREL.



RÉSERVOIR DE RETENTION EN AMONT DU PONCEAU



NO DU SOUS-BASSIN SUPERFICIE (Ha)
Tp, (hrs) OU imp(%)

m ³ /100
11
5
11
2
ANS

DESSINÉ PAR: C. V
PRÉPARÉ PAR:

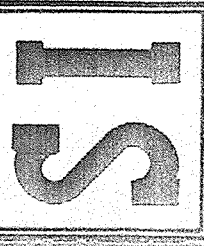
LES CONSULTANTS DE L'OUTAOUAIS INC.
EXPERTS - CONSEILS
MODÈLE OTTHYMO

DATE: 11 / 05 / 92
ÉCHELLE: —
368 - 013 - 4

LÉGENDE

- LIMITE DU BASSIN
- LIMITE DU SECTEUR À URBANISER
- SECTION VOIR PLANS 700 & 701
- LIMITE DE SOUS-BASSIN
- IDENTIFICATION DU SOUS-BASSIN
- SUPERFICIE (HECTAIRE)
- % DES SUPERFICIES IMPERMÉABLES (MOYENNE) / TEMPS DE POINTÉ (HRS)
- POINT DE CALCUL

01	01	03	MODIFIER SELON VILLE DE HULL	app.
no	date	par	révisions	
X				X: NUMÉRO D'IDENTIFICATION DU DÉTAIL
Y				Y: NUMÉRO DE LA PAGE D'OÙ LE DÉTAIL PROVIENT
Z				Z: NUMÉRO DE LA PAGE OÙ LE DÉTAIL APPARAÎT



les consultants de l'outaouais inc.
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LES DÉVELOPPEMENTS IMMOBILIERS

GAMELIN LTÉE

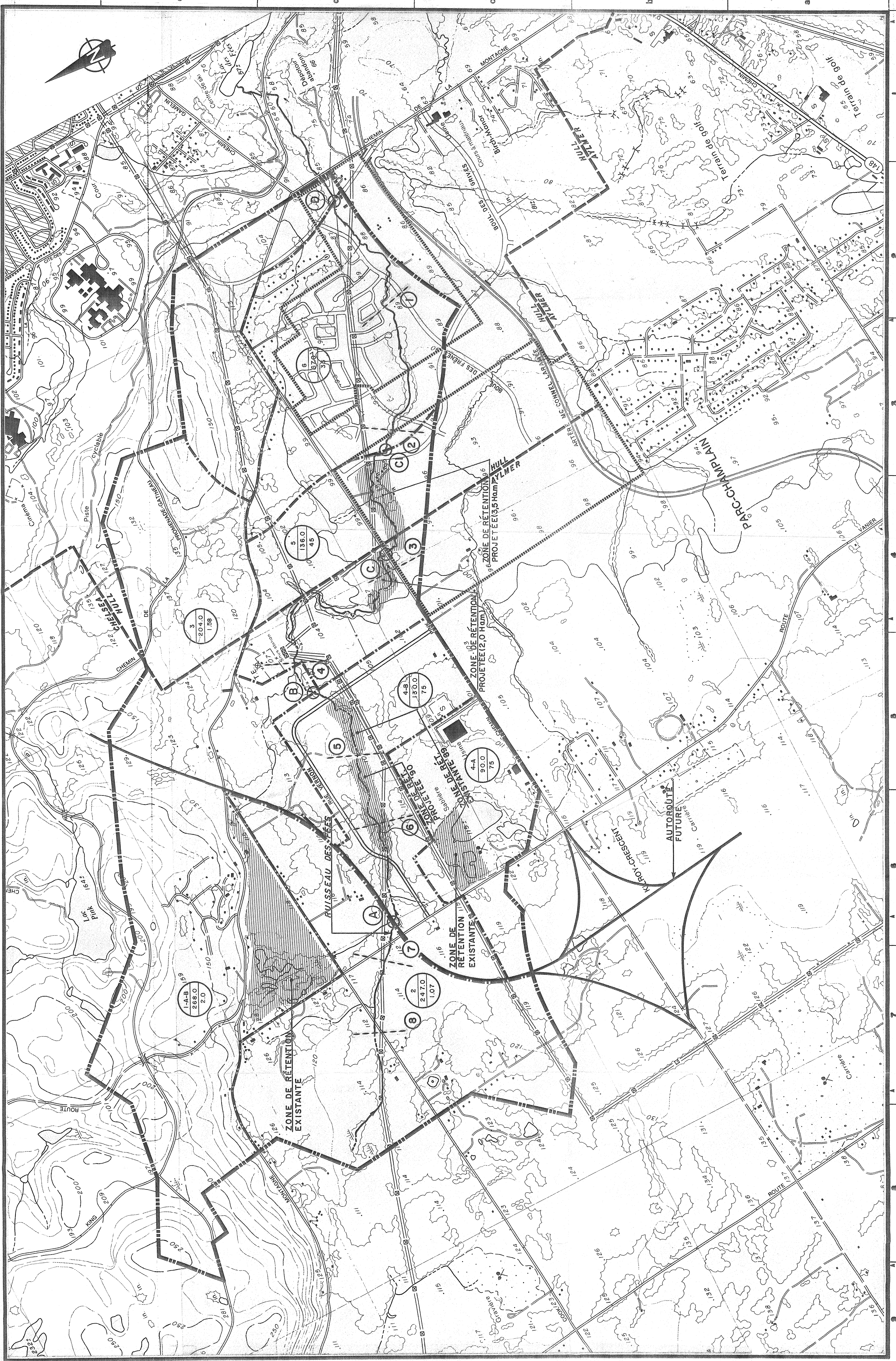
BASSIN DU RUISSEAU DES FÉES

PLAN D'ENSEMBLE

CONDITIONS URBANISÉES

projet no **368-01310101**

plan no **1010101**
rév. **01**



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K1G 3V2
OTTAWA, ONTARIO
TEL. (613) 521-2147

CONTRAT 90-11

ETUDE
DES EFFETS HYDROLOGIQUES DE
L'URBANISATION DU BASSIN
RUISSEAU DES FEES
A MULL

pour

Les Consultants de l'Outaouais



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A HULL

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Les Consultants de l'Outaouais

Fevrier 1989

CONTENU

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1. INTRODUCTION	1
2. MÉTHODES ET RÉSULTATS SANS CONTRÔLE DU RUISSELLEMENT	2
3. URBANISATION PARTIELLE ET CONTRÔLE DU RUISSELLEMENT	4
4. CONCLUSIONS	5

Annexe 1 - Modèle OTTHYMO

Annexe 2 - Résultats détaillés des simulations

1. INTRODUCTION

Le but de cette étude est de déterminer l'effet de l'urbanisation future sur les débits du ruisseau des Fées à Hull, Québec (fig. 1). L'étude est faite pour la partie du bassin située en amont de la route chemin Montagne (fig. 1), ou la surface du bassin est 1 155 ha.

L'occupation future du sol est donnée dans la figure 2 et le tableau 1 pour les sous-bassins montrés dans la figure 3B.

Ces développements ont pour effet un accroissement considérable de la surface impénétrable et par la suite à un accroissement du ruissellement. D'autre part, en vue de l'urbanisation on doit souvent augmenter la capacité du lit naturel, afin de réduire les zones inondables et afin de prévoir la profondeur requise par les égouts pluvieux. Cette modification des canaux naturels a pour résultat une réduction des temps de concentration.

L'effet combiné de l'imperméabilisation et de la réduction du temps de concentration est un accroissement des débits de pointe. Dans les dernières dix années, on a reconnu la nécessité d'examiner ces effets et d'étudier les moyens d'éviter leur effets négatifs en aval par des méthodes de "contrôle de ruissellement". Ces études sont faites dans le cadre d'un plan directeur. La ville d'Aylmer a, par exemple, des plans directeurs pour six bassins. Un plan directeur avec l'étude de 13 alternatives a été fait à Gatineau pour le bassin Moreau, etc. Les nouveaux critères de drainage d'Ontario demandent un plan directeur avant tout développement.

L'étude présente pour le ruisseau des Fées est basée sur des données limitées et étudie un nombre réduit d'options. Elle peut être considérée toutefois comme un plan directeur préliminaire. Son objectif est surtout

de présenter les aspects liés à l'étude du secteur aval proposé pour un développement résidentiel.

2. MÉTHODES ET RÉSULTATS SANS CONTRÔLE DU RUISSELLEMENT

Les débits sont simulés avec le modèle OTTHYMO qui a été aussi utilisé à Aylmer et Gatineau (annexe 1). OTTHYMO (Modèle Hydrologique de l'Université d'Ottawa) permet d'obtenir des hydrogrammes pour différents sous-bassins. Ces hydrogrammes sont acheminés dans le ruisseau et additionnés aux point critique. Le modèle a été vérifié sur de nombreux bassins ruraux et urbains et il a été utilisé dans la plupart des plans directeurs d'Ontario, ou il est recommandé par les nouveaux critères de drainage établis par cette province, ainsi que par la ville de Laval, Montréal Est, etc. La division en sous-bassins est montrée dans les figures 3A pour la situation présente et 3B pour la situation future (urbanisation). Les coefficients de ruissellement ont été choisis après des discussions avec Les Consultants de l'Outaouais qui ont étudié sur le terrain la nature des sols.

Le modèle utilise des "pluies de projet" déterminés à partir des courbes intensité-durée-fréquence ou des orages "historiques" qui ont causé des dégats dans la région. Les orages utilisés dans cette étude sont les mêmes que dans les plans directeurs d'Aylmer et ils sont montrés dans la figure 4.

Les résultats sont des hydrogrammes avec lesquels on peut déterminer les volumes de stockage pour les réservoirs pluviaux. Pour nos objectifs il est surtout intéressant de comparer les débits de pointe avant et après l'urbanisation totale du bassin qui sont donnés dans le tableau 2.

On peut observer un accroissement considérable des débits. Dans la zone résidentielle et à la sortie du bassin, le débit de 100 ans augmente de $47 \text{ m}^3/\text{s}$ à $82,4 \text{ m}^3/\text{s}$. Cette augmentation est en partie causée par le coefficient de débit relativement réduit dans les conditions rurales, à cause des zones sableuses. (Des calculs préliminaires ont indiqué que pour un sol argileux le débit de 100 ans serait $30,6 \text{ m}^3/\text{s}$.) Les résultats pour différents temps de retour sont montrés dans le tableau 2.

Il faut remarquer que sans des mesures de débits pour calibrer le modèle les débits ruraux donnent une ordre de grandeur. Par contre les débits après urbanisation qui sont nécessaire pour la détermination des niveaux sont plus précis (étant donné que l'effet des pertes par infiltration est moins important).

Des accroissements des débits obtenus dans le tableau 2, où la comparaison est faite pour des pluies torrentielles sont plus critiques pour les effets de l'urbanisation que pour les fontes de neige.

Pour un certain débit on doit déterminer les niveaux avec l'aide d'un modèle de calculs des niveaux en régime non-uniforme (calcul de remous) tel que HEC-2. Pour une analyse préliminaire on a utilisé la formule de Manning (écoulement normal). On obtient dans la zone résidentielle aval les niveaux montrés dans la figure 7.

La figure 9 montre d'une manière approximative les niveaux amont du ponçon existant sous le chemin La Montagne. Ce ponçon a une capacité limitée et pour des débits très rare, la route sera déversée.

La capacité du nouveau ponçon en construction sous la nouvelle route est environ $16,6 \text{ m}^3/\text{s}$ (soit environ pour un période de retour de 100 ans).

Le ponçon a un diamètre de 2 100 mm, un peu plus grand que celui du ponçon existant qui a un diamètre de 1 820 mm. Les niveaux créés par le ponçon aval peuvent noyer le nouveau ponçon amont. Pour le débit de 100 ans, on trouve aussi une possibilité d'un déversement dans le bassin du ruisseau situé au sud dans la zone de la propriété de l'Institut de recherche du Ministère de l'agriculture.

Le projet de développement doit évidemment assurer la protection contre l'inondation pour une période de retour de 100 ans par des solutions telles que des canalisations digues ou remblais. Un calcul de remous sera donc nécessaire pour la phase finale du projet. Tenant compte des conditions présentes, le contrôle du ruissellement est très important.

3. URBANISATION PARTIELLE ET CONTRÔLE DU RUISSellement

La tableau 3 donne les résultats pour trois scénarios étudiés pour les conditions futures (voir schémas dans les figures 8A, 8B, 8C).

- α Développement limité à la zone résidentielle du secteur aval (sans réservoir pluvial);
- β Développement du bassin entier avec des réservoirs pluviaux dans tous les développements;
- γ Développement du bassin entier avec des réservoirs pluviaux dans le secteur amont de la zone industrielle.

Le "réservoir pluvial" peut avoir différentes solutions pratiques telles que stockage dans les parcs, stationnements, toits, etc. Le choix nécessite données additionnelles, discussions avec la ville, etc. Pour cette étude on donne seulement les volumes. La surface approximative peut être déterminée pour une profondeur moyenne de 1,5 ÷ 2 m.

Dans le scénario α l'accroissement du débit de 100 ans est environ 100 % au lieu de 300 % pour le développement total sans contrôle du ruissellement.

Dans le scénario β le débit pour chaque zone est réduit par des réservoirs à la valeur des conditions présentes. On voit dans le tableau 3 que le débit à la sortie de la zone développée est un peu plus grand que dans les conditions présentes. La différence pour le débit de 100 est toutefois de moins de 10 %. Il est toutefois distribué sur une durée plus grande, donc l'effet d'érosion aval peut être tout de même accru.

Les volumes des réservoirs pluviaux ont les valeurs suivantes:

Bassin résidentiel aval	58 800 m ³
Bassin amont du chemin Pink	296 000 m ³ .

Dans le scénario γ on a vérifié la possibilité du contrôle de ruissellement seulement pour la partie amont du bassin. On trouve tel que montré dans le tableau 3 que l'accroissement de débit est de 60 %, ce qui n'est pas acceptable.

4. CONCLUSIONS

Tenant compte de l'accroissement considérable des débits causé dans le cas d'une urbanisation totale du bassin du ruisseau des Fées, il est nécessaire de prévoir un programme de contrôle du ruissellement.

Si la ville de Hull accepte le principe du contrôle du ruissellement, on peut utiliser le modèle développé pour les bassins pour un calcul détaillé des storages.

L'étude préliminaire montre que le storage peut être étagé en commençant avec 50 800 m³ dans la zone résidentielle.

L'effet d'érosion du secteur avant demande des études supplémentaires. On peut toutefois considérer que le contrôle des érosions peut conduire à accroissement des volumes indiqués pour le contrôle des débits de pointe. Un accroissement des volumes de 25 % est possible.

Paul Wisner, ingénieur, PhD



Peter Spal, hydrologiste

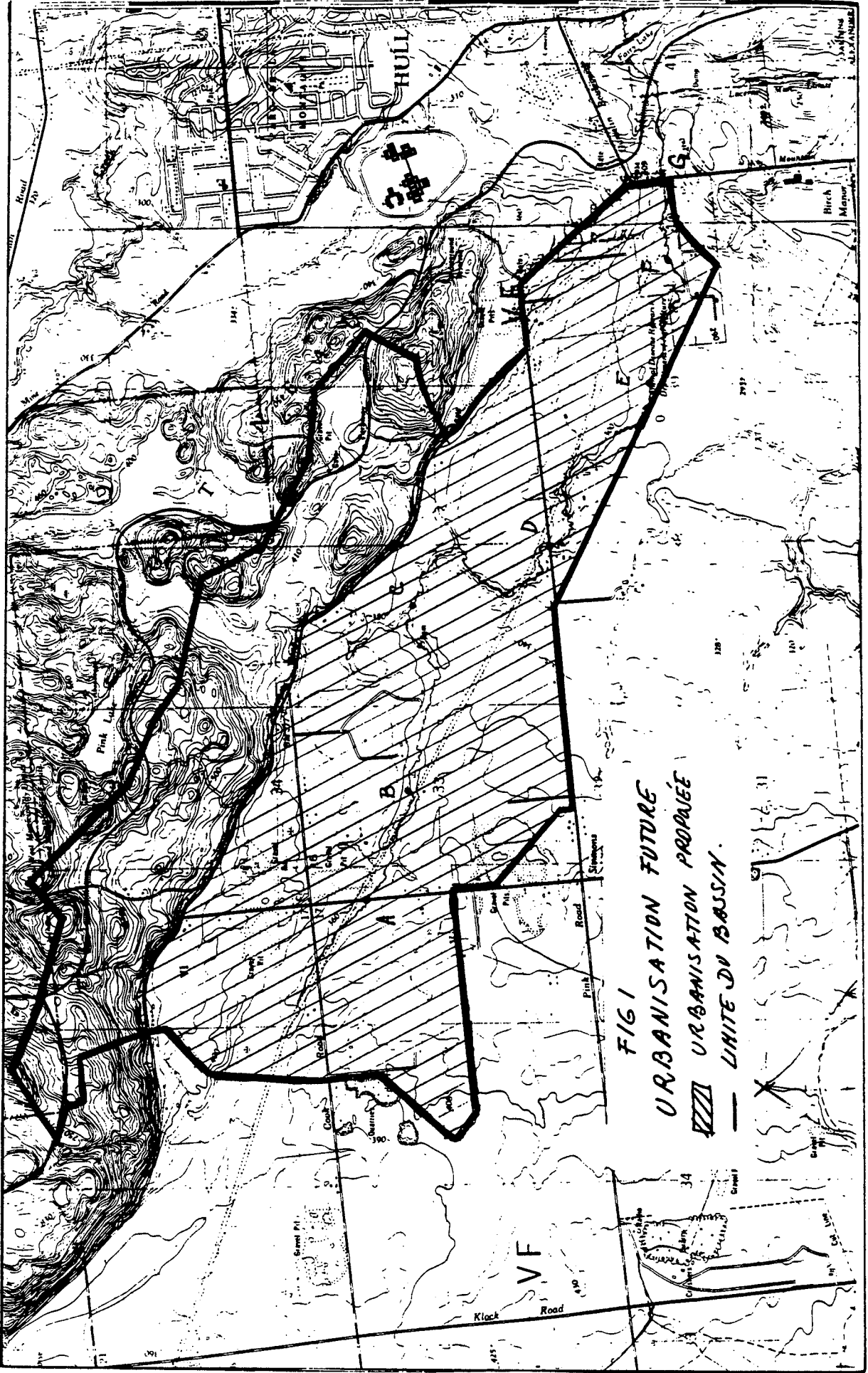


Tableau 1 Occupation du Sol			
Sous Bassin	Surface (ha)	Type	Imperméabilité
2A	230	Res. 36 per./ac	36 %
2B	23	Res. 36 per./ac	36 %
4A	98	Ind.	75 %
4B	269	Ind.	75 %
7A	62.5	Res. 54 per./ac	45 %
7B	77.8	Res. 54 per./ac	45 %
7C	45.5	36 per./ac	30 %

Tableau 2 Effet de l'urbanisation sans contrôle du ruissellement				
Section du Ruisseau	Débit 5 ans (mcs)		Débit 100 ans (mcs)	
	Présent	Futures	Présent	Futures
B	2.7	29.6	5.4	54.7
D	6.2	52.0	12.9	95.0
G	7.2	45.6	14.7	82.4

Tableau 3 Débit avec contrôle du ruissellement								
Section	5 Ans (mcs)				100 Ans (mcs)			
	Présent	α	β	γ	Présent	α	β	γ
A			20.2	20.2			38.6	38.6
B	2.7	2.7	29.6	29.6	5.4	5.4	54.7	54.7
C			49.2	49.2			89.0	89.0
			52.0*	52.0*			95.0*	95.0*
D	6.2	6.2	7.6	7.6	12.9	12.9	13.0	13.0
E		6.8		8.0		13.9		13.2
F		12.0		12.6		22.5		23.1
G	7.2	11.5	9.3	11.8	14.7	23.5	15.9	24.0

*Débit d'entrée dans le reservoir



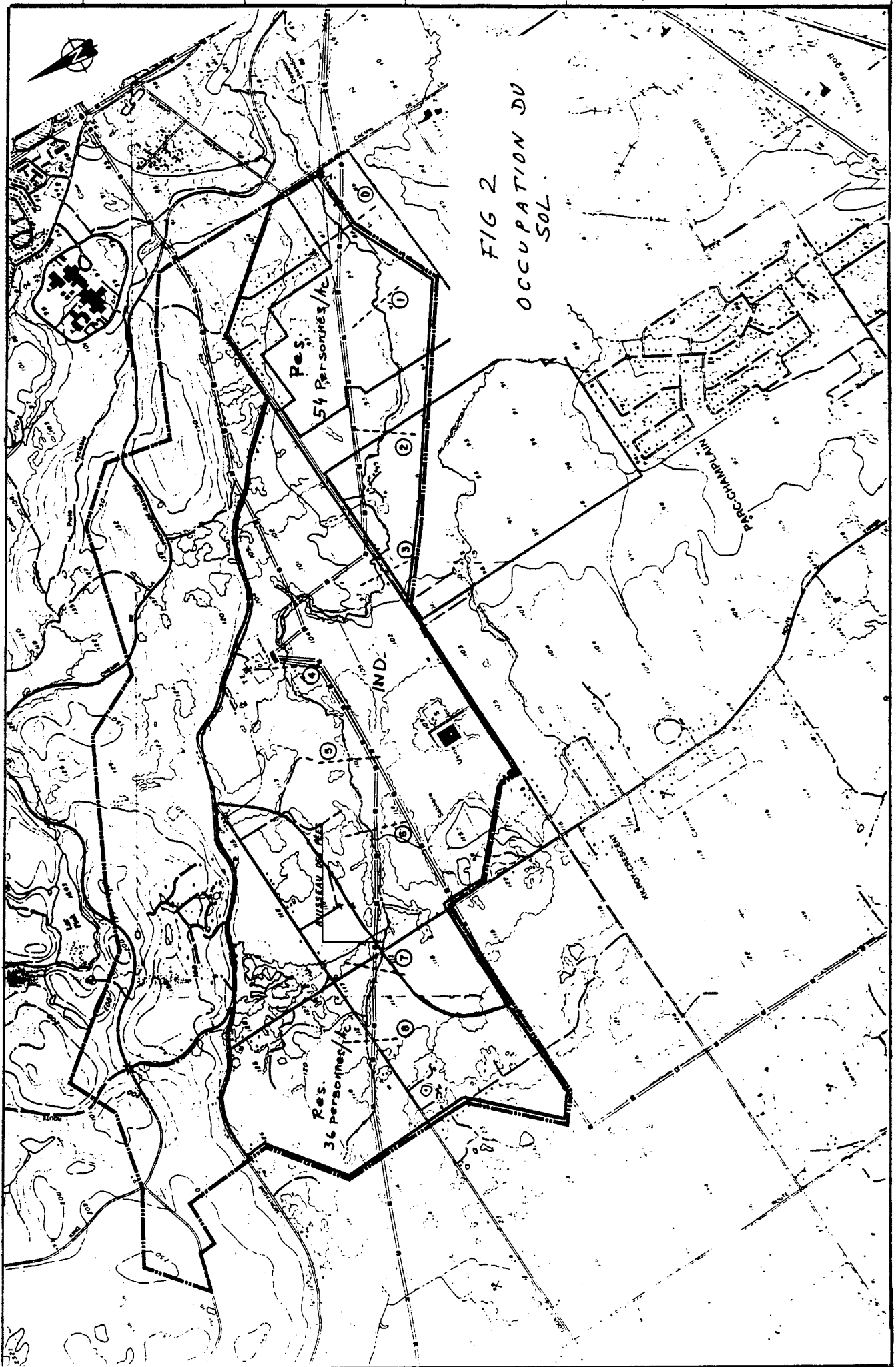


FIG 2
OCCUPATION DU
SOL.

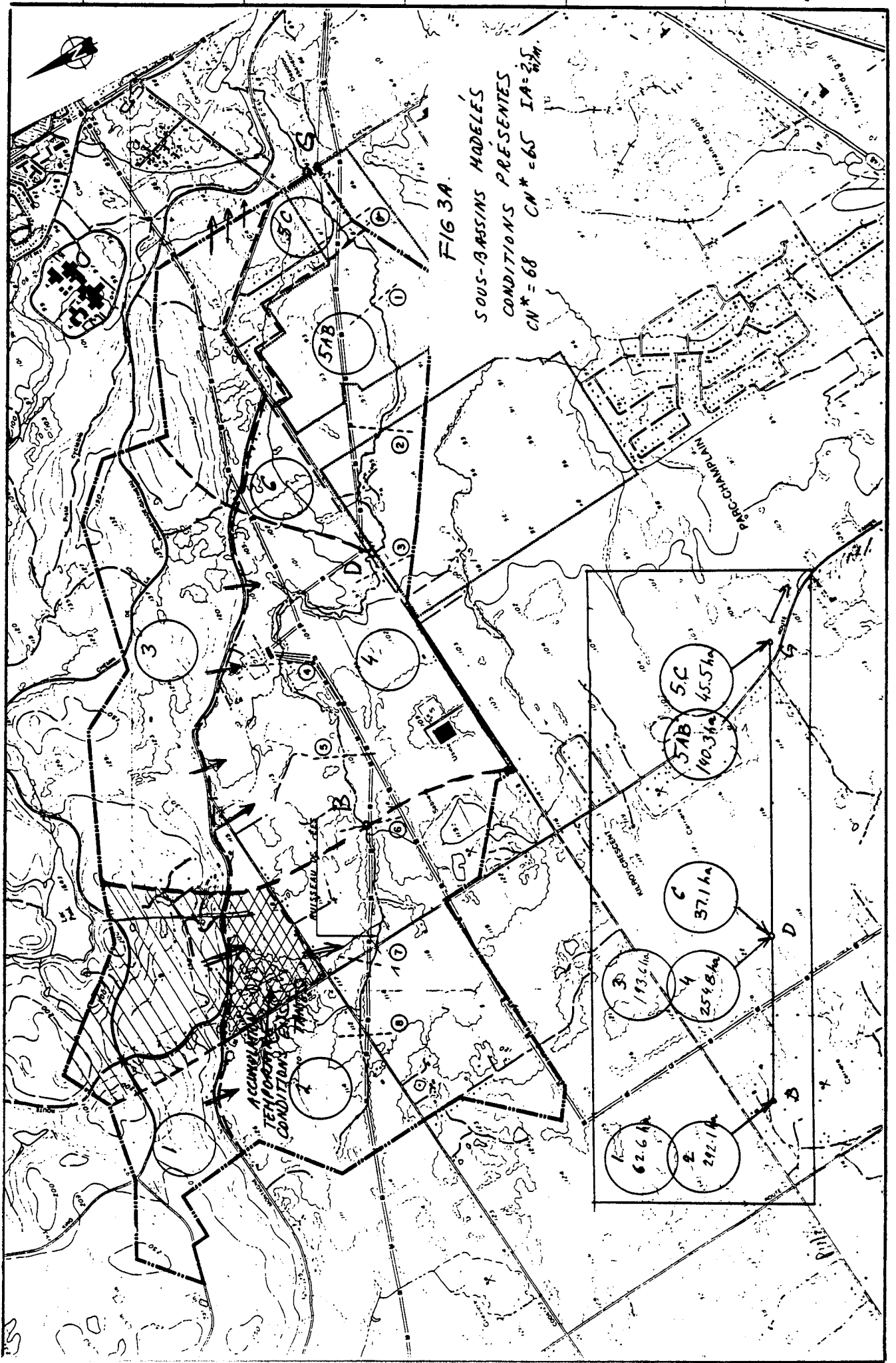
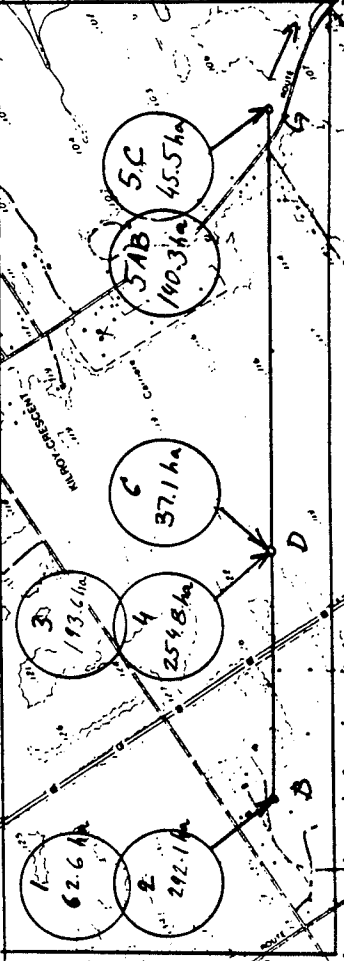


FIG 3A

SOUS-BASSINS MODELES
 CONDITIONS PRESENTES
 CN* = 68 CN* = 65 IA = 25
 1/10000

ACCUMULATED WATER
 THERMOPHORE
 CONDITIONS



1/10000

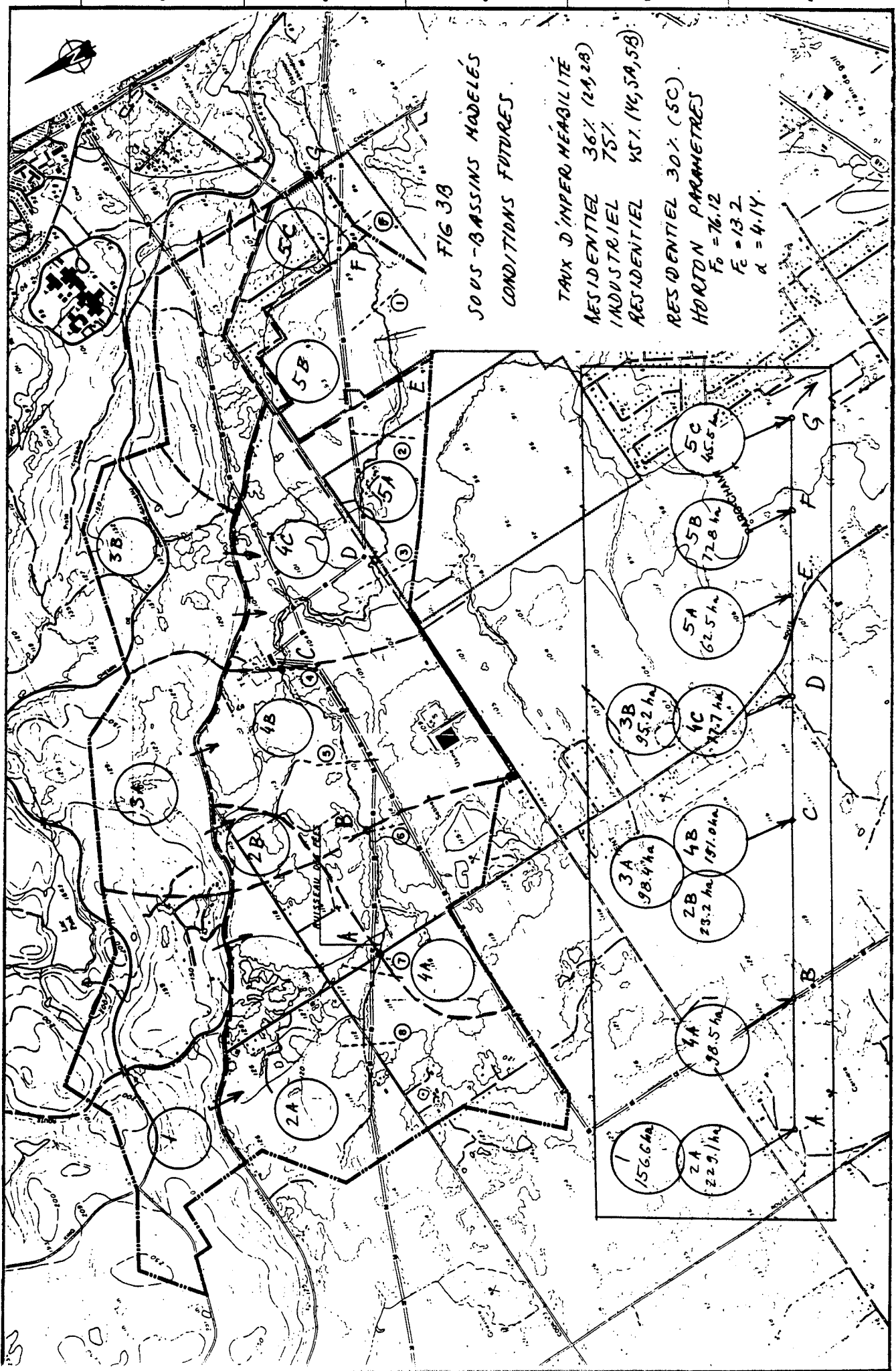


FIG 3B

SOUS-BASSINS MODELES
CONDITIONS FUTURES

TAUX D'IMPERMEABILITE
RESIDENTIEL 36% (2A, 2B)
INDUSTRIEL 75%
RESIDENTIEL 45% (4C, 5A, 5B)
RESIDENTIEL 30% (5C)
HORTON PARAMETRES
 $F_0 = 76.12$
 $F_1 = 13.2$
 $\alpha = 4.14$

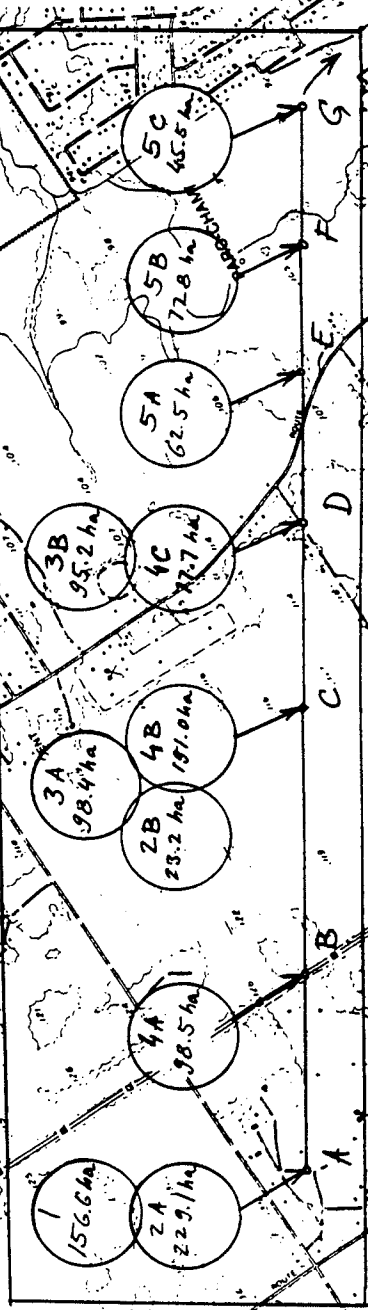
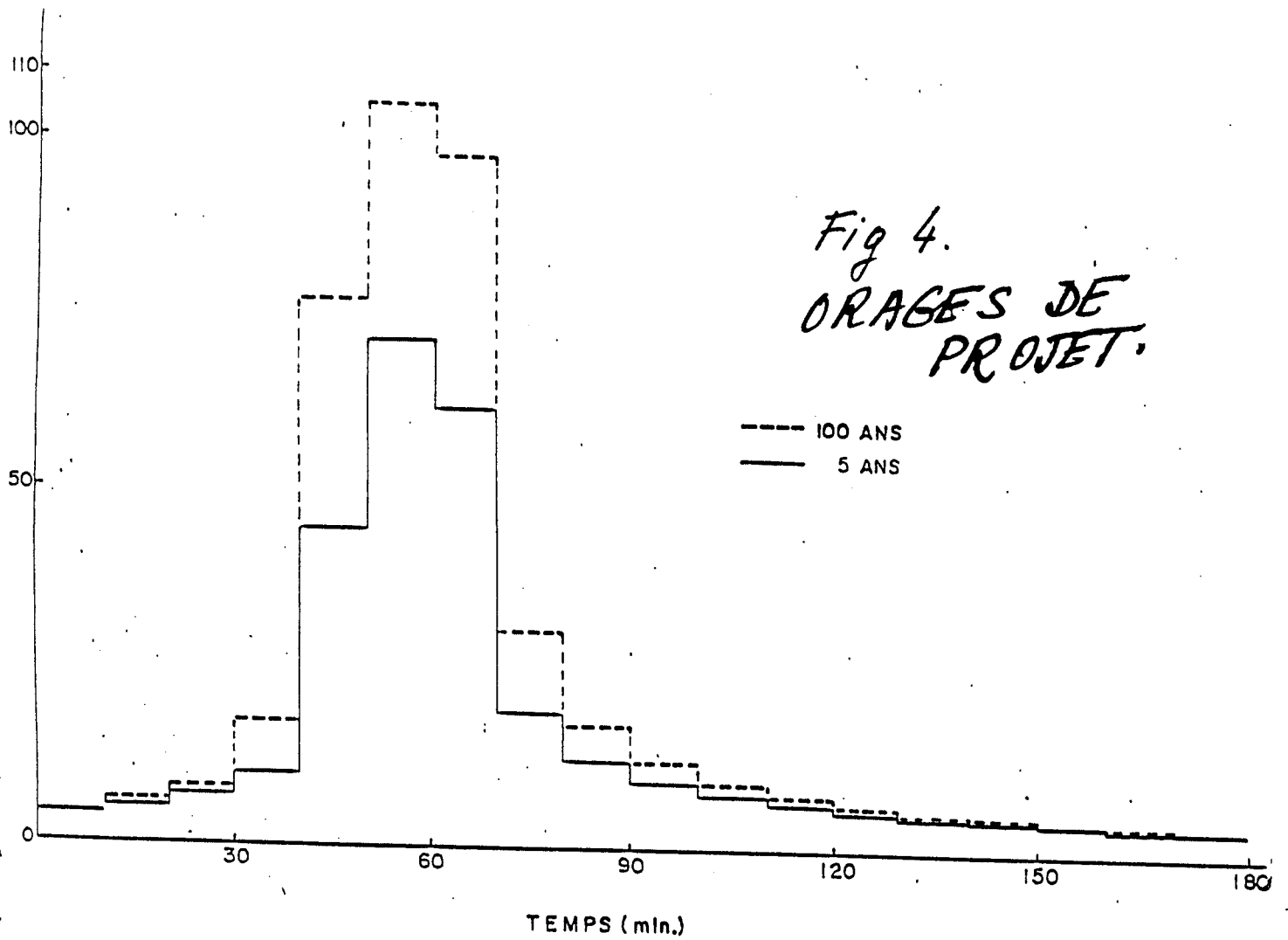


Fig 4.
ORAGES DE
PROJET.



VALEUR EN mm/hr

TEMPS/min.	5 ANS	100 ANS
10	4.23	4.92
20	5.27	6.35
30	7.07	8.95
40	11.52	18.54
50	45.05	78.42
60	72.96	107.19
70	62.52	99.64
80	19.19	31.1
90	12.59	17.51
100	9.5	12.65
110	7.67	9.05
120	6.46	8.05
130	5.59	6.81
140	4.94	5.89
150	4.44	5.2
160	4.03	4.65
170	3.7	4.21
180	3.42	3.85

FIG 5 HYDROGRAME T = 100 ANS (PRESENT)
POINT 6 (CHEMIN DE LA MONTAGNE).

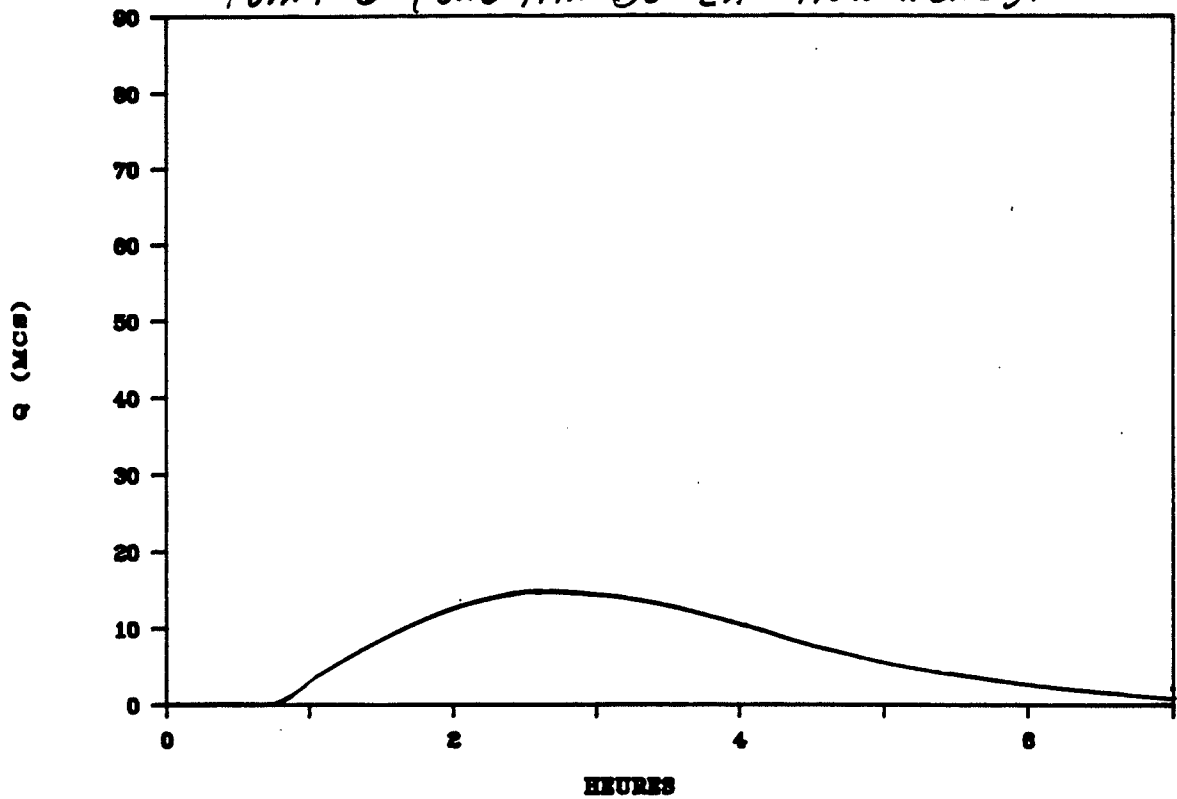
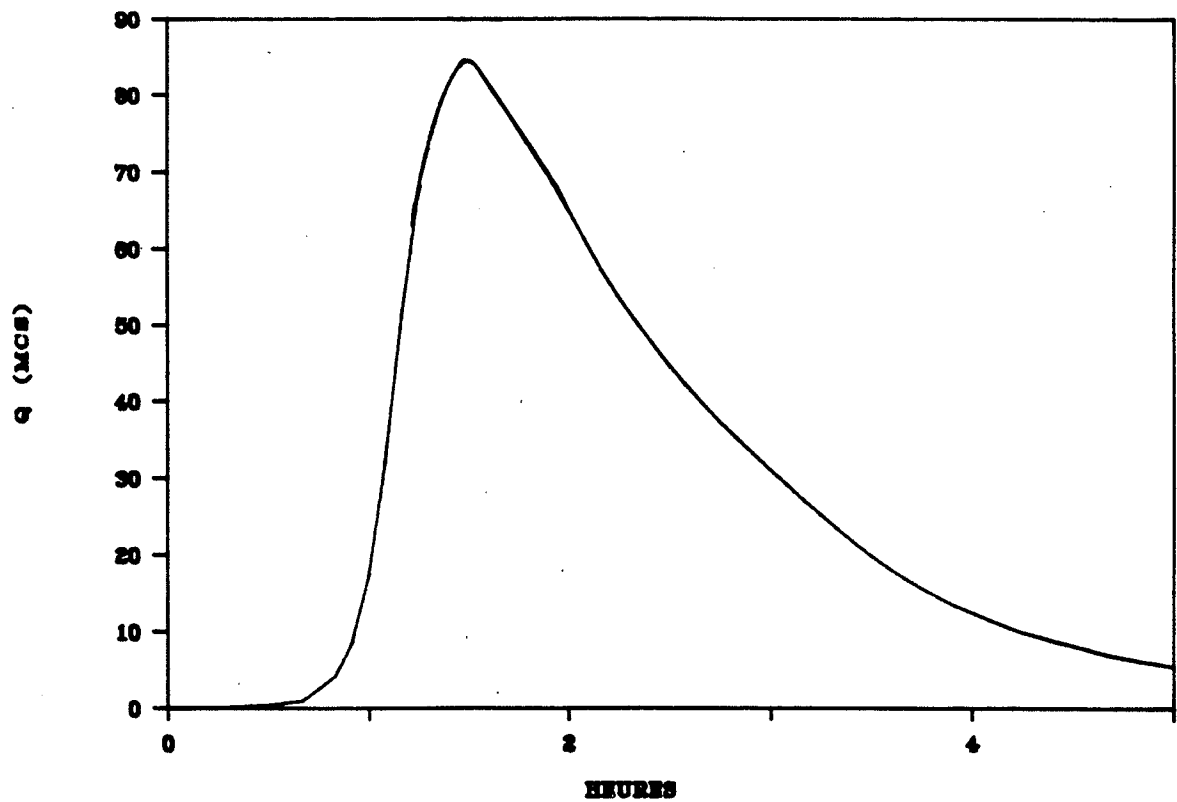
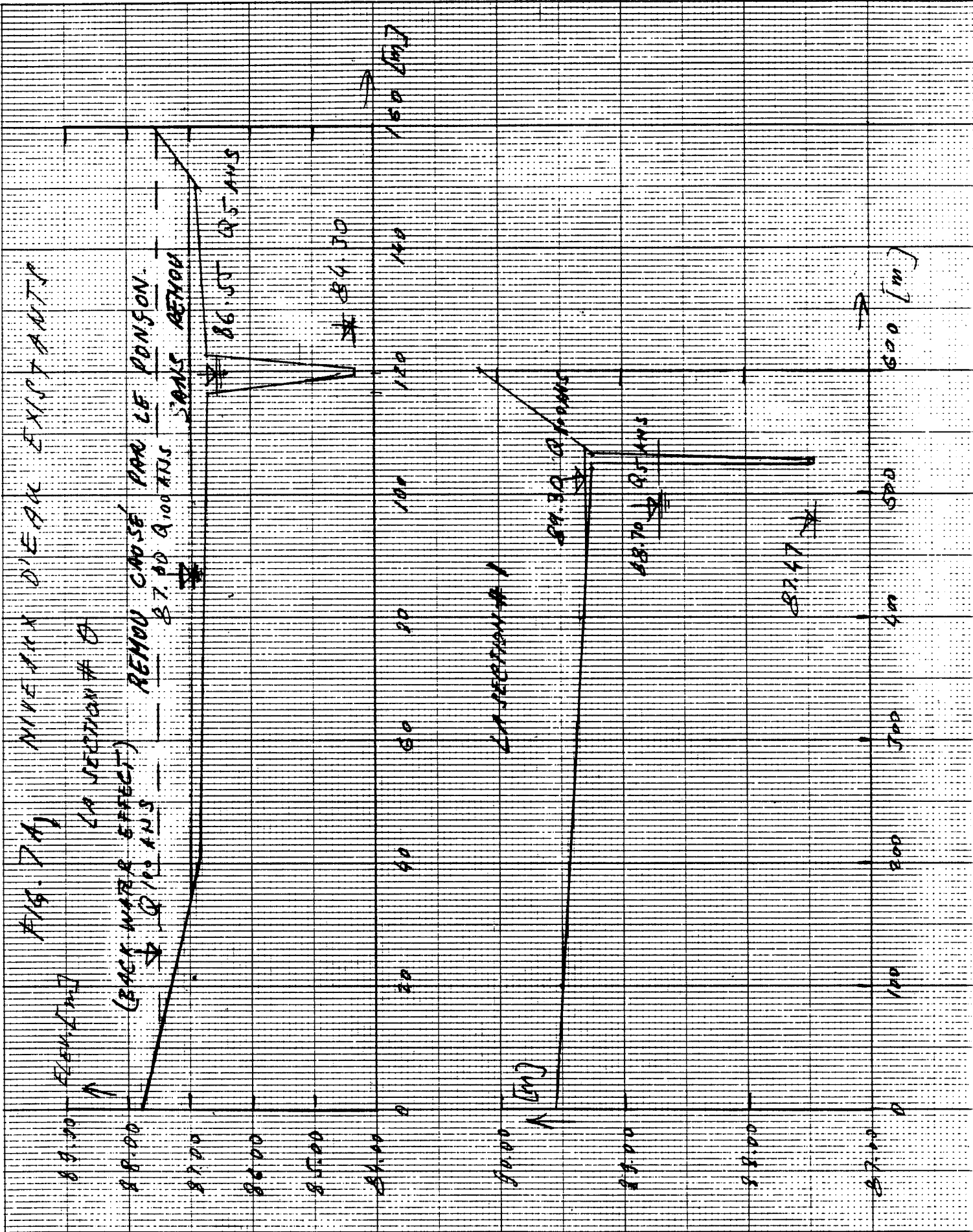


FIG 6 HYDROGRAME T = 100 ANS (FUTUR.)





les cours d'eau, canaux ou conduites est en général non-continu, non-uniforme et ne peut être décrit qu'avec l'aide des équations dynamiques complètes de mouvement et de continuité connues sous le nom d'équation de St-Venant. Une solution directe de ces équations n'est pas possible et leur résolution pour "l'acheminement hydraulique" se fait à l'aide de méthodes numériques ou par différence finie (par exemple la méthode implicite du modèle HVM-Dorsch ou celle explicite du modèle WRE-Transport) ou alors par simplification de ces équations en utilisant les différentes formes de la méthode de la cinématique des ondes. Pour "l'acheminement hydrologique" les méthodes sont dérivées des relations de stockage où le débit sortant d'un bief à un temps $(t+\Delta t)$ est une fonction linéaire du débit entrant à un temps (t) et $(t+\Delta t)$ et du débit sortant au temps (t) .

II.4.1 Acheminement par des conduites

Le modèle OTTHYMO possède une nouvelle commande appelée KINROUTE pour acheminer les hydrogrammes par des conduites. Des tests ont montré que l'acheminement par KINROUTE donne des résultats proches de ceux obtenus par des modèles dynamiques plus complets de systèmes de drainages, ceci pour des pentes rencontrées généralement dans la pratique (Réf. no

KINROUTE est un modèle du type Cunge-Muskingum qui permet la représentation de l'atténuation des ondes. Cette méthode diffère de celles qui cherchent des solutions directes des équations cinématiques des ondes. Le système de résolution est simple et les paramètres sont fonctions des caractéristiques physiques et hydrauliques des conduites. Un des avantages sur les solutions numériques est qu'il est possible de faire varier les paramètres du modèle (en particulier la vitesse de l'onde) avec la variation du débit.

Le modèle utilise la relation de la cinématique des ondes dans la forme:

$$\frac{1}{C} \frac{\partial Q}{\partial t} + \frac{\partial Q}{\partial X} = 0$$

Fig. 8A ALTERNATIVE α

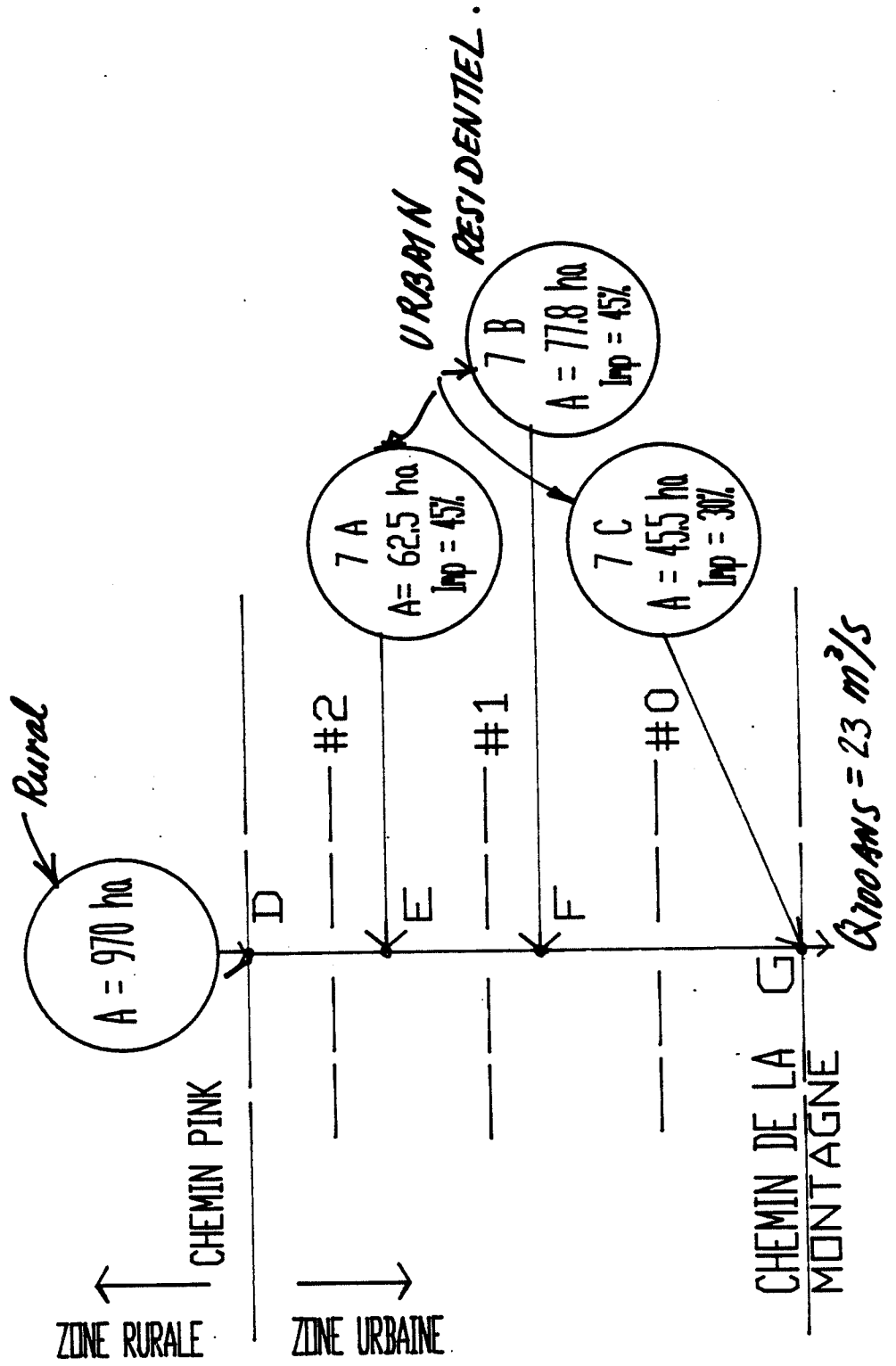


Fig. 8B. ALTERNATIVE β

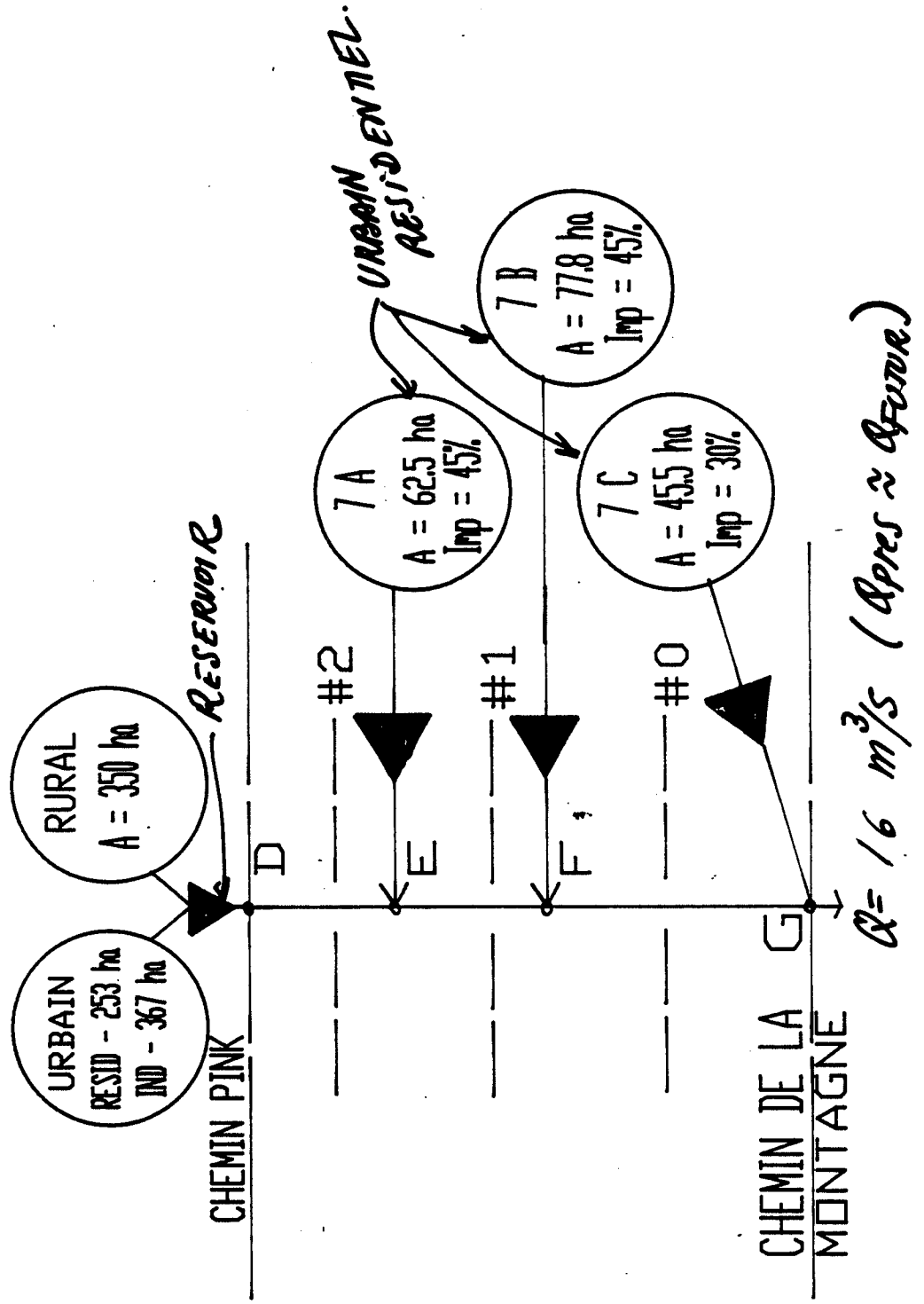
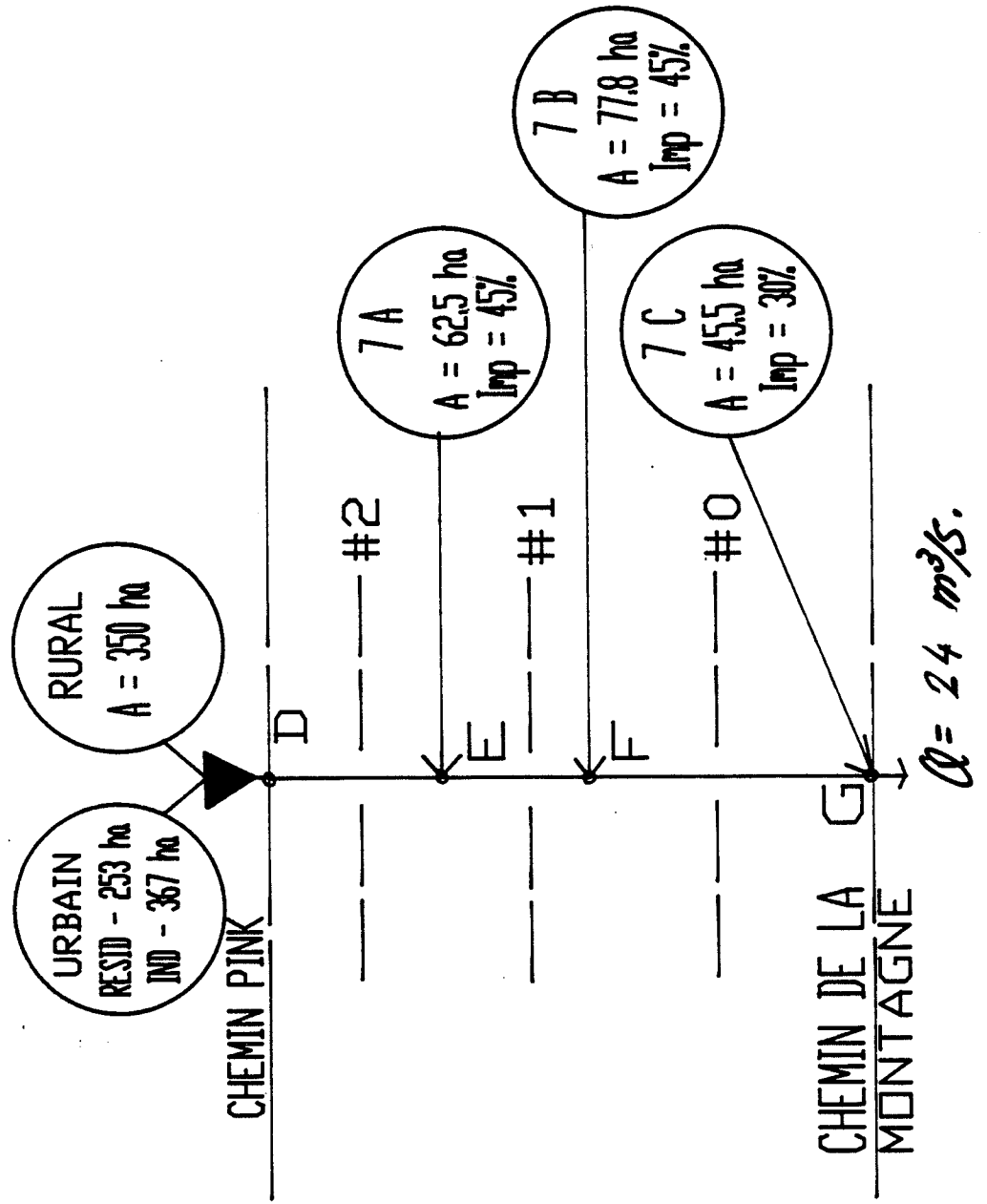


Fig. 8C. ALTERNATIVE 2



ANNEXE 1

Modèle OTTHYMO
Modèle Hydrologique de
L'Univeristé Ottawa

I PRESENTATION D'OTTHYMO

Les modifications apportées au modèle Hymo ont été effectuées afin d'adapter ce modèle aux études de systèmes de drainage et aux simulations des hydrogrammes des bassins-versants en partie urbanisées.

Les compléments principaux apportés à HYMO sont les sous-programmes:

COMPUTE URBHYD pour la simulation des surfaces urbanisées en tenant compte des différentes réponses des zones imperméables et perméables.

KINROUTE pour acheminer les hydrogrammes, par la méthode de la cinématique des ondes, dans les conduites et déterminer leurs diamètres.

Le modèle possède d'autres modifications, incluant un programme pour l'écoulement un milieu rural basé sur le modèle de Nash (COMPUTE NASHYD) et une amélioration de la procédure pour le calcul des pertes par infiltration. En outre, OTTHYMO peut être utilisé soit en unités anglaises soit en unités métriques.

Les principes d'utilisation d'OTTHYMO sont les mêmes que ceux de HYMO. Dans une application typique, OTTHYMO simule les hydrogrammes pour chaque sous-bassin, achemine les hydrogrammes par un cours d'eau ou une conduite et les additionne à l'aval.

Le programme calcule de l'amont vers l'aval en utilisant les ouvrages de drainage, (conduites ou canaux) jusqu'à l'exutoire. Il est également possible d'acheminer les hydrogrammes par des réservoirs dans le but d'une étude du contrôle de l'écoulement. Les principes de base d'OTTHYMO seront mieux illustrés par un simple exemple (exemple 1).

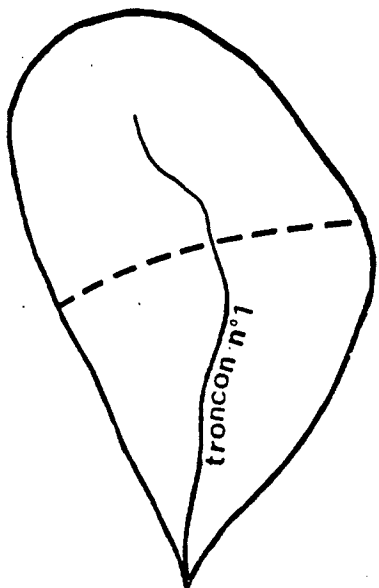
Il y a trois types d'opérations:

- a) les opérations d'exécutions pour ajouter, imprimer, dessiner les hydrogrammes
- b) les opérations de simulation des hydrogrammes pour chaque sous-bassin
- c) l'acheminement par des cours d'eau, conduites ou réservoirs.

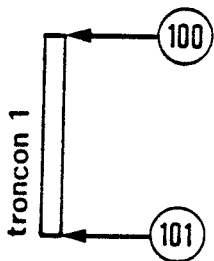
Chacune de ces opérations s'effectue à l'aide d'une "commande" indiquant le sous-programme à utiliser. L'utilisateur spécifie la commande et les autres données comme entrée, dans un certain ordre, mais avec format libre. Les hydrogrammes calculés et la description des tronçons du cours d'eau sont chacun identifiés par un identificateur "ID" pour le stockage, temporaire, en mémoire. Le programme accepte 6 "ID" à la fois pour les hydrogrammes. Malgré cette limitation en réutilisant ceux-ci, il est possible de faire une simulation avec un grand nombre de sous-bassins.

Exemple n° 1

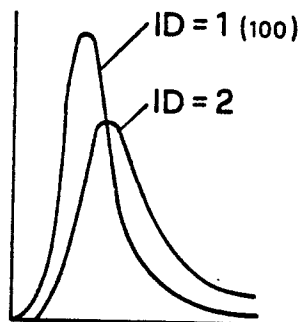
principe de bases de l'utilisation de OTTHYMO



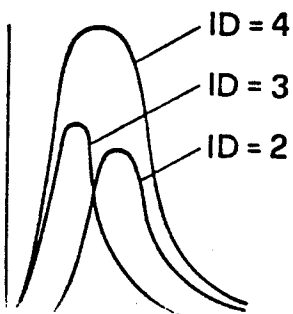
1. Calcul de l'hydrogramme pour le sous-bassin 100 (et lui donner une identité: ID = 1)
(commande COMPUTE NASHYD et COMPUTE HYD)



2. Acheminer l'hydrogramme (ID = 1) par le canal (tronçon n° 1). L'hydrogramme acheminé est modifié et reçoit une nouvelle identité (ID = 2)
(commande ROUTE associée avec COMPUTE RATING CURVE et COMPUTE TRAVEL TIME ou commande KINROUTE pour les conduites)



3. Calcul de l'hydrogramme du sous-bassin 101 (et lui donner une identité; ID = 3)
(commande COMPUTE URBHYD)



4. Faire la somme des hydrogrammes ID = 2 et ID = 3 et donner une nouvelle identité à l'hydrogramme résultant (ID = 4)
(commande ADDHYD)

II PROCEDURES HYDROLOGIQUES UTILISEES PAR OTTHYMO

Ce chapitre décrit brièvement la procédure de calcul pour la simulation des hydrogrammes et leur acheminement par une rivière ou dans un réservoir. Des précisions au sujet de ces procédures figurent au chapitre IV.

II.1 Rappel des principes de base de la simulation des hydrogrammes

Chaque sous-programme calculant un hydrogramme est composé de deux sous-modèles.

1. Un premier sous-modèle qui calcule les pertes totales de la précipitation en tenant compte de la rétention initiale ou du stockage dans les dépressions de surface de même que de l'infiltration.
2. Un deuxième sous-modèle qui transforme la pluie nette en ruissellement simulant la réponse du bassin-versant à la précipitation excédentaire.

Si la réponse instantanée du bassin-versant, c'est-à-dire l'hydrogramme unitaire instantané (HUI), est connue, l'hydrogramme peut être déterminé par intégration de l'HUI. En pratique, cette transformation est effectuée par pas de temps fini. Celui-ci ne doit pas être plus grand que le cinquième, environ, du temps de concentration.

Dans un modèle conceptuel, la forme de l'HUI est définie par une équation mathématique. Le modèle conceptuel le plus simple fait l'hypothèse d'un bassin-versant se comportant comme un "réservoir linéaire" dans lequel le stockage S est directement proportionnel au débit sortant Q . ($S = K Q$). Un tel modèle possède un unique paramètre K qui est le coefficient de stockage du réservoir linéaire. D'autres modèles, tel que celui proposé par Nash (1957), sont composés d'une cascade de n réservoirs, linéaires et égaux, et ont 2 paramètres. Il est possible d'augmenter le degré de liberté en utilisant des modèles conceptuels composés de cascades de réservoirs en parallèles tels que ceux proposés par Wittenberg (1975) et

Diskin (1978). Il existe donc de nombreux modèles conceptuels linéaires utilisant diverses combinaisons de réservoirs (Dodge, 1973). Des modèles non-linéaires qui tiennent compte de la non-linéarité de la réponse du bassin-versant existent également (Ding, 1974). Deux facteurs principaux doivent être pris en compte pour la conception d'un modèle opérationnel.

1. Le nombre minimum de paramètre à calibrer.
2. La possibilité de simuler une surface urbanisée d'une façon détaillée.

II.2 Simulation de l'hydrogramme pour des bassins ruraux

Les commandes COMPUTE NASHYD et COMPUTE HYD sont utilisées pour la simulation des bassins ruraux.

II.2.1 COMPUTE NASHYD

Cette commande utilise la procédure modifiée du CN pour calculer les pertes et le modèle de Nash (1957) pour calculer l'hydrogramme unitaire. Le modèle de Nash est un modèle conceptuel utilisant une cascade de n réservoirs linéaires. On peut montrer que le débit à la sortie du dernier réservoir au temps t est:

$$q(t) = \frac{1}{K_n \Gamma(n)} e^{-t/K_n} (t/K_n)^{n-1}$$

- où $\Gamma(n)$ est la fonction gamma
n le nombre de réservoirs
 K_n le coefficient de stockage de chaque réservoir.

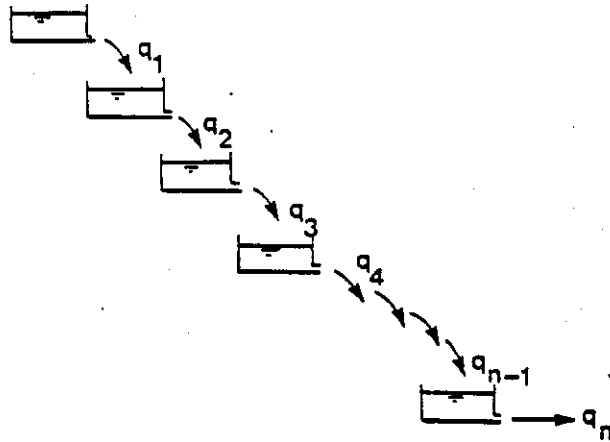


Fig. 2.1 : Cascade de réservoirs linéaires (Nash, 1957)

Cette relation est utilisée pour définir la forme de l'hydrogramme unitaire instantané (HUI). Pour $dq/dt = 0$, le débit étant maximum nous trouvons que le temps de montée t_p est fonction de n et K_n .

$$t_p = (n-1)K_n$$

Le HUI peut être exprimé en un terme sans dimensions par les paramètres de l'équation de la distribution gamma:

$$q = q_p [t/t_p]^{(n-1)} e^{-(n-1)(t/t_p)}$$

Deux paramètres doivent être déterminés pour obtenir l'hydrogramme unitaire. Si n peut être déterminé, alors il ne reste qu'un seul paramètre à fixer. A partir d'un nombre limité de simulations sur des petits bassins-versants, il a été trouvé en première approximation que $n = 3$. Une discussion des valeurs de t_p est donnée en appendice B.

Le calcul des pertes par le SCS (Soil Conservation Service) a été légèrement modifié.

L'équation de transformation de la précipitation en volume ruisselé est:

$$Q = \frac{(P - I_a)^2}{P - I_a + S}$$

où Q = volume ruisselé en mm

P = précipitations totales (mm)

S = pertes potentielles totales en paramètre de stockage

I_a = pertes initiales.

Les courbes CN du SCS sont fréquemment utilisées. S est relié au CN par $CN = 25400 / (254 + S)$ (en unités métriques). La sélection du CN est basée sur 4 groupes de sols différents, A,B,C,D et sur la couverture végétale. Le sol A correspond à un sol à haut taux d'infiltration tandis que le D à un bas taux d'infiltration. Les tables permettant de fixer le CN se trouvent dans les manuels du SCS tel que le NEH-4 et le SCS TR-55.

Le modèle Hymo, ainsi que d'autres modèles, font l'hypothèse que les pertes initiales sont égales aux 20 % des pertes par stockage, $I_a = 0.2 S$, ce qui réduit le nombre de paramètre à un. Mais cette hypothèse amène quelquefois à des résultats erronés, spécialement pour des orages de courtes durées et de hautes fréquences. Le volume ruisselé calculé est beaucoup plus petit que celui observé. Une étude faite en collaboration avec l'Institut de Génie rural montre que les résultats seront meilleurs si les pertes initiales sont basées sur les observations (Jobin, 1982). Il a été proposé dans la recherche IMPSWM-IGR d'utiliser l'indice de précipitation antécédente (IPA) qui est un meilleur indicateur du stockage que les classes AMC de la méthode SCS. Les essais sur le bassin-versant suisse de la Seymaz et les bassins canadiens Etobiwke, Sawmill Creek l'ont confirmé. On déterminera les pertes initiales de la façon suivante: (Cette méthode conduira par la suite à la calibration du paramètre CN qui sera noté CN*).

Initialement, il s'agit d'analyser les débits pour savoir si oui ou non une précipitation a engendré un ruissellement. Chaque événement est reporté sur un graphe, avec en ordonnée la précipitation et l'IPA en abscisse, en distinguant si il a provoqué ou non

un ruissellement. Nous pouvons ainsi tracer une courbe séparant les différents événements. Cette courbe représente le seuil de ruissellement. Ainsi pour un état antécédent d'humidité du sol donné nous pourrions tirer une valeur qui représente la hauteur minimale de pluie qui doit précipiter avant qu'un ruissellement ne se produise. Cette valeur qui est en fait égale aux pertes initiales a été déterminée dans les bassins mentionnés plus haut comme étant plus petite que 0,2S. Cette procédure améliore largement la calibration. Ainsi, la commande COMPUTE NASHYD permet que l'on spécifie les pertes initiales.

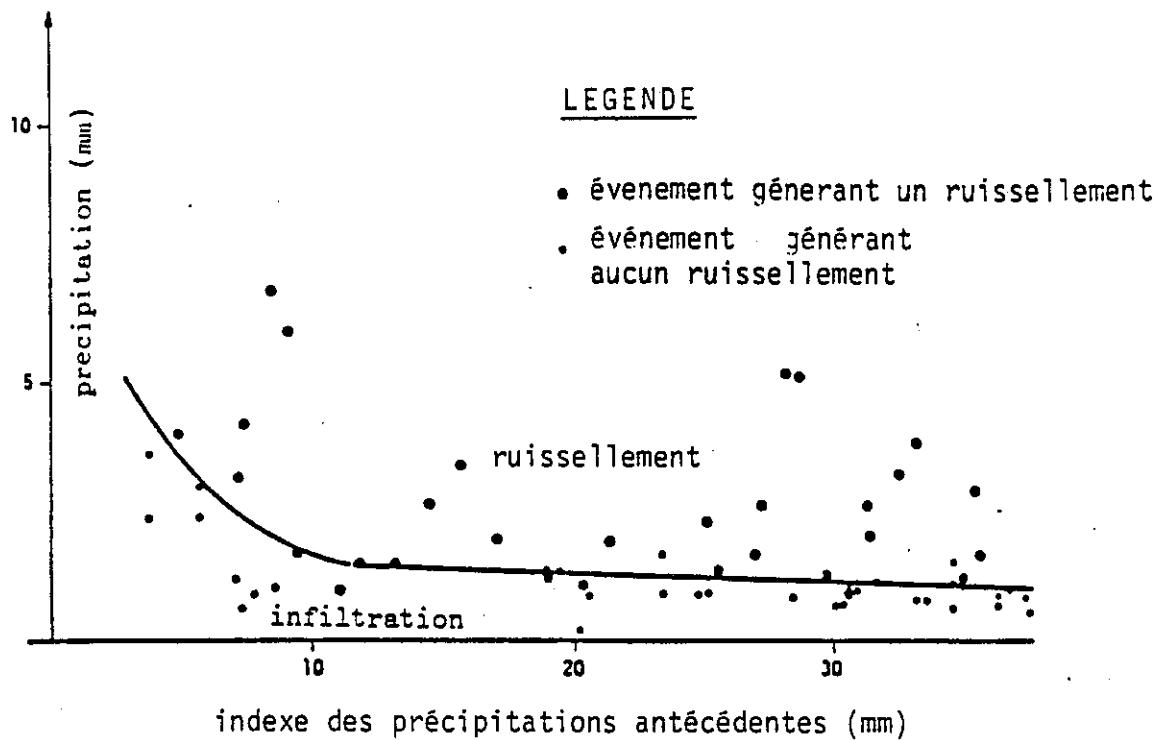


Fig. 2.2 : Seuil de ruissellement pour le bassin-versant de la Seymaz. (Réf. no

II.2.2 COMPUTE HYD

Cette commande utilisée dans le modèle original HYMO a subi quelques modifications. Les précipitations sont dorénavant introduites sous forme d'un hyétoگرامme et les pertes initiales peuvent être fixées par l'utilisateur.

L'HUI se compose de trois parties.

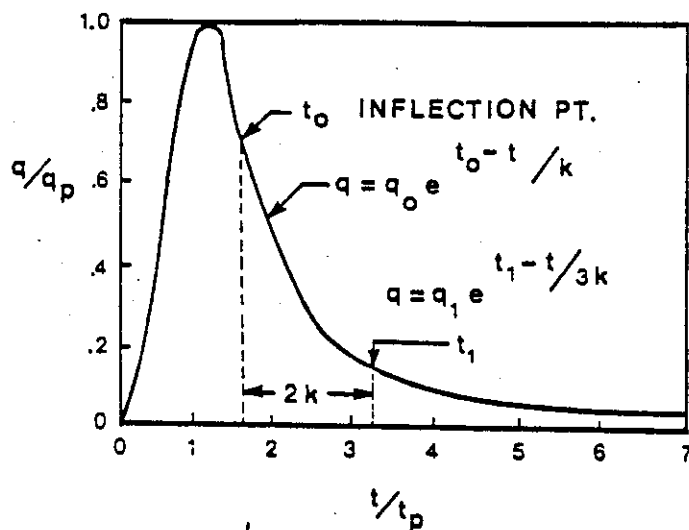


Fig. 2.3 : Hydrogramme unitaire sans dimension

La première partie, du début de la montée jusqu'au point d'inflexion, t_0 , est calculée par l'équation de la distribution gamma à 2 paramètres (éq.p. 6). Les autres équations sont sur la figure 2.3.

Le paramètre de forme sans dimension, n , est une fonction de K/t_p et q_p est une fonction de n et t_p . Ainsi, il n'y a besoin que de 2 paramètres, K et t_p , pour calculer l'HUI (le manuel d'utilisation de HYMO donne des relations empiriques pour K et t_p en fonction des caractéristiques du bassin-versant. Ces relations sont basées sur les bassins du sud des Etats-Unis et ne sont pas applicables ailleurs).

II.3 Simulation de l'hydrogramme pour des bassins urbains

II.3.1 COMPUTE URBHYD

Cette commande est utilisée pour simuler les hydrogrammes des zones urbaines. Elle fait appel à un modèle conceptuel utilisant deux réservoirs linéaires en parallèle, (fig. 2.4) pour simuler les hydrogrammes des parties perméables et imperméables du bassin-versant (P'ng, 1982).

Hydrogramme unitaire

Dans un réservoir linéaire, le stockage S est directement proportionnel au débit sortant Q .

$$S = K.Q$$

où K est le coefficient de stockage.

L'hydrogramme unitaire de durée Δt pour un réservoir linéaire peut être obtenu par les deux équations suivantes:

$$Q_p = I (1 - e^{-\Delta t/K})$$

$$Q = Q_p e^{-\zeta/K}$$

où Q_p = débit maximum de l'hydrogramme unitaire

Q = ordonnée au temps ζ

$\zeta = t - \Delta t$

I = débit entrant

Différentes relations basées sur le temps d'équilibre calculé à partir de la théorie cinématique des ondes sont utilisées pour obtenir le coefficient de stockage de deux réservoirs linéaires (ex. Neuman, 1977, Pedersen, 1980). Elles ont été testées. Ces relations font l'hypothèse que le bassin-versant peut être représenté par une surface plane. Dans OTTHYMO, le coefficient de stockage utilisé est celui de Pedersen (1980) qui est égal à la moitié du temps d'équilibre obtenu par la méthode des ondes cinématiques.

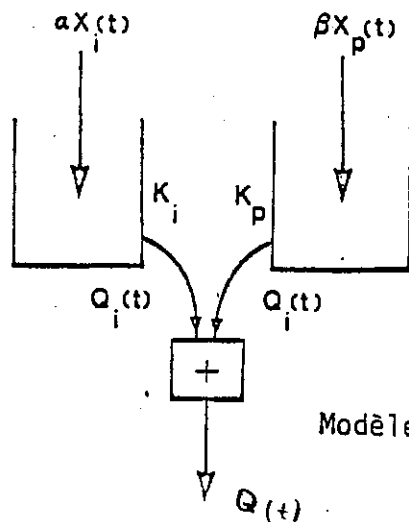


Fig. 2.4 :

Modèle de deux réservoirs parallèles

L'équation pour le coefficient de stockage est:

$$K = \frac{a L^{0.6} n^{0.6}}{i^{0.4} S^{0.3}}$$

- où K = coefficient de stockage
L = longueur de parcours du ruissellement superficiel sur le bassin-versant (m)
n = coefficient de rugosité de Manning
i = intensité maximale de la pluie nette (mm/hr)
S = pente (%)
a = coefficient

Le coefficient de stockage est différent pour les deux réservoirs linéaires afin de tenir compte des temps de réponse des parties perméables et imperméables du bassin-versant.

Volume ruisselé

La commande, à partir d'un hyétogramme d'entrée (mm/hr) calcule deux distributions de pluie nette. La pluie nette de la partie imperméable est obtenue après déduction du stockage dans les dépressions. La pluie tombant sur la surface imperméable non directement connectée est supposée tomber sur la surface perméable. Les pertes pour les surfaces perméables sont calculées en tenant compte des pertes par infiltration et des pertes par stockage dans les dépressions de surface. Il y a deux options pour calculer les pertes par infiltrations sur la surface perméable. La première option est le calcul de l'infiltration à l'aide de l'équation de Horton, la deuxième est la procédure modifiée, utilisant le CN*, discutée précédemment.

L'équation de Horton est:

$$f = f_c + (f_o - f_c)e^{-\alpha t}$$

- ou f_o = taux d'infiltration initial (mm/hr)
 f_c = taux d'infiltration final (mm/hr)
 α = facteur de décroissance

Les deux pluies nettes calculées sont alors combinées aux hydrogrammes unitaires correspondant pour donner deux hydrogrammes. Ceux-ci sont additionnés pour obtenir l'hydrogramme final du bassin-versant.

Le modèle a été vérifié par comparaison avec des simulations (SWMM) plus détaillées, ceci pour différents bassins-versants, différents taux d'imperméabilités et différentes tailles des bassins. La commande URBHYD a été employée pour des bassins-versants non-discretisés et donc sans acheminement, et les résultats comparés avec ceux obtenus avec le modèle SWMM qui utilise des bassins-versants très détaillés. La comparaison entre les différents débits de pointe est bonne.

Le modèle a également été vérifié à l'aide des mesures sur les bassins-versants Gray Haven à Baltimore, Malvern à Burlington et Fulton Drive à Edmonton. La figure 2.6 montre la comparaison entre les débits de pointes maximum simulés et mesurés. D'autres comparaisons se trouvent au chapitre IV.

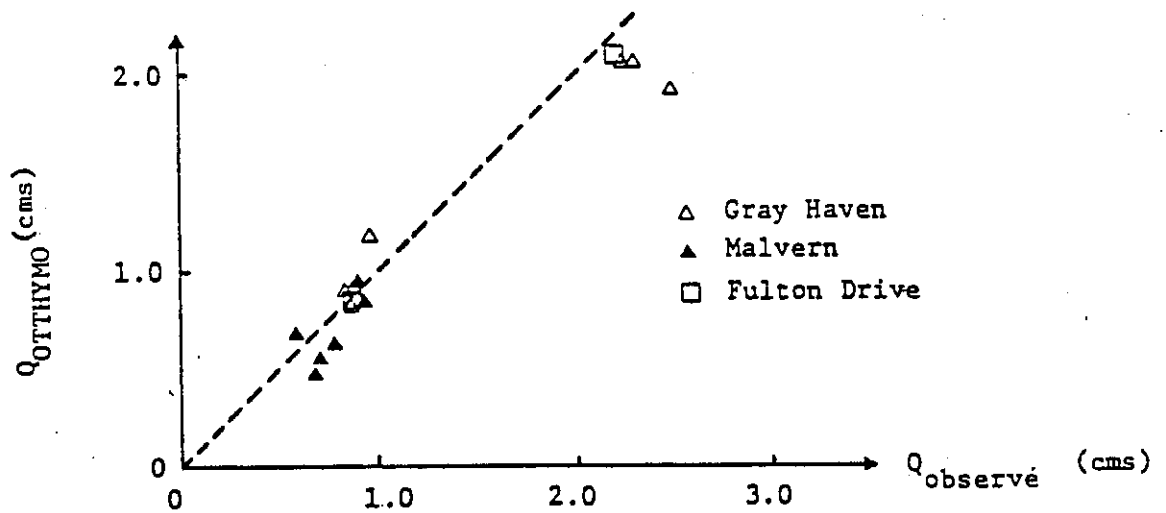


Fig. 2.5 : Comparaison des débits maximum observés et simulés

II.4 Procédures d'acheminement

Les techniques d'acheminement peuvent être classées en "acheminement hydraulique" et "acheminement hydrologique". L'écoulement dans

les cours d'eau, canaux ou conduites est en général non-continu, non-uniforme et ne peut être décrit qu'avec l'aide des équations dynamiques complètes de mouvement et de continuité connues sous le nom d'équation de St-Venant. Une solution directe de ces équations n'est pas possible et leur résolution pour "l'acheminement hydraulique" se fait à l'aide de méthodes numériques ou par différence finie (par exemple la méthode implicite du modèle HVM-Dorsch ou celle explicite du modèle WRE-Transport) ou alors par simplification de ces équations en utilisant les différentes formes de la méthode de la cinématique des ondes. Pour "l'acheminement hydrologique" les méthodes sont dérivées des relations de stockage où le débit sortant d'un bief à un temps $(t+\Delta t)$ est une fonction linéaire du débit entrant à un temps (t) et $(t+\Delta t)$ et du débit sortant au temps (t) .

II.4.1 Acheminement par des conduites

Le modèle OTTHYMO possède une nouvelle commande appelée KINROUTE pour acheminer les hydrogrammes par des conduites. Des tests ont montré que l'acheminement par KINROUTE donne des résultats proches de ceux obtenus par des modèles dynamiques plus complets de systèmes de drainages, ceci pour des pentes rencontrées généralement dans la pratique (Réf. no

KINROUTE est un modèle du type Cunge-Muskingum qui permet la représentation de l'atténuation des ondes. Cette méthode diffère de celles qui cherchent des solutions directes des équations cinématiques des ondes. Le système de résolution est simple et les paramètres sont fonctions des caractéristiques physiques et hydrauliques des conduites. Un des avantages sur les solutions numériques est qu'il est possible de faire varier les paramètres du modèle (en particulier la vitesse de l'onde) avec la variation du débit.

Le modèle utilise la relation de la cinématique des ondes dans la forme:

$$\frac{1}{C} \frac{\partial Q}{\partial t} + \frac{\partial Q}{\partial X} = 0$$

où C est la vitesse de l'onde qui peut être évaluée par la loi de Kleitz-Seddar:

$$C = \frac{dQ}{dA}_{x=\text{const.}} = \frac{1}{B} \frac{dQ}{dy}_{x=\text{const.}}$$

$Q(x,t)$ est le débit et, x et t sont respectivement les coordonnées de lieu et de temps.

La forme de l'équation est identique à celle du modèle de Muskingum:

$$Q_{i+1}^{j+1} = C_1 Q_i^j + C_2 Q_i^{j+1} + C_3 Q_{i+1}^j$$

$$C_1 = \frac{K\theta + \Delta t/2}{K(1-\theta) + \Delta t/2} ; C_2 = \frac{-K\theta + \Delta t/2}{K(1-\theta) + \Delta t/2} ; C_3 = \frac{K(1-\theta) - \Delta t/2}{K(1-\theta) + \Delta t/2}$$

La vitesse de l'onde C est par hypothèse constante. Δx est la longueur du tronçon et K représente le temps de parcours d'un certain débit dont on fait également l'hypothèse qu'il est constant. Le facteur pondéral θ varie avec l'écoulement et peut être obtenu à l'aide de l'équation suivante:

$$\theta = \frac{1}{2} \left(1 - \frac{Q}{BS_0 C \Delta x} \right) ; 0 \leq \theta \leq 0.5$$

où B est la largeur de la surface d'écoulement
 S_0 est la pente de la conduite.

En ce qui concerne la précision du modèle cinématique par différence finie, elle peut être considérée comme identique à une approximation du second ordre du modèle de la diffusion des ondes. KINROUTE calcule également le diamètre des conduites.

ANNEXE 2

Résultats Détaillés
Des Simulation

```

*****
**                                     **
**           M I C R O H Y M O --- 3   **
**                                     **
**           ( P . C . D T T H Y M O ) **
**                                     **
**           V E R S I O N 2.0+       **
**                                     **
**                                     **
**           ADAPTED FOR MICROCOMPUTER BY **
**                                     **
**           ANDREW BRODIE ASSOCIATES INC. **
**                                     **
**                                     **
**           ANDREW BRODIE & ASSOCIATES INC **
**                                     **
*****
THE METRIC UNITS OPTION HAS BEEN SPECIFIED

```

START RAINFALL BEGIN AT 0.0 HRS

```

* COMMENTS
* RUISSEAU DES FEES
* 5 STROM
* PRE-DEV COND. REVISED
* DT=0.0833 NI=36
* FILE NAME FEESP.01

```

* GET INFLOW TO THE POINT -B-

* SUBAREA 1

```

COMPUTE NASHYD ID=1 HYD=101 DT=0.0833H DA=62.6 HECT AA=0.0 AB=0.0
CN=68 IA=2.5 MM N=3 TP=1.57 H NI=36
4.23 4.23 5.27 5.27 7.07 7.07 11.52 11.52 45.05 45.05
72.96 72.96 62.52 62.52 19.19 19.19 12.59 12.59 9.5 9.5
7.67 7.67 6.46 6.46 5.59 5.59 4.94 4.94 4.44 4.44
4.03 4.03 3.7 3.7 3.42 3.42

```

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 1.52 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = .660 CMS RUNOFF VOLUME = 12.71 MM TIME TO PEAK = 2.999 HRS
TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .26

PRINT HYD ID=1 1

HYDROGRAPH FROM AREA 101

RUNOFF VOLUME = 12.71 MM
PEAK DISCHARGE RATE = .660 CMS

* SUBAREA 2

```

COMPUTE NASHYD ID=2 HYD=102 DT=0.0833 H DA=292.1 HECT AA=0.0 AB=0.0
CN=55 IA=2.5 MM N=3 TP=2.0 H NI=36
-1

```

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 5.58 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = 1.662 CMS RUNOFF VOLUME = 8.28 MM TIME TO PEAK = 3.499 HRS
TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .17

ADD HYD ID=4 HYD=312 IDI=1 IDII=2
PEAK FLOW = 2.297 CMS RUNOFF VOLUME = 9.06 MM TIME TO PEAK= 3.33 HOURS

```

ADD HYD ID=4 HYD NO=312 ID I=1 ID II=2
STORE HYD ID=6 HYD=102 DT=0.0833 H DA=285.64 HECT AA=0.0 AB=0.0
.0 .0 .0 .0 .2 .2 .3 .3 .4 .4 .4 .4 .4 .4 .4 .4 .4 .4 .4 .4
.4 .4 .4 .4 .4 .4 .4 .4 .4 .4 .4 .4 .4 .4 .4 .4 .4 .4 .4 .4

```

TPEAK(6)= .8330
PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 102

RUNOFF VOLUME = 1.28 MM
 PEAK DISCHARGE RATE = .400 CMS

ADD HYD ID=3 HYD=312 ID I=6 ID II=4
 PEAK FLOW = 2.662 CMS RUNOFF VOLUME = 5.59 MM TIME TO PEAK= 3.08 HOURS

ADD HYD ID=3 HYD NO=312 ID I=6 ID II=4

*-----
 * INFLOW TO THE POINT -B-
 *-----

PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 312

RUNOFF VOLUME = 5.59 MM
 PEAK DISCHARGE RATE = 2.662 CMS

*-----
 * ROUTING FROM THE POINT B TO POINT D
 *-----

COMPUTE RATING CURVEID=1 VSN=1 NSEG=3 NINEL=100.57
 MAXEL=104.24
 CHSLP=0.004
 FPSLP=0.004
 N=0.05 DIST=113 N=-0.03 DIST=117 N=0.05 DIST=226
 0 104.24 100 101.79 110 101.17 113.0 101.17
 113.8 100.57 116.5 100.57 117 101.30 120 101.52
 126 102.40 226 102.98

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
100.57	.0	.0
100.76	.6	.4
100.96	1.2	1.2
101.15	1.9	2.3
101.34	3.4	4.2
101.54	6.0	7.2
101.73	9.5	11.6
101.92	14.1	17.1
102.12	20.4	24.9
102.31	28.5	35.4
102.50	39.3	46.7
102.69	57.3	65.4
102.89	83.2	93.4
103.08	116.2	135.2
103.27	151.5	190.8
103.47	188.3	257.2
103.66	226.6	334.1
103.85	266.5	421.4
104.05	307.8	519.1
104.24	350.7	627.1

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
 L=2800 SLP=0.004

TRAVEL TIME TABLE
 REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.19	0.	1.1938
.39	1.	.7999
.58	2.	.6417
.77	4.	.6414
.97	7.	.6490
1.16	12.	.6390
1.35	17.	.6401
1.55	25.	.6390
1.74	35.	.6274
1.93	47.	.6540
2.12	65.	.6812
2.32	93.	.6931
2.51	135.	.6689
2.70	191.	.6177
2.90	257.	.5695
3.09	334.	.5276
3.28	421.	.4918
3.48	519.	.4612
3.67	627.	.4350

ROUTE

ID=6 HYD=201
 TARI-2 RT-0 00220

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 5.59 MM
 PEAK DISCHARGE RATE = 2.286 CMS

*-----
 * GET INFLOW TO POINT -D-
 *-----
 * SUBAREA 3
 *-----

COMPUTE NASHYD ID=1 HYD=103 DT=0.0833 H DA=193.55 HECT AA=0.0 AB=0.0
 CN=68 IA=2.5 MM N=3 TP=1.58H NI=36

-1
 SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 4.68 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
 PEAK DISCHARGE = 2.032 CMS RUNOFF VOLUME = 12.71 MM TIME TO PEAK = 2.999 HRS
 TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .26

*-----
 * SUBAREA 4
 *-----

COMPUTE NASHYD ID=2 HYD=104 DT=0.0833 H DA=254.84 HECT AA=0.0 AB=0.0
 CN=55 IA=2.5 MM N=3 TP=0.79H NI=36

-1
 SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 12.32 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
 PEAK DISCHARGE = 2.856 CMS RUNOFF VOLUME = 8.28 MM TIME TO PEAK = 1.999 HRS
 TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .17

ADD HYD ID=3 HYD=312 IDI=1 IDII=2
 PEAK FLOW = 4.418 CMS RUNOFF VOLUME = 10.19 MM TIME TO PEAK= 2.25 HOURS

ADD HYD ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2
 ID=1 HYD=163 IDI=6 IDII=3
 PEAK FLOW = 6.046 CMS RUNOFF VOLUME = 7.49 MM TIME TO PEAK= 2.83 HOURS

ADD HYD ID=1 HYD NO=163 ID I=6 ID II=3

*-----
 * SUBAREA 6
 *-----

COMPUTE NASHYD ID=2 HYD=106 DT=0.0833 H DA=37.10 HECT AA=0.0 AB=0.0
 CN=55 IA=2.5 MM N=3 TP=0.39H NI=36

-1
 SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 3.63 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
 PEAK DISCHARGE = .670 CMS RUNOFF VOLUME = 8.28 MM TIME TO PEAK = 1.499 HRS
 TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .17

ADD HYD ID=3 HYD=312 IDI=1 IDII=2
 PEAK FLOW = 6.229 CMS RUNOFF VOLUME = 7.51 MM TIME TO PEAK= 2.67 HOURS

ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2

*-----
 * INFLOW TO POINT -D-
 *-----

PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 312

RUNOFF VOLUME = 7.51 MM
 PEAK DISCHARGE RATE = 6.229 CMS

*-----
 * ROUTING FROM THE POINT D TO POINT 6
 *-----

COMPUTE RATING CURVEID=1 VSN=1 NSEG=3 NINEL=94.48
 MAXEL=97.89
 CHSLP=0.0035
 FPSLP=0.0035
 N=0.05 DIST=102.5 N=-0.03 DIST=107.5 N=0.05 DIST=210
 0.0 97.89 100 95.77 102.5 95.57 103.5 94.48
 106.5 94.48 107.5 95.39 110 95.78 210 96.54

RATING CURVE VALLEY SECTION 1.0
 WATER FLOW FLOW
 SURFACE AREA RATE
 ELEV SQ METRES CMS

94.66	.6	.3
94.84	1.2	1.1
95.02	1.9	2.1
95.20	2.6	3.0
95.38	3.2	4.1
95.56	4.0	5.2
95.74	5.0	6.4
95.92	6.2	7.7
96.10	7.5	9.1
96.27	9.0	10.6
96.45	10.5	12.2
96.63	12.0	13.9
96.81	13.5	15.6
96.99	15.0	17.4
97.17	16.5	19.2
97.35	18.0	21.1
97.53	19.5	23.0
97.71	21.0	25.0
97.89	22.5	27.0

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=2850 SLP=0.0035

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.18	0.	1.3471
.36	1.	.8953
.54	2.	.7145
.72	3.	.6126
.90	5.	.5454
1.08	7.	.4929
1.26	10.	.4654
1.44	14.	.5472
1.62	20.	.7217
1.79	32.	.8267
1.97	50.	.8536
2.15	78.	.8097
2.33	116.	.7345
2.51	162.	.6698
2.69	216.	.6164
2.87	277.	.5722
3.05	346.	.5352
3.23	423.	.5040
3.41	508.	.4772

ROUTE ID=6 HYD=201
INDI=3 DT= 0.0833
PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 7.51 MM
PEAK DISCHARGE RATE = 5.940 CMS

*-----
* GET INFLOW TO POINT -6-
*-----
*-----
* SUBAREA 5AB
*-----

COMPUTE NASHYD ID=1 HYD=107 DT=0.0833 H DA=140.30 HECT AA=0.0 AB=0.0
CN=55 IA=2.5 MM N=3 TP=0.88H NI=36

-1
SHAPE CONSTANT, N = 3.00
UNIT PEAK = 6.09 CMS

SUM OF THE UNIT HYDROGRAPH SQ-ORDINATES = 12.00
PEAK DISCHARGE = 1.456 CMS RUNOFF VOLUME = 8.28 MM TIME TO PEAK = 2.166 HRS
TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .17

*-----
* SUBAREA 5C
*-----

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=45.5 CCK=1.0
XIMP=0.15 TIMP=0.15 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LGI=550 MNI=0.013
SLP=1 LBP=550 MNP=0.25

-1
UNIT PEAK = .157 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 8.06 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .027 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 59.39 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 2.083 CMS RUNOFF VOLUME = 16.08 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .33

ADD HYD ID=3 HYD=261 IDI=1 IDII=2
PEAK FLOW = 2.375 CMS RUNOFF VOLUME = 10.19 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=3 HYD NO=261 ID I=1 ID II=2
ADD HYD ID=2 HYD=216 IDI=3 IDII=6
PEAK FLOW = 7.200 CMS RUNOFF VOLUME = 7.89 MM TIME TO PEAK= 2.92 HOURS

ADD HYD ID=2 HYD NO=216 ID I=3 ID II=6

* INFLOW TO POINT -G-

PRINT HYD ID=2 1

HYDROGRAPH FROM AREA 216

RUNOFF VOLUME = 7.89 MM
PEAK DISCHARGE RATE = 7.200 CMS

FINISH


```

*****
**                                     **
**           M I C R O H Y M O --- 3   **
**                                     **
**           ( P . C . O T T H Y M O ) **
**                                     **
**           V E R S I O N 2.0+         **
**                                     **
**                                     **
**           ADAPTED FOR MICROCOMPUTER BY **
**                                     **
**           ANDREW BRODIE ASSOCIATES INC. **
**                                     **
**                                     **
**           ANDREW BRODIE & ASSOCIATES INC **
**                                     **
**                                     **
*****
THE METRIC UNITS OPTION HAS BEEN SPECIFIED

```

START RAINFALL BEGIN AT 0.0 HRS

```

* COMMENTS
* RUISSEAU DES FEES
* 100 STROM
* PRE-DEV COND. REVISED
* DT=0.0833 NI=36
* FILE NAME FEES100P.DT1
*-----
* GET INFLOW TO THE POINT -B-
*-----
*-----
* SUBAREA 1
*-----

```

```

COMPUTE NASHYD ID=1 HYD=101 DT=0.0833H DA=62.6 HECT AA=0.0 AB=0.0
CN=68 IA=2.5 MM N=3 TP=1.57 H NI=36
4.92 4.92 6.35 6.35 8.95 8.95 18.54 18.54 78.42 78.42
107.19 107.19 99.64 99.64 31.1 31.1 17.51 17.51 12.65
12.65 9.85 9.85 8.05 8.05 6.81 6.81 5.89 5.89 5.2 5.2
4.65 4.65 4.21 4.21 3.85 3.85

```

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 1.52 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = 1.368 CMS RUNOFF VOLUME = 25.71 MM TIME TO PEAK = 2.916 HRS
TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .36

PRINT HYD ID=1 1

HYDROGRAPH FROM AREA 101

RUNOFF VOLUME = 25.71 MM
PEAK DISCHARGE RATE = 1.368 CMS

```

*-----
* SUBAREA 2
*-----

```

```

COMPUTE NASHYD ID=2 HYD=102 DT=0.0833 H DA=292.1 HECT AA=0.0 AB=0.0
CN=55 IA=2.5 MM N=3 TP=2.0 H NI=36
-1

```

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 5.58 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = 3.561 CMS RUNOFF VOLUME = 17.54 MM TIME TO PEAK = 3.332 HRS
TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .24

ADD HYD ID=4 HYD=312 IDI=1 IDII=2
PEAK FLOW = 4.873 CMS RUNOFF VOLUME = 18.98 MM TIME TO PEAK= 3.25 HOURS

```

ADD HYD ID=4 HYD NO=312 ID I=1 ID II=2
STORE HYD ID=6 HYD=102 DT=0.0833 H DA=285.64 HECT AA=0.0 AB=0.0
.0 .0 .0 .0 .2 .2 .3 .3 .4 .4 .5 .5 .5 .5 .5 .5 .5 .5
.5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5

```

TPEAK(6)= .9996
PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 102

PEAK DISCHARGE RATE = .500 CMS

ADD HYD ID=3 HYD=312 IDI=6 IDII=4
PEAK FLOW = 5.351 CMS RUNOFF VOLUME = 11.21 MM TIME TO PEAK= 3.08 HOURS

ADD HYD ID=3 HYD NO=312 ID I=6 ID II=4
*-----
* INFLOW TO THE POINT -B-
*-----
PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 312

RUNOFF VOLUME = 11.21 MM
PEAK DISCHARGE RATE = 5.351 CMS

*-----
* ROUTING FROM THE POINT B TO POINT D # 4
*-----
COMPUTE RATING CURVEID=1 VSN=1 NSEG=3 NINEL=100.57
MAXEL=104.24
CHSLP=0.004
FPSLP=0.004
N=0.05 DIST=113 N=-0.03 DIST=117 N=0.05 DIST=226
0 104.24 100 101.79 110 101.17 113.0 101.17
113.8 100.57 116.5 100.57 117 101.30 120 101.52
126 102.40 226 102.98

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
100.57	.0	.0
100.76	.6	.4
100.96	1.2	1.2
101.15	1.9	2.3
101.34	3.4	4.2
101.54	6.0	7.2
101.73	9.5	11.6
101.92	14.1	17.1
102.12	20.4	24.9
102.31	28.5	35.4
102.50	39.3	46.7
102.69	57.3	65.4
102.89	83.2	93.4
103.08	116.2	135.2
103.27	151.5	190.8
103.47	188.3	257.2
103.66	226.6	334.1
103.85	266.5	421.4
104.05	307.8	519.1
104.24	350.7	627.1

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=2800 SLP=0.004

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.19	0.	1.1938
.39	1.	.7999
.58	2.	.6417
.77	4.	.6414
.97	7.	.6490
1.16	12.	.6390
1.35	17.	.6401
1.55	25.	.6390
1.74	35.	.6274
1.93	47.	.6540
2.12	65.	.6812
2.32	93.	.6931
2.51	135.	.6689
2.70	191.	.6177
2.90	257.	.5695
3.09	334.	.5276
3.28	421.	.4918
3.48	519.	.4612
3.67	627.	.4350

ROUTE ID=6 HYD=201

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 11.21 MM
 PEAK DISCHARGE RATE = 4.639 CMS

*-----
 * GET INFLOW TO POINT -D-
 *-----

* SUBAREA 3
 *-----

COMPUTE NASHYD ID=1 HYD=103 DT=0.0833 H DA=193.55 HECT AA=0.0 AB=0.0
 CN=68 IA=2.5 MM N=3 TP=1.58H NI=36

-1
 SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 4.68 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
 PEAK DISCHARGE = 4.209 CMS RUNOFF VOLUME = 25.71 MM TIME TO PEAK = 2.916 HRS
 TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .36

*-----
 * SUBAREA 4
 *-----

COMPUTE NASHYD ID=2 HYD=104 DT=0.0833 H DA=254.84 HECT AA=0.0 AB=0.0
 CN=55 IA=2.5 MM N=3 TP=0.79H NI=36

-1
 SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 12.32 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
 PEAK DISCHARGE = 6.439 CMS RUNOFF VOLUME = 17.54 MM TIME TO PEAK = 1.916 HRS
 TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .24

ADD HYD ID=3 HYD=312 IDI=1 IDII=2
 PEAK FLOW = 9.677 CMS RUNOFF VOLUME = 21.07 MM TIME TO PEAK= 2.17 HOURS

ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2
 ADD HYD ID=1 HYD=163 IDI=6 IDII=3
 PEAK FLOW = 12.463 CMS RUNOFF VOLUME = 15.27 MM TIME TO PEAK= 2.50 HOURS

ADD HYD ID=1 HYD NO=163 ID I=6 ID II=3

*-----
 * SUBAREA 6
 *-----

COMPUTE NASHYD ID=2 HYD=106 DT=0.0833 H DA=37.10 HECT AA=0.0 AB=0.0
 CN=55 IA=2.5 MM N=3 TP=0.39H NI=36

-1
 SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 3.63 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
 PEAK DISCHARGE = 1.547 CMS RUNOFF VOLUME = 17.53 MM TIME TO PEAK = 1.499 HRS
 TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .24

ADD HYD ID=3 HYD=312 IDI=1 IDII=2
 PEAK FLOW = 12.908 CMS RUNOFF VOLUME = 15.34 MM TIME TO PEAK= 2.42 HOURS

ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2

*-----
 * INFLOW TO POINT -D-
 *-----

PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 312

RUNOFF VOLUME = 15.34 MM
 PEAK DISCHARGE RATE = 12.908 CMS

*-----
 * ROUTING FROM THE POINT D TO POINT 6
 *-----

COMPUTE RATING CURVEID=1 VSN=1 NSEG=3 NINEL=94.48
 MAXEL=97.89
 CHSLP=0.0035
 FPSLP=0.0035
 N=0.05 DIST=102.5 N=-0.03 DIST=107.5 N=0.05 DIST=210
 0.0 97.89 100 95.77 102.5 95.57 103.5 94.48
 106.5 94.48 107.5 95.39 110 95.78 210 96.54

RATING CURVE VALLEY SECTION 1.0
 WATER FLOW FLOW
 SURFACE AREA RATE
 ELEV SQ METRES CMS

94.66	.6	.3
94.84	1.2	1.1
95.02	1.9	2.1
95.20	2.7	3.5
95.38	3.5	5.1
95.56	4.5	7.2
95.74	5.8	9.9
95.92	9.3	13.5
96.10	18.5	20.2
96.27	33.3	31.9
96.45	54.0	50.0
96.63	79.8	78.0
96.81	107.6	116.0
96.99	136.9	151.8
97.17	167.8	215.5
97.35	200.1	276.9
97.53	234.0	346.2
97.71	269.4	423.3
97.89	306.4	508.3

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=2850 SLP=0.0035

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.18	0.	1.3471
.36	1.	.8953
.54	2.	.7145
.72	3.	.6126
.90	5.	.5454
1.08	7.	.4929
1.26	10.	.4654
1.44	14.	.5472
1.62	20.	.7217
1.79	32.	.8267
1.97	50.	.8536
2.15	78.	.8097
2.33	116.	.7345
2.51	162.	.6698
2.69	216.	.6164
2.87	277.	.5722
3.05	346.	.5352
3.23	423.	.5040
3.41	508.	.4772

ROUTE ID=6 HYD=201
INDI=3 DT= 0.0833
PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 15.34 MM
PEAK DISCHARGE RATE = 12.002 CMS

*-----
* GET INFLOW TO POINT -6-
*-----
* SUBAREA SAB
*-----

COMPUTE NASHYD ID=1 HYD=107 DT=0.0833 H DA=140.30 HECT AA=0.0 AB=0.0
CN=55 IA=2.5 MM N=3 TP=0.88H NI=36

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 6.09 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = 3.270 CMS RUNOFF VOLUME = 17.54 MM TIME TO PEAK = 2.082 HRS
TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .24

*-----
* SUBAREA SC
*-----

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=45.5 CCK=1.0
XIMP=0.15 TIMP=0.15 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LBI=550 MNI=0.013
SLP=1 LGP=550 MNP=0.25

UNIT PEAK = .175 CMS
PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
STORAGE COEFF. SC = 6.91 MINS

UNIT PEAK = .035 LMS
PEAK INTENSITY (RAIN EXCESS) = 81.48 MM/HR
STORAGE COEFF. SC = 45.45 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 5.009 CMS RUNOFF VOLUME = 37.41 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .52

ADD HYD ID=3 HYD=261 IDI=1 IDII=2
PEAK FLOW = 5.729 CMS RUNOFF VOLUME = 22.40 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=3 HYD NO=261 ID I=1 ID II=2
ADD HYD ID=2 HYD=216 IDI=3 IDII=6
PEAK FLOW = 14.714 CMS RUNOFF VOLUME = 16.34 MM TIME TO PEAK= 2.67 HOURS

ADD HYD ID=2 HYD NO=216 ID I=3 ID II=6

*-----
* INFLOW TO POINT -G-
*-----

PRINT HYD ID=2 1

HYDROGRAPH FROM AREA 216

RUNOFF VOLUME = 16.34 MM
PEAK DISCHARGE RATE = 14.714 CMS

FINISH

```

XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
XX                                                                 XX
XX          M I C R O H Y M O --- 3                               XX
XX                                                                 XX
XX          ( P . C . D T T H Y M O )                             XX
XX                                                                 XX
XX          V E R S I O N 2.0+                                    XX
XX                                                                 XX
XX                                                                 XX
XX          ADAPTED FOR MICROCOMPUTER BY                          XX
XX                                                                 XX
XX          ANDREW BRODIE ASSOCIATES INC.                         XX
XX                                                                 XX
XX                                                                 XX
XX          ANDREW BRODIE & ASSOCIATES INC                        XX
XX                                                                 XX
XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
THE METRIC UNITS OPTION HAS BEEN SPECIFIED

```

START RAINFALL BEGIN AT 0.0 HRS

```

* COMMENTS
* RUISSEEAU DES FEES
* 5 STROM
* POST-DEV COND.ALT.-ALFA- R E V I S E D
* DT=0.0833 NI=36
* FILE NAME FEESF.OT6

```

* GET INFLOW TO THE POINT -B-

* SUBAREA 1

```

COMPUTE NASHYD      ID=1 HYD=101 DT=0.0833H DA=62.6 HECT AA=0.0 AB=0.0
                   CN=68 IA=2.5 MM N=3 TP=1.57 H NI=36
                   4.23 4.23 5.27 5.27 7.07 7.07 11.52 11.52 45.05 45.05
                   72.96 72.96 62.52 62.52 19.19 19.19 12.59 12.59 9.5 9.5
                   7.67 7.67 6.46 6.46 5.59 5.59 4.94 4.94 4.44 4.44
                   4.03 4.03 3.7 3.7 3.42 3.42

```

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 1.52 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = .660 CMS RUNOFF VOLUME = 12.71 MM TIME TO PEAK = 2.999 HRS
TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .26

PRINT HYD ID=1 1

HYDROGRAPH FROM AREA 101

RUNOFF VOLUME = 12.71 MM
 PEAK DISCHARGE RATE = .660 CMS

 * SUBAREA 2

COMPUTE NASHYD ID=2 HYD=102 DT=0.0833 H DA=292.1 HECT AA=0.0 AB=0.0
 CN=55 IA=2.5 MM N=3 TP=2.0 H NI=36
 -1

SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 5.58 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
 PEAK DISCHARGE = 1.662 CMS RUNOFF VOLUME = 8.28 MM TIME TO PEAK = 3.499 HRS
 TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .17

ADD HYD ID=4 HYD=312 IDI=1 IDII=2
 PEAK FLOW = 2.297 CMS RUNOFF VOLUME = 9.06 MM TIME TO PEAK= 3.33 HOURS

ADD HYD ID=4 HYD NO=312 ID I=1 ID II=2
 STORE HYD ID=6 HYD=102 DT=0.0833 H DA=295.64 HECT AA=0.0 AB=0.0
 .0 .0 .0 .0 .2 .2 .3 .3 .4 .4 .5 .5 .5 .5 .5 .5 .5
 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5 .5
 TPEAK(6)= .9996
 PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 102

RUNOFF VOLUME = 1.55 MM
 PEAK DISCHARGE RATE = .500 CMS

ADD HYD ID=3 HYD=312 IDI=6 IDII=4
 PEAK FLOW = 2.762 CMS RUNOFF VOLUME = 5.71 MM TIME TO PEAK= 3.08 HOURS

ADD HYD ID=3 HYD NO=312 ID I=6 ID II=4

 * INFLOW TO THE POINT -B-

 PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 312

RUNOFF VOLUME = 5.71 MM
 PEAK DISCHARGE RATE = 2.762 CMS

 * ROUTING FROM THE POINT B TO POINT D

COMPUTE RATING CURVEID=1 VSN=1 NSE6=3 NINEL=100.57
 MAXEL=104.24
 CHSLP=0.004
 FPSLP=0.004
 N=0.05 DIST=113 N=-0.03 DIST=117 N=0.05 DIST=226
 0 104.24 100 101.79 110 101.17 113.0 101.17
 113.8 100.57 116.5 100.57 117 101.30 120 101.52
 126 102.40 226 102.98

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
100.57	.0	.0
100.76	.6	.4
100.96	1.2	1.2
101.15	1.9	2.3
101.34	3.4	4.2
101.54	6.0	7.2
101.73	9.5	11.6
101.92	14.1	17.1
102.12	20.4	24.9
102.31	28.5	35.4
102.50	39.3	46.7
102.69	57.3	65.4
102.89	83.2	93.4
103.08	116.2	135.2
103.27	151.5	190.8
103.47	190.0	257.0

103.85 266.5 421.4
 104.05 307.8 519.1
 104.24 350.7 627.1

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
 L=2600 SLP=0.004

TRAVEL TIME TABLE
 REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.19	0.	1.1938
.39	1.	.7599
.58	2.	.6417
.77	4.	.6414
.97	7.	.6490
1.16	12.	.6390
1.35	17.	.6401
1.55	25.	.6390
1.74	35.	.6274
1.93	47.	.6540
2.12	65.	.6812
2.32	93.	.6931
2.51	135.	.6689
2.70	191.	.6177
2.90	257.	.5695
3.09	334.	.5276
3.28	421.	.4918
3.48	519.	.4612
3.67	627.	.4350

ROUTE ID=6 HYD=201
 INDI=3 DT= 0.08330
 PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 5.71 MM
 PEAK DISCHARGE RATE = 2.364 CMS

*-----
 * GET INFLOW TO POINT -D-
 *-----
 * SUBAREA 3
 *-----

COMPUTE NASHYD ID=1 HYD=103 DT=0.0833 H DA=193.55 HECT AA=0.0 AB=0.0
 CN=68 IA=2.5 MM N=3 TP=1.58H NI=36
 -1

SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 4.66 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
 PEAK DISCHARGE = 2.032 CMS RUNOFF VOLUME = 12.71 MM TIME TO PEAK = 2.999 HRS
 TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .26

*-----
 * SUBAREA 4
 *-----

COMPUTE NASHYD ID=2 HYD=104 DT=0.0833 H DA=254.84 HECT AA=0.0 AB=0.0
 CN=55 IA=2.5 MM N=3 TP=0.79H NI=36
 -1

SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 12.32 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
 PEAK DISCHARGE = 2.856 CMS RUNOFF VOLUME = 8.28 MM TIME TO PEAK = 1.999 HRS
 TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .17

ADD HYD ID=3 HYD=312 ID I=1 ID II=2
 PEAK FLOW = 4.418 CMS RUNOFF VOLUME = 10.19 MM TIME TO PEAK= 2.25 HOURS

ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2
 ADD HYD ID=1 HYD=163 ID I=6 ID II=3
 PEAK FLOW = 6.148 CMS RUNOFF VOLUME = 7.56 MM TIME TO PEAK= 2.83 HOURS

ADD HYD ID=1 HYD NO=163 ID I=6 ID II=3

*-----
 * SUBAREA 6
 *-----

COMPUTE NASHYD ID=2 HYD=106 DT=0.0833 H DA=37.10 HECT AA=0.0 AB=0.0
 CN=55 IA=2.5 MM N=3 TP=0.39H NI=36
 -1

SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 3.63 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .17
 ADD HYD ID=3 HYD=312 IDI=1 IDII=2
 PEAK FLOW = 6.327 CMS RUNOFF VOLUME = 7.58 MM TIME TO PEAK= 2.75 HOURS

ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2
 *-----
 * INFLOW TO POINT -D-
 *-----
 * PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 312

RUNOFF VOLUME = 7.58 MM
 PEAK DISCHARGE RATE = 6.327 CMS

*-----
 * ROUTING FROM THE POINT D TO POINT E
 *-----
 *
 * ROUTING - X SECTION #2
 *-----

COMPUTE RATING CURVE ID=1 VSN=1 NSEG=1 NINEL=90.58
 MAXEL=92.84
 CHSLP=0.0041
 FPSLP=0.0041

N=0.03 DIST=18
 0.0 92.84 1.0 92.84
 2.0 92.24 4.0 92.24
 7.4 90.96 8.0 90.58
 10 90.58 10.4 91.28
 14 92.32 16 92.32
 17 92.84 18 92.84

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
90.58	.0	.0
90.70	.3	.1
90.82	.5	.4
90.94	.9	.8
91.06	1.2	1.2
91.17	1.6	1.8
91.29	2.0	2.6
91.41	2.5	3.3
91.53	3.1	4.3
91.65	3.8	5.6
91.77	4.6	7.0
91.89	5.5	8.8
92.01	6.4	10.8
92.13	7.4	13.1
92.25	8.6	14.1
92.36	10.1	16.3
92.48	11.8	20.8
92.60	13.6	25.8
92.72	15.4	31.2
92.84	17.3	34.4

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
 L=1350 SLP=0.0041

TRAVEL TIME TABLE
 REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.12	0.	.7780
.24	0.	.5191
.36	1.	.4140
.48	1.	.3606
.59	2.	.3245
.71	3.	.2987
.83	3.	.2856
.95	4.	.2716
1.07	6.	.2579
1.19	7.	.2450
1.31	9.	.2331
1.43	11.	.2223
1.55	13.	.2123
1.67	14.	.2278
1.78	16.	.2313
1.90	21.	.2126
2.02	26.	.1977
2.14	31.	.1853

* INFLOW TO POINT ---

PRINT HYD ID=2 1

HYDROGRAPH FROM AREA 261

RUNOFF VOLUME = 9.77 MM
PEAK DISCHARGE RATE = 11.990 CMS

* ROUTING FROM THE POINT F TO POINT G

* ARTIFICIAL CHANNEL

COMPUTE RATINGS CURVEID=1 VSN=1 NSEG=1 NINEL=84.30
MAXEL=87.00
CHSLP=0.0004
FPSLP=0.0004

N=0.035 DIST=24.
0.0 87.00 4.0 85.3
6.5 85.3 8. 84.3
16.0 84.3 17.5 85.3
20.0 85.3 24.0 87.00

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
84.30	.0	.0
84.44	1.2	.1
84.58	2.4	.6
84.73	3.7	1.1
84.87	5.0	1.8
85.01	6.4	2.6
85.15	7.9	3.6
85.29	9.4	4.7
85.44	11.7	5.2
85.58	14.1	6.9
85.72	16.7	8.8
85.86	19.3	10.9
86.01	22.0	13.3
86.15	24.7	15.8
86.29	27.6	18.6
86.43	30.6	21.6
86.57	33.7	24.8
86.72	36.9	28.2
86.86	40.1	31.8
87.00	43.5	35.7

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=600 SLP=0.0004

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.14	0.	1.0967
.28	1.	.7062
.43	1.	.5499
.57	2.	.4625
.71	3.	.4055
.85	4.	.3649
.99	5.	.3342
1.14	5.	.3778
1.28	7.	.3428
1.42	9.	.3157
1.56	11.	.2939
1.71	13.	.2760
1.85	16.	.2609
1.99	19.	.2479
2.13	22.	.2367
2.27	25.	.2268
2.42	28.	.2181
2.56	32.	.2102
2.70	36.	.2032

ROUTE ID=6 HYD=201
INDI=2 DT= 0.08330

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 13 RATE = 174.83
PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 51 RATE = 189.26
PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 52 RATE = 185.92

```

-----
      OUTFLOW NUMBER = 55RATE = 182.11
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
      OUTFLOW NUMBER = 54RATE = 177.32
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
      OUTFLOW NUMBER = 55RATE = 173.45
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
      OUTFLOW NUMBER = 56RATE = 168.75
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
      OUTFLOW NUMBER = 57RATE = 163.89
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
      OUTFLOW NUMBER = 58RATE = 158.95
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
      OUTFLOW NUMBER = 59RATE = 153.98
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
      OUTFLOW NUMBER = 60RATE = 149.02
PRINT HYD          ID=6 1

```

HYDROGRAPH FROM AREA 201

```

RUNOFF VOLUME = 9.77 MM
PEAK DISCHARGE RATE = 8.617 CMS

```

```

*-----
* GET INFLOW TO POINT -6-
*-----
*
* SUBAREA 50
*-----

```

```

COMPUTE URSHYD      ID=1 HYD=102 DT=0.0833 DA=45.5 LKK=1.0
                   XIMP=0.30 TIMP=0.30 NI=36 FO=76.12 FC=13.2 DCAY=4.14
                   F/DD=0.0 DFPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
                   SLI=1 L6I=550 MNI=0.013
                   SLP=1 L6P=550 MNP=0.25
                   -1

```

```

UNIT PEAK = .157 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 8.06 MINS

```

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

```

UNIT PEAK = .027 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 59.39 MINS

```

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 3.109 CMS RUNOFF VOLUME = 21.70 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .45

```

ADD HYD          ID=2 HYD=261 IDI=1 IDII=6
PEAK FLOW =      11.494 CMS      RUNOFF VOLUME = 10.18 MM      TIME TO PEAK= 1.17 HOURS

```

```

      ADD HYD          ID=2      HYD NO=261      ID I=1      ID II=6

```

```

*-----
* TOTAL OUTLET FROM SIDE POINT -6-
*-----
PRINT HYD          ID=2 1

```

HYDROGRAPH FROM AREA 261

```

RUNOFF VOLUME = 10.18 MM
PEAK DISCHARGE RATE = 11.494 CMS

```

```

*-----
FINISH

```

```

XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
XX                                                                                   XX
XX           M I C R O H Y M O --- 3                                                                                   XX
XX                                                                                   XX
XX           ( P . C . D T T H Y M O )                                                                                   XX
XX                                                                                   XX
XX           V E R S I O N  2.0+                                                                                       XX
XX                                                                                   XX
XX                                                                                   XX
XX           ADAPTED FOR MICROCOMPUTER BY                                                                                   XX
XX                                                                                   XX
XX           ANDREW BRODIE ASSOCIATES INC.                                                                                   XX
XX                                                                                   XX
XX                                                                                   XX
XX           ANDREW BRODIE & ASSOCIATES INC                                                                                   XX
XX                                                                                   XX
XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX

```

THE METRIC UNITS OPTION HAS BEEN SPECIFIED

START RAINFALL BEGIN AT 0.0 HRS

```

* COMMENTS
* RUISSEAU DES FEES
* 100 STROM
* POST-DEV COND. ALT. -ALFA- R E V I S E D
* DT=0.0833 NI=36
* FILE NAME FEES100P.OT6

```

* GET INFLOW TO THE POINT -B-

* SUBAREA 1

```

COMPUTE NASHYD      ID=1 HYD=101 DT=0.0833H DA=62.6 HECT AA=0.0 AB=0.0
                   CN=68 IA=2.5 MM N=3 TP=1.57 H NI=36
                   4.92 4.92 6.35 6.35 8.95 8.95 18.54 18.54 78.42 78.42
                   107.19 107.19 99.64 99.64 31.1 31.1 17.51 17.51 12.65
                   12.65 9.85 9.85 8.05 8.05 6.81 6.81 5.89 5.89 5.2 5.2
                   4.65 4.65 4.21 4.21 3.85 3.85

```

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 1.52 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = 1.368 CMS RUNOFF VOLUME = 25.71 MM TIME TO PEAK = 2.916 HRS
TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .36

103.85 288.5 421.4
 104.05 307.8 519.1
 104.24 350.7 627.1

COMPUTE TRAVEL TIME ID=6 REACH=1 NYS=1
 L=2600 SLP=0.004

TRAVEL TIME TABLE
 REACH 1.0

WATER DEPTH METRES	FLDW RATE CMS	TRAVEL TIME HRS
.19	0.	1.1936
.39	1.	.7989
.58	2.	.6417
.77	4.	.6414
.97	7.	.6490
1.16	12.	.6390
1.35	17.	.6401
1.55	25.	.6390
1.74	35.	.6274
1.93	47.	.6540
2.12	65.	.6812
2.32	93.	.6931
2.51	135.	.6689
2.70	191.	.6177
2.90	257.	.5695
3.09	334.	.5276
3.28	421.	.4918
3.48	519.	.4612
3.67	627.	.4350

ROUTE ID=6 HYD=201
 INDI=3 DT= 0.08330
 PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 11.21 MM
 PEAK DISCHARGE RATE = 4.639 CMS

 * GET INFLOW TO POINT -D-

 * SUBAREA 3

COMPUTE NASHYD ID=1 HYD=103 DT=0.0833 H DA=193.55 HECT AA=0.0 AB=0.0
 CN=68 IA=2.5 MM N=3 TP=1.58H NI=36

SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 4.68 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
 PEAK DISCHARGE = 4.209 CMS RUNOFF VOLUME = 25.71 MM TIME TO PEAK = 2.916 HRS
 TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .36

 * SUBAREA 4

COMPUTE NASHYD ID=2 HYD=104 DT=0.0833 H DA=254.84 HECT AA=0.0 AB=0.0
 CN=55 IA=2.5 MM N=3 TP=0.79H NI=36

SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 12.32 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
 PEAK DISCHARGE = 6.439 CMS RUNOFF VOLUME = 17.54 MM TIME TO PEAK = 1.916 HRS
 TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .24

ADD HYD ID=3 HYD=312 IDI=1 IDII=2
 PEAK FLOW = 9.677 CMS RUNOFF VOLUME = 21.07 MM TIME TO PEAK= 2.17 HOURS

ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2
 ADD HYD ID=1 HYD=163 IDI=6 IDII=3
 PEAK FLOW = 12.463 CMS RUNOFF VOLUME = 15.27 MM TIME TO PEAK= 2.50 HOURS

ADD HYD ID=1 HYD NO=163 ID I=6 ID II=3

 * SUBAREA 6

COMPUTE NASHYD ID=2 HYD=106 DT=0.0833 H DA=37.10 HECT AA=0.0 AB=0.0
 CN=55 IA=2.5 MM N=3 TP=0.39H NI=36

SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 3.63 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .24
 ADD HYD ID=3 HYD=312 IDI=1 IDII=1
 PEAK FLOW = 12.908 CMS RUNOFF VOLUME = 15.34 MM TIME TO PEAK = 2.42 HOURS

ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2

 X INFLOW TO POINT -D-
 X-----
 PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 312

RUNOFF VOLUME = 15.34 MM
 PEAK DISCHARGE RATE = 12.908 CMS

 X ROUTING FROM THE POINT D TO POINT E
 X-----
 X ROUTING - X SECTION #2
 X-----

COMPUTE RATING CURVE ID=1 VSN=1 NSEG=1 NINEL=90.58
 MAXEL=92.84
 CHSLP=0.0041
 FPSLP=0.0041

N=0.03 DIST=18

0.0	92.84	1.0	92.84
2.0	92.24	4.0	92.24
7.4	90.96	8.0	90.58
10	90.58	10.4	91.28
14	92.32	16	92.32
17	92.84	18	92.84

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
90.58	.0	.0
90.70	.3	.1
90.82	.5	.4
90.94	.9	.8
91.06	1.2	1.2
91.17	1.6	1.8
91.29	2.0	2.6
91.41	2.5	3.3
91.53	3.1	4.3
91.65	3.8	5.6
91.77	4.6	7.0
91.89	5.5	8.8
92.01	6.4	10.8
92.13	7.4	13.1
92.25	8.6	14.1
92.36	10.1	16.3
92.48	11.8	20.8
92.60	13.6	25.8
92.72	15.4	31.2
92.84	17.3	34.4

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
 L=1350 SLP=0.0041

TRAVEL TIME TABLE
 REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.12	0.	.7780
.24	0.	.5181
.36	1.	.4140
.48	1.	.3606
.59	2.	.3245
.71	3.	.2987
.83	3.	.2856
.95	4.	.2716
1.07	6.	.2579
1.19	7.	.2450
1.31	9.	.2331
1.43	11.	.2223
1.55	13.	.2123
1.67	14.	.2278
1.78	16.	.2313
1.90	21.	.2126
2.02	26.	.1977
2.14	31.	.1853

ROUTE ID=6 HYD=201
 INDI=3 DT= 0.08330
 PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 15.34 MM
 PEAK DISCHARGE RATE = 12.765 CMS

*-----
 * GET INFLOW TO POINT -E-
 *-----

* SUBAREA 5A
 *-----

COMPUTE URSHYD ID=1 HYD=102 DT=0.0833 DA=62.5 CCK=1.0
 XIMP=0.45 TIMP=0.45 NI=36 FO=76.12 FC=13.2 DCAY=4.14
 F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
 SLI=1 LGI=645 MNI=0.013
 SLP=1 LBP=645 MNP=0.25

-1
 UNIT PEAK = .164 CMS
 PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
 STORAGE COEFF. SC = 7.60 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .032 CMS
 PEAK INTENSITY(RAIN EXCESS) = 81.48 MM/HR
 STORAGE COEFF. SC = 50.01 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 10.270 CMS RUNOFF VOLUME = 49.56 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .69

ADD HYD ID=2 HYD=261 IDI=1 IDII=6
 PEAK FLOW = 13.865 CMS RUNOFF VOLUME = 17.14 MM TIME TO PEAK= 2.42 HOURS

ADD HYD ID=2 HYD NO=261 ID I=1 ID II=6

*-----
 * INFLOW TO POINT -E-
 *-----

PRINT HYD ID=2 1

HYDROGRAPH FROM AREA 261

RUNOFF VOLUME = 17.14 MM
 PEAK DISCHARGE RATE = 13.865 CMS

*-----
 * ROUTING FROM THE POINT E TO POINT F
 *-----

* ROUTING - X SECTION #1
 *-----

COMPUTE RATING CURVEID=1 VSN=1 NSEG=1 NINEL=87.47
 MAXEL=89.90
 CHSLP=0.0054
 FPSLP=0.0054

N=0.03 DIST=18
 0.0 89.90 1. 89.90
 2.0 89.27 9.0 89.27
 9.8 87.47 12.2 87.47
 13. 89.21 16. 89.39
 20. 89.40 21.0 89.90
 22 89.90

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
87.47	.0	.0
87.60	.3	.2
87.73	.6	.6
87.85	1.0	1.1
87.98	1.3	1.7
88.11	1.7	2.5

88.37	2.9	4.3
88.49	2.9	5.3
88.52	3.4	6.4
88.75	3.8	7.6
88.88	4.3	8.9
89.00	4.7	10.2
89.13	5.2	11.7
89.26	5.8	12.3
89.39	7.4	10.5
89.52	9.7	14.3
89.64	12.0	20.4
89.77	14.4	27.3
89.90	16.9	34.1

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=900 SLP=0.0054

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.4259
.26	1.	.2823
.38	1.	.2254
.51	2.	.1938
.64	2.	.1732
.77	3.	.1586
.90	4.	.1475
1.02	5.	.1388
1.15	6.	.1317
1.28	6.	.1257
1.41	9.	.1206
1.53	10.	.1162
1.66	12.	.1123
1.79	12.	.1174
1.90	11.	.1152
2.05	14.	.1697
2.17	20.	.1478
2.30	27.	.1320
2.43	34.	.1236

ROUTE

ID=6 HYD=201
INDI=2 DT= 0.08330

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 27 RATE = 446.88

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 28 RATE = 463.11

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 29 RATE = 474.28

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 30 RATE = 481.45

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 31 RATE = 485.36

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 32 RATE = 486.84

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 33 RATE = 486.42

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 34 RATE = 484.56

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 35 RATE = 481.55

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 36 RATE = 477.64

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 37 RATE = 473.02

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 38 RATE = 466.67

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 39 RATE = 458.54

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 40 RATE = 449.92

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 41 RATE = 440.98

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 42 RATE = 431.69

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 43 RATE = 422.06

PRINT HYD

ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 17.14 MM
PEAK DISCHARGE RATE = 13.787 CMS

* BEI INFLOW TO POINT --

* SUBAREA 5B

COMPUTE URBHYD ID=1 HYD=102 DT=0.0633 DA=77.8 COKK=1.0
XIMP=0.45 TIMP=0.45 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSF=4.67 STI=0.0 STP=0.0
SLI=1 LBI=720 MNI=0.013
SLP=1 LBP=720 MNP=0.25

UNIT PEAK = .156 CMS
PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
STORAGE COEFF. SC = 8.12 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .030 CMS
PEAK INTENSITY(RAIN EXCESS) = 31.48 MM/HR
STORAGE COEFF. SC = 53.42 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 12.562 CMS RUNOFF VOLUME = 49.56 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .69

ADD HYD ID=2 HYD=261 IDI=1 IDII=6
PEAK FLOW = 22.482 CMS RUNOFF VOLUME = 19.13 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=2 HYD NO=261 ID I=1 ID II=6

* INFLOW TO POINT --

PRINT HYD ID=2 1

HYDROGRAPH FROM AREA 261

RUNOFF VOLUME = 19.13 MM
PEAK DISCHARGE RATE = 22.482 CMS

* ROUTING FROM THE POINT F TO POINT G

* ARTIFICIAL CHANNEL

COMPUTE RATING CURVEID=1 VSN=1 NSEG=1 NINEL=84.30
MAXEL=87.00
CHSLP=0.0004
FPSLP=0.0004

N=0.035 DIST=24.
0.0 87.00 4.0 85.3
6.5 85.3 8. 84.3
16.0 84.3 17.5 85.3
20.0 85.3 24.0 87.00

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
84.30	.0	.0
84.44	1.2	.2
84.58	2.4	.6
84.73	3.7	1.1
84.87	5.0	1.6
85.01	6.4	2.6
85.15	7.9	3.6
85.29	9.4	4.7
85.44	11.7	5.2
85.58	14.1	6.9
85.72	16.7	8.8
85.86	19.3	10.9
86.01	22.0	13.3
86.15	24.7	15.8
86.29	27.6	18.6
86.43	30.6	21.6
86.57	33.7	24.8
86.72	36.9	28.2
86.86	40.1	31.8
87.00	43.5	35.7

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=600 SLP=0.0004

TRAVEL TIME TABLE
 REACH= 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.14	0.	1.0967
.26	1.	.7062
.43	1.	.5499
.57	2.	.4625
.71	3.	.4055
.85	4.	.3649
.99	5.	.3342
1.14	5.	.3778
1.28	7.	.3428
1.42	9.	.3157
1.56	11.	.2939
1.71	13.	.2760
1.85	16.	.2609
1.99	19.	.2479
2.13	22.	.2367
2.27	25.	.2268
2.42	28.	.2181
2.56	32.	.2102
2.70	36.	.2032

ROUTE ID=6 HYD=201
 INDI=2 DT= 0.08330

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 18 RATE = 562.42
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 39 RATE = 493.79
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 40 RATE = 488.00
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 41 RATE = 480.71
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 42 RATE = 472.42
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 43 RATE = 463.42
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 46 RATE = 436.15
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 47 RATE = 427.75
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 48 RATE = 416.86
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 49 RATE = 404.55
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 69 RATE = 192.55
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 70 RATE = 187.99
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 71 RATE = 182.95
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 72 RATE = 177.54
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 73 RATE = 171.86
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 74 RATE = 165.99
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 75 RATE = 160.03
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 76 RATE = 154.05
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 77 RATE = 148.06
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 78 RATE = 142.10
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 79 RATE = 136.17
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS, CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 80 RATE = 130.33

PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 19.13 MM
 PEAK DISCHARGE RATE = 17.235 CMS

 * GET INFLOW TO POINT -6-

 *-----
 * SUBAREA 5C

TIME=0.30 TIME=0.30 RATE=0.00 FDF=76.12 DF=1312 DCAF=1.14
F/DD=0.0 DPST=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LBI=550 MNI=0.013
SLP=1 LBP=550 MNP=0.25
-1

UNIT PEAK = .175 CMS
PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
STORAGE COEFF. SC = 6.91 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .035 CMS
PEAK INTENSITY(RAIN EXCESS) = 31.48 MM/HR
STORAGE COEFF. SC = 45.45 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 6.335 CMS RUNOFF VOLUME = 43.49 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .60

ADD HYD ID=2 HYD=261 IDI=1 IDII=6
PEAK FLOW = 23.453 CMS RUNOFF VOLUME = 19.98 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=2 HYD NO=261 ID I=1 ID II=6

X-----
* TOTAL OUTLET FROM SIDE POINT -6-
X-----

PRINT HYD ID=2 1

HYDROGRAPH FROM AREA 261

RUNOFF VOLUME = 19.98 MM
PEAK DISCHARGE RATE = 23.453 CMS

X-----
FINISH

```

**
**
** ANDREW BRODIE ASSOCIATES INC.
**
**
**
** ANDREW BRODIE & ASSOCIATES INC
**
**
XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
THE METRIC UNITS OPTION HAS BEEN SPECIFIED

```

START RAINFALL BEGINS AT 0.0 HRS

```

* COMMENTS
* RUISSEAU DES FEES
* 5 STRM
* POST-DEV COND.ALTERNATIVE -BETA- R E V I S E D
* DT=0.0833 NI=36
* FILE NAME FEES5F.0T7

```

```

*-----
* GET INFLOW TO THE POINT -A-
*-----
* SUBAREA 1
*-----

```

```

COMPUTE NASHYD ID=1 HYD=101 DT=0.0833 H DA=156.64 HECT AA=0.0 AB=0.0
CN=68 (A=2.5 MM N=3 TP=1.57 H NI=36
4.23 4.23 5.27 5.27 7.07 7.07 11.52 11.52 45.05 45.05
72.96 72.96 62.52 62.52 19.19 19.19 12.59 12.59 9.5 9.5
7.67 7.67 6.46 6.46 5.59 5.59 4.94 4.94 4.44 4.44
4.03 4.03 3.7 3.7 3.42 3.42

```

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 3.81 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = 1.652 CMS RUNOFF VOLUME = 12.71 MM TIME TO PEAK = 2.999 HRS
TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .26

PRINT HYD 10=1 1

HYDROGRAPH FROM AREA 101

RUNOFF VOLUME = 12.71 MM
PEAK DISCHARGE RATE = 1.652 CMS

```

*-----
* SUBAREA 2A
*-----

```

```

COMPUTE URSHYD ID=2 HYD=102 DT=0.0833 DA=299.12 CKK=1.0
XIMP=0.36 TIMP=0.36 NI=36 FD=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DFSP=4.67 STI=0.0 STP=0.0
SLI=1 LBI=1235 MNI=0.013
SLP=1 LBP=1235 MNP=0.25
-1

```

UNIT PEAK = .108 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 13.10 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .017 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 96.49 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 20.111 CMS RUNOFF VOLUME = 23.94 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .50

```

ADD HYD ID=4 HYD=412 IDI=1 IDII=2
PEAK FLOW = 20.238 CMS RUNOFF VOLUME = 20.08 MM TIME TO PEAK= 1.17 HOURS

```

ADD HYD ID=4 HYD NO=412 ID I=1 ID II=2

```

*-----
* INFLOW TO THE POINT -A-
*-----

```

PRINT HYD 10=4 1

HYDROGRAPH FROM AREA 412

RUNOFF VOLUME = 20.08 MM
PEAK DISCHARGE RATE = 20.238 CMS

 * ROUTING FROM THE POINT A TO POINT B
 *-----
 COMPUTE RATING CURVEID=1 VSN=1 NSEG=3 NINEL=0.0
 MAXEL=2.5
 CHSLP=0.0035
 FPSLP=0.0035

N=0.03 DIST=9.5 N=-0.02 DIST=16.5 N=0.03 DIST=26
 0 2.5 4.5 1.0
 9.5 1.0 11.5 0.0
 14.5 0.0 16.5 1.0
 21.5 1.0 26.0 2.5
 126 102.40 226 102.98

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
.00	.0	.0
.13	.4	.3
.26	.9	1.0
.39	1.5	2.0
.53	2.1	3.4
.66	2.8	5.1
.79	3.6	7.2
.92	4.5	9.7
1.05	5.9	12.9
1.18	8.2	17.8
1.32	10.7	23.8
1.45	13.2	30.8
1.58	15.8	38.9
1.71	18.6	47.8
1.84	21.4	57.7
1.97	24.4	68.4
2.11	27.5	80.1
2.24	30.6	92.8
2.37	33.9	106.3
2.50	37.2	120.7

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
 L=750 SLP=0.0035

TRAVEL TIME TABLE
 REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.2900
.26	1.	.1920
.39	2.	.1525
.53	3.	.1301
.66	5.	.1152
.79	7.	.1044
.92	10.	.0962
1.05	13.	.0954
1.18	18.	.0964
1.32	24.	.0933
1.45	31.	.0892
1.58	39.	.0850
1.71	48.	.0810
1.84	58.	.0775
1.97	68.	.0743
2.11	80.	.0714
2.24	93.	.0688
2.37	106.	.0664
2.50	121.	.0643

ROUTE ID=6 HYD=201
 INDI=4 DT= 0.08330
 PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 20.08 MM
 PEAK DISCHARGE RATE = 18.029 CMS

 * GET INFLOW TO POINT -B-
 *-----
 * SUBAREA 4A
 *-----
 COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=89.43 CKK=1.0
 T1MP=0.75 T2MP=0.75 NI=36 FO=76.12 FC=13.2 DCAY=4.14
 F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0

SLP=1 LRP=810 MNP=0.25

UNIT PEAK = .132 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 10.17 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .022 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 74.91 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 11.741 CMS RUNOFF VOLUME = 38.54 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .90

ADD HYD ID=3 HYD=342 IDI=6 IDII=2
PEAK FLOW = 29.585 CMS RUNOFF VOLUME = 23.11 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=3 HYD NG=342 ID I=6 ID II=2
*-----
* INFLOW TO THE POINT -B-
*-----
PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 342

RUNOFF VOLUME = 23.11 MM
PEAK DISCHARGE RATE = 29.585 CMS

*-----
* ROUTING FROM THE POINT B TO POINT C
*-----
COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=1300 SLP=0.0043

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.5027
.26	1.	.3327
.39	2.	.2643
.53	3.	.2254
.66	5.	.1997
.79	7.	.1810
.92	10.	.1667
1.05	13.	.1654
1.18	18.	.1672
1.32	24.	.1618
1.45	31.	.1546
1.58	39.	.1473
1.71	48.	.1405
1.84	58.	.1343
1.97	68.	.1287
2.11	80.	.1237
2.24	93.	.1192
2.37	106.	.1151
2.50	121.	.1114

ROUTE ID=6 HYD=201
INDI=3 DT= 0.08330
PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 23.11 MM
PEAK DISCHARGE RATE = 25.272 CMS

*-----
* GET INFLOW TO POINT -C-
*-----
* SUBAREA 3A
*-----
COMPUTE NASHYD ID=1 HYD=103 DT=0.0833 H DA=98.38 HECT AA=0.0 AB=0.0

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 3.21 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = 1.288 CMS RUNOFF VOLUME = 12.71 MM TIME TO PEAK = 2.499 HRS
TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .26

*-----
* SUBAREA 28
*-----

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=23.23 CRK=1.0
XIMP=0.36 TIMP=0.36 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LBI=395 MNI=0.013
SLP=1 LBP=395 MNP=0.25

UNIT PEAK = .180 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 6.61 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .033 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 48.89 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 1.880 CMS RUNOFF VOLUME = 23.95 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .50

ADD HYD ID=3 HYD=312 IDI=1 IDII=2
PEAK FLOW = 2.048 CMS RUNOFF VOLUME = 14.85 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2
ADD HYD ID=1 HYD=163 IDI=6 IDII=3
PEAK FLOW = 26.834 CMS RUNOFF VOLUME = 21.60 MM TIME TO PEAK= 1.25 HOURS

ADD HYD ID=1 HYD NO=163 ID I=6 ID II=3

*-----
* SUBAREA 48
*-----

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=191 CRK=1.0
XIMP=0.75 TIMP=0.75 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LBI=1128 MNI=0.013
SLP=1 LBP=1128 MNP=0.25

UNIT PEAK = .113 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 12.40 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .018 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 91.38 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 24.005 CMS RUNOFF VOLUME = 38.54 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .80

ADD HYD ID=3 HYD=312 IDI=1 IDII=2
PEAK FLOW = 49.177 CMS RUNOFF VOLUME = 25.37 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2

*-----
* INFLOW TO POINT -C-
*-----

PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 312

RUNOFF VOLUME = 25.37 MM
PEAK DISCHARGE RATE = 49.177 CMS

*-----

COMPUTE TRAVEL TIME ID=6 REACH=1 NV5=1
L=750 SLP=0.008

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.2900
.26	1.	.1920
.39	2.	.1525
.53	3.	.1301
.66	5.	.1152
.79	7.	.1044
.92	10.	.0962
1.05	13.	.0954
1.18	18.	.0964
1.32	24.	.0933
1.45	31.	.0892
1.58	39.	.0850
1.71	48.	.0810
1.84	58.	.0775
1.97	68.	.0743
2.11	80.	.0714
2.24	93.	.0688
2.37	106.	.0664
2.50	121.	.0643

ROUTE ID=6 HYD=201
INDI=3 DT= 0.08330
PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 25.37 MM
PEAK DISCHARGE RATE = 46.767 CMS

*-----
* SET INFLOW TO POINT -D- (S W M POND)
*-----

* SUBAREA 3B

COMPUTE NASHYD ID=1 HYD=103 DT=0.0833 H DA=95.17 HECT AA=0.0 AB=0.0
CN=68 IA=2.5 MM N=3 TP=1.50 H NI=36

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 2.42 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = 1.038 CMS RUNOFF VOLUME = 12.71 MM TIME TO PEAK = 2.916 HRS
TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .26

*-----
* SUBAREA 4C

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=77.71 CCK=1.0
XIMP=0.45 TIMP=0.45 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LGI=719 MNI=0.013
SLP=1 LGP=719 MNP=0.25

UNIT PEAK = .139 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 9.47 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .024 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 69.74 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 6.824 CMS RUNOFF VOLUME = 27.31 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .57

ADD HYD ID=3 HYD=216 IDI=1 IDII=2
PEAK FLOW = 5.911 CMS RUNOFF VOLUME = 19.27 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=3 HYD NO=216 ID I=1 ID II=2

PEAK FLOW = 51.997 CMS RUNOFF VOLUME = 24.35 MM TIME TO PEAK = 1.25 HOURS

ADD HYD ID=1 HYD NO=216 ID 1=6 ID 11=3

 * INFLOW TO S W M POND)
 *-----

PRINT HYD ID=1 1

HYDROGRAPH FROM AREA 216

RUNOFF VOLUME = 24.35 MM
 PEAK DISCHARGE RATE = 51.997 CMS

ROUTE RESERVOIR ID=5 500 1
 DISCHARGE STORAGE
 0.0 0.0
 3.0 4.2
 6.2 7.7
 9.0 23.1
 13.0 29.56

PEAK DISCHARGE = 7.6418 CMS RUNOFF VOLUME = 24.2581 MM

PRINT HYD ID=5 1

HYDROGRAPH FROM AREA 500

RUNOFF VOLUME = 24.26 MM
 PEAK DISCHARGE RATE = 7.642 CMS

 * OUTFLOW FROM S W M POND (POINT -D-))
 *-----

 * ROUTING FROM THE POINT D TO POINT E)
 *-----

 * ROUTING - X SECTION #2)
 *-----

COMPUTE RATING CURVE ID=1 VSN=1 NSE6=1 NINEL=90.58
 MAXEL=92.84
 CHSLP=0.0041
 FPSLP=0.0041

N=0.03 DIST=18

0.0	92.84	1.0	92.84
2.0	92.24	4.0	92.24
7.4	90.96	8.0	90.58
10	90.58	10.4	91.28
14	92.32	16	92.32
17	92.84	18	92.84

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
90.58	.0	.0
90.70	.3	.1
90.82	.5	.4
90.94	.9	.8
91.06	1.2	1.2
91.17	1.6	1.8
91.29	2.0	2.6
91.41	2.5	3.3
91.53	3.1	4.3
91.65	3.8	5.6
91.77	4.6	7.0
91.89	5.5	8.8
92.01	6.4	10.8
92.13	7.4	13.1
92.25	8.6	14.1
92.36	10.1	16.3
92.48	11.6	20.8
92.60	13.6	25.8
92.72	15.4	31.2
92.84	17.3	34.4

COMPUTE TRAVEL TIME ID=3 REACH=1 NVS=1
 L=1350 SLP=0.0041

TRAVEL TIME TABLE
 REACH 1.0

DEPTH METRES	RATE CMS	TIME HRS
.12	0.	.7780
.24	0.	.5181
.36	1.	.4140
.48	1.	.3606
.59	2.	.3245
.71	3.	.2987
.83	3.	.2856
.95	4.	.2716
1.07	5.	.2579
1.19	7.	.2450
1.31	9.	.2331
1.43	11.	.2223
1.55	13.	.2123
1.67	14.	.2278
1.78	16.	.2313
1.90	21.	.2126
2.02	26.	.1977
2.14	31.	.1853
2.26	34.	.1883

ROUTE ID=3 HYD=201
 INDI=5 DT= 0.08330
 PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 24.24 MM
 PEAK DISCHARGE RATE = 7.631 CMS

*-----
 * GET INFLOW TO POINT -E-
 *-----
 * SUBAREA 5A
 *-----

COMPUTE URBHYD ID=1 HYD=102 DT=0.0833 DA=62.5 CKK=1.0
 YIMP=0.45 TIMP=0.45 NI=36-FO=76.12 FC=13.2 DCAY=4.14
 F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
 SLP=1 LGI=645 MNI=0.013
 SLP=1 LBP=645 MNF=0.25

UNIT PEAK = .146 CMS
 PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
 STORAGE COEFF. SC = 8.87 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .025 CMS
 PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
 STORAGE COEFF. SC = 65.34 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 5.569 CMS RUNOFF VOLUME = 27.31 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .57

*-----
 * INFLOW TO POINT -E-
 *-----
 PRINT HYD ID=1 1

HYDROGRAPH FROM AREA 102

RUNOFF VOLUME = 27.31 MM
 PEAK DISCHARGE RATE = 5.569 CMS

*-----
 * ROUTING FROM THE POINT E TO POINT F
 *-----
 * ROUTING - X SECTION #1
 *-----

COMPUTE RATING CURVEID=1 VSN=1 NSEG=1 NINEL=87.47
 MAXEL=89.90
 CHSLP=0.0054
 FPSLP=0.0054

N=0.03 DIST=18

2.0	89.27	9.0	89.27
9.8	87.47	12.2	87.47
18.	89.21	16.	89.39
20.	85.40	21.0	89.96
22	89.90		

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
87.47	.0	.0
87.50	.3	.2
87.73	.6	.6
87.85	1.0	1.1
87.96	1.3	1.7
88.11	1.7	2.5
88.24	2.1	3.3
88.37	2.5	4.3
88.49	2.9	5.3
88.62	3.4	6.4
88.75	3.8	7.6
88.88	4.3	8.9
89.00	4.7	10.2
89.13	5.2	11.7
89.26	5.8	12.3
89.39	7.4	10.5
89.52	9.7	14.3
89.64	12.0	20.4
89.77	14.4	27.3
89.90	16.9	34.1

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=900 SLP=0.0054

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.4259
.26	1.	.2823
.38	1.	.2254
.51	2.	.1938
.64	2.	.1732
.77	3.	.1586
.90	4.	.1475
1.02	5.	.1388
1.15	6.	.1317
1.28	8.	.1257
1.41	9.	.1206
1.53	10.	.1162
1.66	12.	.1123
1.79	12.	.1174
1.56	11.	.1152
2.05	14.	.1697
2.17	20.	.1478
2.30	27.	.1320
2.43	34.	.1236

ROUTE ID=6 HYD=201
INDI=3 DT= 0.08330
PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 24.22 MM
PEAK DISCHARGE RATE = 7.628 CMS

* GET INFLOW TO POINT -F-

* SUBAREA 58

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=77.8 CCK=1.0
XIMP=0.45 TIMP=0.45 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LGI=720 MNI=0.013
SLP=1 LBP=720 MNP=0.25

-1
UNIT PEAK = .139 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 9.47 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .023 CMS
 PEAK INTENSITY (RAIN EXCESS) = 41.75 MM/HR
 STORAGE COEFF. SC = 69.80 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 46.34 MM

PEAK DISCHARGE = 6.830 CMS RUNOFF VOLUME = 27.31 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .57

ADD HYD ID=4 HYD=261 IDI=1 IDII=2
 PEAK FLOW = 12.400 CMS RUNOFF VOLUME = 27.31 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=4 HYD NO=261 ID I=1 ID II=2
 ROUTE RESERVOIR ID=1 500.4
 DISCHARGE STORAGE
 0.0 0.0
 0.8 1.16
 1.5 2.24
 2.0 3.74
 3.2 4.56

PEAK DISCHARGE = 1.6159 CMS RUNOFF VOLUME= 27.2252 MM
 ADD HYD ID=2 HYD=261 IDI=1 IDII=3
 PEAK FLOW = 9.184 CMS RUNOFF VOLUME = 24.59 MM TIME TO PEAK= 3.25 HOURS

ADD HYD ID=2 HYD NO=261 ID I=1 ID II=3

*-----
 * INFLOW TO POINT -F-
 *-----
 PRINT HYD ID=2 1

HYDROGRAPH FROM AREA 261

RUNOFF VOLUME = 24.59 MM
 PEAK DISCHARGE RATE = 9.184 CMS

*-----
 * ROUTING FROM THE POINT F TO POINT 6
 *-----
 * ARTIFICIAL CHANNEL
 *-----

COMPUTE RATING CURVE ID=1 VSN=1 NSEG=1 NINEL=84.30
 MAXEL=87.00
 CHSLP=0.0004
 FPSLP=0.0004

N=0.035 DIST=24.
 0.0 87.00 4.0 85.3
 6.5 85.3 8. 84.3
 16.0 84.3 17.5 85.3
 20.0 85.3 24.0 87.00

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
84.30	.0	.0
84.44	1.2	.2
84.58	2.4	.6
84.73	3.7	1.1
84.87	5.0	1.8
85.01	6.4	2.6
85.15	7.9	3.6
85.29	9.4	4.7
85.44	11.7	5.2
85.58	14.1	6.9
85.72	16.7	8.8
85.86	19.3	10.9
86.01	22.0	13.3
86.15	24.7	15.8
86.29	27.6	18.6
86.43	30.6	21.6
86.57	33.7	24.8
86.72	36.9	28.2
86.86	40.1	31.8
87.00	43.5	35.7

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
 L=600 SLP=0.0004

TRAVEL TIME TABLE
 REACH 1.0

DEPTH METRES	TIME CMS	TIME HRS
.14	0.	1.0967
.28	1.	.7062
.43	1.	.5499
.57	2.	.4625
.71	3.	.4055
.85	4.	.3649
.99	5.	.3342
1.14	5.	.3778
1.28	7.	.3428
1.42	9.	.3157
1.56	11.	.2939
1.71	13.	.2760
1.85	16.	.2609
1.99	19.	.2479
2.13	22.	.2367
2.27	25.	.2268
2.42	28.	.2181
2.56	32.	.2102
2.70	36.	.2032

```

ROUTE      ID=6  HYD=201
           INDI=2 DT= 0.08330
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 20RATE = 172.52
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 21RATE = 196.43
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 110RATE = 189.14
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 111RATE = 186.33
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 112RATE = 183.22
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 113RATE = 179.89
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 114RATE = 176.40
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 115RATE = 172.79
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 116RATE = 169.12
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 117RATE = 165.42
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 118RATE = 161.71
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 119RATE = 158.01
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 120RATE = 154.34
PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS, CONVERGENCE WAS FORCED.
  OUTFLOW NUMBER = 121RATE = 150.70

```

PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 24.55 MM
PEAK DISCHARGE RATE = 9.032 CMS

```

*-----*
* GET INFLOW TO POINT -6-
*-----*
* SUBAREA 5C
*-----*

```

```

COMPUTE URBHYD  ID=1 HYD=102 DT=0.0833 DA=45.5 CCK=1.0
                 XIMP=0.30 TIMP=0.30 NI=36 FO=76.12 FC=13.2 DCAY=4.14
                 F/DD=0.0 DPSP=1.57 DPSP=4.67 STI=0.0 STP=0.0
                 SLP=1 L6I=550 MNI=0.013
                 SLP=1 L6P=550 MNP=0.25
                 -1

```

UNIT PEAK = .157 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 8.06 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .027 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 59.39 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 9.032 CMS NUMBER OF PEAKS = 1 TIME TO PEAK = 1.000 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .45

ROUTE RESERVOIR	ID=5 500 1	DISCHARGE	STORAGE
		0.0	0.0
		1.0	0.19
		2.1	0.29
		3.0	0.36
		5.0	0.48

PEAK DISCHARGE = 1.9846 CMS RUNOFF VOLUME= 21.6976 MM

*
PRINT HYD ID=5 1

HYDROGRAPH FROM AREA 500

RUNOFF VOLUME = 21.70 MM
PEAK DISCHARGE RATE = 1.985 CMS

ADD HYD ID=2 HYD=261 ID1=5 ID11=6
PEAK FLOW = 9.336 CMS RUNOFF VOLUME = 24.44 MM TIME TO PEAK= 3.25 HOURS

ADD HYD ID=2 HYD NU=261 ID I=5 ID II=6

x-----
x TOTAL OUTLET FROM SIDE POINT -6-
x-----

PRINT HYD ID=2 1

HYDROGRAPH FROM AREA 261

RUNOFF VOLUME = 24.44 MM
PEAK DISCHARGE RATE = 9.336 CMS

x-----
FINISH

87.98	1.3	1.7
88.11	1.7	2.5
88.24	2.1	3.3
88.37	2.5	4.3
88.49	2.9	5.3
88.62	3.4	6.4
88.75	3.8	7.6
88.88	4.3	8.9
89.00	4.7	10.2
89.13	5.2	11.7
89.26	5.8	12.3
89.39	7.4	10.5
89.52	9.7	14.3
89.64	12.0	20.4
89.77	14.4	27.3
89.90	16.9	34.1

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=900 SLP=0.0054

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.4259
.26	1.	.2823
.38	1.	.2254
.51	2.	.1938
.64	2.	.1732
.77	3.	.1586
.90	4.	.1475
1.02	5.	.1388
1.15	6.	.1317
1.28	8.	.1257
1.41	9.	.1206
1.53	10.	.1162
1.66	12.	.1123
1.79	12.	.1174
1.56	11.	.1152
2.05	14.	.1697
2.17	20.	.1478
2.30	27.	.1320
2.43	34.	.1236

ROUTE ID=6 HYD=201
INDI=2 DT= 0.08330
PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 24.40 MM
PEAK DISCHARGE RATE = 8.038 CMS

*-----
* GET INFLOW TO POINT -F-
*-----
*
* SUBAREA 5B
*-----
*

COMPUTE URBHYD ID=1 HYD=102 DT=0.0833 DA=77.8 CCK=1.0
XIMP=0.45 TIMP=0.45 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPS1=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LGI=720 MNI=0.013
SLP=1 LGP=720 MNP=0.25

-1
UNIT PEAK = .139 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 9.47 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .023 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 69.80 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 6.830 CMS RUNOFF VOLUME = 27.31 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .57

ADD HYD ID=2 HYD=261 IDI=1 IDII=6
PEAK FLOW = 12.573 CMS RUNOFF VOLUME = 24.59 MM TIME TO PEAK= 1.17 HOURS
ADD HYD ID=2 HYD NO=261 ID I=1 ID II=6

*-----
*


```

**                               ANDREW BRODIE ASSOCIATES INC.                               **
**                                                                                       **
**                                                                                       **
**                                                                                       **
**                                                                                       **
**ANDREW BRODIE & ASSOCIATES INC**
**                                                                                       **
**                                                                                       **
XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
THE METRIC UNITS OPTION HAS BEEN SPECIFIED

```

START RAINFALL BEGINS AT 0.0 HRS

```

* COMMENTS
* RUISSEAU DES FEES
* 100 STROM
* POST-DEV COND.ALTERNATIVE -BETA- R E V I S E D
* DT=0.0833 NI=36
* FILE NAME FEES100F.DT7

```

*-----
* GET INFLOW TO THE POINT -A-
*-----

* SUBAREA 1

```

*-----
COMPUTE NASHYD ID=1 HYD=101 DT=0.0833 H DA=156.64 HECT AA=0.0 AB=0.0
CN=68 IA=2.5 MM N=3 TP=1.57 H NI=36
4.92 4.92 6.35 6.35 8.95 8.95 18.54 18.54 78.42 78.42
107.19 107.19 99.64 99.64 31.1 31.1 17.51 17.51 12.65
12.65 9.95 9.85 8.05 8.05 6.81 6.81 5.89 5.89 5.2 5.2
4.65 4.65 4.21 4.21 3.85 3.85

```

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 3.81 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = 3.423 CMS RUNOFF VOLUME = 25.71 MM TIME TO PEAK = 2.916 HRS
TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .36

PRINT HYD ID=1 1

HYDROGRAPH FROM AREA 101

RUNOFF VOLUME = 25.71 MM
PEAK DISCHARGE RATE = 3.423 CMS

*-----

* SUBAREA 2A

```

*-----
COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=299.12 CKK=1.0
IIMP=0.36 TIMP=0.36 NI=36 FO=78.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSF=4.67 STI=0.0 STP=0.0
SLI=1 LGI=1235 MNI=0.013
SLP=1 L6P=1235 MNP=0.25

```

UNIT PEAK = .122 CMS
PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
STORAGE COEFF. SC = 11.23 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .022 CMS
PEAK INTENSITY(RAIN EXCESS) = 81.48 MM/HR
STORAGE COEFF. SC = 73.85 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 72.27 MM
PEAK DISCHARGE = 38.319 CMS RUNOFF VOLUME = 45.90 MM TIME TO PEAK = 1.166 HRS
RUNOFF VOLUMETRIC COEFFICIENT = .64

ADD HYD ID=4 HYD=412 IDI=1 IDII=2
PEAK FLOW = 38.626 CMS RUNOFF VOLUME = 38.96 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=4 HYD NO=412 ID I=1 ID II=2

*-----
* INFLOW TO THE POINT -A-
*-----

PRINT HYD ID=4 1

HYDROGRAPH FROM AREA 412

RUNOFF VOLUME = 38.97 MM
PEAK DISCHARGE RATE = 38.626 CMS

 * ROUTING FROM THE POINT A TO POINT B

COMPUTE RATING CURVEID=1 VSN=1 NSE6=3 NINEL=0.0
 MAXEL=2.5
 CHSLP=0.0035
 FPSLP=0.0035
 N=0.03 DIST=9.5 N=-0.02 DIST=16.5 N=0.03 DIST=26
 0 2.5 4.5 1.0
 9.5 1.0 11.5 0.0
 14.5 0.0 16.5 1.0
 21.5 1.0 26.0 2.5
 126 102.40 226 102.98

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
.00	.0	.0
.13	.4	.3
.26	.9	1.0
.39	1.5	2.0
.53	2.1	3.4
.66	2.8	5.1
.79	3.6	7.2
.92	4.5	9.7
1.05	5.9	12.9
1.18	8.2	17.8
1.32	10.7	23.8
1.45	13.2	30.8
1.58	15.8	38.9
1.71	18.6	47.8
1.84	21.4	57.7
1.97	24.4	68.4
2.11	27.5	80.1
2.24	30.6	92.8
2.37	33.9	106.3
2.50	37.2	120.7

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
 L=750 SLP=0.0035

TRAVEL TIME TABLE
 REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.2900
.26	1.	.1920
.39	2.	.1525
.53	3.	.1301
.66	5.	.1152
.79	7.	.1044
.92	10.	.0962
1.05	13.	.0954
1.18	18.	.0964
1.32	24.	.0933
1.45	31.	.0892
1.58	39.	.0850
1.71	48.	.0810
1.84	58.	.0775
1.97	68.	.0743
2.11	80.	.0714
2.24	93.	.0688
2.37	106.	.0664
2.50	121.	.0643

ROUTE ID=6 HYD=201
 INDI=4 DT= 0.08330
 PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 38.97 MM
 PEAK DISCHARGE RATE = 35.115 CMS

 * GET INFLOW TO POINT -B-

* SUBAREA 4A

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=89.43 CCK=1.0
 XIMP=0.75 TIMP=0.75 NI=36 FO=76.12 FC=13.2 DCAY=4.14
 F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 3.21 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = 2.719 CMS RUNOFF VOLUME = 25.71 MM TIME TO PEAK = 2.416 HRS
TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .36

*-----
* SUBAREA 2B
*-----

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=28.25 CCK=1.0
XIMP=0.36 TIMP=0.36 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LGI=395 MNI=0.013
SLP=1 LGP=395 MNP=0.25

-1
UNIT PEAK = .199 CMS
PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
STORAGE COEFF. SC = 5.67 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .043 CMS
PEAK INTENSITY(RAIN EXCESS) = 81.48 MM/HR
STORAGE COEFF. SC = 37.26 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 3.721 CMS RUNOFF VOLUME = 45.92 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .64

ADD HYD ID=3 HYD=312 IDI=1 IDII=2
PEAK FLOW = 4.124 CMS RUNOFF VOLUME = 29.57 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2
ID=1 HYD=163 IDI=6 IDII=3
PEAK FLOW = 51.591 CMS RUNOFF VOLUME = 40.30 MM TIME TO PEAK= 1.25 HOURS

ADD HYD ID=1 HYD NO=163 ID I=6 ID II=3

*-----
* SUBAREA 4B
*-----

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=191 CCK=1.0
XIMP=0.75 TIMP=0.75 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LGI=1128 MNI=0.013
SLP=1 LGP=1128 MNP=0.25

-1
UNIT PEAK = .127 CMS
PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
STORAGE COEFF. SC = 10.63 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .023 CMS
PEAK INTENSITY(RAIN EXCESS) = 81.48 MM/HR
STORAGE COEFF. SC = 69.94 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 40.276 CMS RUNOFF VOLUME = 61.70 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .85

ADD HYD ID=3 HYD=312 IDI=1 IDII=2
PEAK FLOW = 89.047 CMS RUNOFF VOLUME = 45.07 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2

*-----
* INFLOW TO POINT -C-
*-----

PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 312

RUNOFF VOLUME = 45.07 MM
PEAK DISCHARGE RATE = 89.047 CMS

*-----

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=750 SLP=0.008

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.2900
.26	1.	.1920
.39	2.	.1525
.53	3.	.1301
.66	5.	.1152
.79	7.	.1044
.92	10.	.0962
1.05	13.	.0954
1.18	18.	.0964
1.32	24.	.0933
1.45	31.	.0892
1.58	39.	.0850
1.71	48.	.0810
1.84	58.	.0775
1.97	68.	.0743
2.11	80.	.0714
2.24	93.	.0688
2.37	106.	.0664
2.50	121.	.0643

ROUTE ID=6 HYD=201
INDI=3 DT= 0.08330
PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 45.07 MM
PEAK DISCHARGE RATE = 85.277 CMS

*-----
* GET INFLOW TO POINT -D- (S W M POND)
*-----

* SUBAREA 38
*-----

COMPUTE WASHYD ID=1 HYD=103 DT=0.0833 H DA=95.17 HECT AA=0.0 AB=0.0
CN=68 IA=2.5 MM N=3 TP=1.50 H NI=36

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 2.42 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 42.00
PEAK DISCHARGE = 2.157 CMS RUNOFF VOLUME = 25.71 MM TIME TO PEAK = 2.832 HRS
TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .36

*-----
* SUBAREA 40
*-----

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=77.71 CCK=1.0
XIMP=0.45 TIMP=0.45 NI=36 FD=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LGI=719 MNI=0.013
SLP=1 L6P=719 MNP=0.25

UNIT PEAK = .156 CMS
PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
STORAGE COEFF. SC = 8.12 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .030 CMS
PEAK INTENSITY(RAIN EXCESS) = 81.48 MM/HR
STORAGE COEFF. SC = 53.38 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 12.551 CMS RUNOFF VOLUME = 49.56 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .69

ADD HYD ID=3 HYD=216 IDI=1 IDII=2
PEAK FLOW = 12.760 CMS RUNOFF VOLUME = 36.43 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=3 HYD NO=216 ID I=1 ID II=2

SLP=1 LQF=610 MNP=0.25
 -1
 UNIT PEAK = .148 CMS
 PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
 STORAGE COEFF. SC = 8.72 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .028 CMS
 PEAK INTENSITY(RAIN EXCESS) = 81.48 MM/HR
 STORAGE COEFF. SC = 57.34 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 19.604 CMS RUNOFF VOLUME = 61.71 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .85

ADD HYD ID=3 HYD=342 IDI=6 IDII=2
 PEAK FLOW = 54.719 CMS RUNOFF VOLUME = 42.69 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=3 HYD NO=342 ID I=6 ID II=2

*-----
 * INFLOW TO THE POINT -B-
 *-----
 PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 342

RUNOFF VOLUME = 42.70 MM
 PEAK DISCHARGE RATE = 54.719 CMS

*-----
 * ROUTING FROM THE POINT B TO POINT C
 *-----
 COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
 L=1300 SLP=0.0043

TRAVEL TIME TABLE
 REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.5027
.26	1.	.3327
.39	2.	.2643
.53	3.	.2254
.66	5.	.1997
.79	7.	.1810
.92	10.	.1667
1.05	13.	.1654
1.18	18.	.1672
1.32	24.	.1618
1.45	31.	.1546
1.58	39.	.1473
1.71	48.	.1405
1.84	58.	.1343
1.97	68.	.1287
2.11	80.	.1237
2.24	93.	.1192
2.37	106.	.1151
2.50	121.	.1114

ROUTE ID=6 HYD=201
 INDI=3 DT= 0.08330
 PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 42.70 MM
 PEAK DISCHARGE RATE = 48.297 CMS

*-----
 * GET INFLOW TO POINT -L-
 *-----
 * SUBAREA 3A
 *-----
 COMPUTE NASHYD ID=1 HYD=103 DT=0.0833 H DA=98.38 HECT AA=0.0 AB=0.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.12	0.	.7780
.24	0.	.5181
.36	1.	.4140
.48	1.	.3606
.59	2.	.3245
.71	3.	.2987
.83	3.	.2856
.95	4.	.2716
1.07	6.	.2579
1.19	7.	.2450
1.31	9.	.2331
1.43	11.	.2223
1.55	13.	.2123
1.67	14.	.2278
1.78	16.	.2313
1.90	21.	.2126
2.02	26.	.1977
2.14	31.	.1853
2.26	34.	.1883

ROUTE ID=3 HYD=201
 INDI=5 DT= 0.08330
 PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 43.29 MM
 PEAK DISCHARGE RATE = 12.997 CMS

*-----
 * GET INFLOW TO POINT -E-
 *-----
 * SUBAREA SA
 *-----

COMPUTE URBHYD ID=1 HYD=102 DT=0.0833 DA=62.5 CCK=1.0
 YIMP=0.45 TIMP=0.45 NI=36 FO=76.12 FC=13.2 DCAY=4.14
 F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
 SLP=1 LBP=645 MNP=0.013
 SLP=1 LBP=645 MNP=0.25

UNIT PEAK = .164 CMS
 PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
 STORAGE COEFF. SC = 7.60 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .032 CMS
 PEAK INTENSITY(RAIN EXCESS) = 81.48 MM/HR
 STORAGE COEFF. SC = 50.01 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 10.270 CMS RUNOFF VOLUME = 49.56 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .69

*-----
 * INFLOW TO POINT -E-
 *-----
 PRINT HYD ID=1 1

HYDROGRAPH FROM AREA 102

RUNOFF VOLUME = 49.56 MM
 PEAK DISCHARGE RATE = 10.270 CMS

*-----
 * ROUTING FROM THE POINT E TO POINT F
 *-----
 * ROUTING - X SECTION #1
 *-----
 COMPUTE RATING CURVEID=1 VSN=1 NSEG=1 NINEL=87.47
 MAXEL=89.90
 CHRI P=0.0054

N=0.03 DIST=18
 0.0 89.90 1. 89.90
 2.0 89.27 3.0 89.27
 9.8 87.47 12.2 87.47
 13. 89.21 16. 89.39
 20. 89.40 21.0 89.90
 22 89.90

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
87.47	.0	.0
87.60	.3	.2
87.73	.6	.6
87.85	1.0	1.1
87.98	1.3	1.7
88.11	1.7	2.5
88.24	2.1	3.3
88.37	2.5	4.3
88.49	2.9	5.3
88.62	3.4	6.4
88.75	3.8	7.6
88.88	4.3	8.9
89.00	4.7	10.2
89.13	5.2	11.7
89.26	5.8	12.3
89.39	7.4	10.5
89.52	9.7	14.3
89.64	12.0	20.4
89.77	14.4	27.3
89.90	16.9	34.1

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
 L=900 SLP=0.0054

TRAVEL TIME TABLE
 REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.4259
.26	1.	.2823
.38	1.	.2254
.51	2.	.1938
.64	2.	.1732
.77	3.	.1586
.90	4.	.1475
1.02	5.	.1388
1.15	6.	.1317
1.28	8.	.1257
1.41	9.	.1206
1.53	10.	.1162
1.66	12.	.1123
1.79	12.	.1174
1.56	11.	.1152
2.05	14.	.1697
2.17	20.	.1478
2.30	27.	.1320
2.43	34.	.1236

ROUTE ID=6 HYD=201
 INDI=3 DT= 0.08330
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 40RATE = 440.74
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 43RATE = 448.54
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 60RATE = 427.52
 PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 43.25 MM
 PEAK DISCHARGE RATE = 12.846 CMS

*-----
 * GET INFLOW TO POINT -F-
 *-----

* SUBAREA 58

*-----
 COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=77.8 CKK=1.0
 XIMP=0.45 TIMP=0.45 NI=36 FO=76.12 FC=13.2 DCAY=4.14
 F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0

SLP=1 L6P=720 MNP=0.25

UNIT PEAK = .156 CMS
PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
STORAGE COEFF. SC = 0.12 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .030 CMS
PEAK INTENSITY(RAIN EXCESS) = 81.48 MM/HR
STORAGE COEFF. SC = 53.42 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 12.562 CMS RUNOFF VOLUME = 49.56 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .69

ADD HYD ID=4 HYD=261 IDI=1 IDII=2
PEAK FLOW = 22.833 CMS RUNOFF VOLUME = 49.56 MM TIME TO PEAK= 1.17 HOURS

ADD HYD	ID=4	HYD NO=261	ID I=1	ID II=2
ROUTE RESERVOIR	ID=1 300 4			
	DISCHARGE	STORAGE		
	0.0	0.0		
	0.8	1.16		
	1.5	2.24		
	2.0	3.74		
	3.2	4.56		

STORAGE-DISCHARGE TABLE EXCEEDED.

PEAK DISCHARGE = 3.3355 CMS RUNOFF VOLUME= 49.3889 MM

ADD HYD ID=2 HYD=261 IDI=1 IDII=3
PEAK FLOW = 15.732 CMS RUNOFF VOLUME = 44.02 MM TIME TO PEAK= 3.17 HOURS

ADD HYD ID=2 HYD NO=261 ID I=1 ID II=3

*
*-----
* INFLOW TO POINT F-
*-----

PRINT HYD ID=2 1

HYDROGRAPH FROM AREA 261

RUNOFF VOLUME = 44.02 MM
PEAK DISCHARGE RATE = 15.732 CMS

*-----
* ROUTING FROM THE POINT F TO POINT G
*-----
* ARTIFICIAL CHANNEL
*-----

COMPUTE RATING CURVE ID=1 VSN=1 NSEG=1 NINEL=84.30
MAXEL=87.00
CHSLP=0.0004
FPSLP=0.0004

N=0.035	DIST=24.		
0.0	87.00	4.0	85.3
6.5	85.3	8.	84.3
16.0	84.3	17.5	85.3
20.0	85.3	24.0	87.00

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
84.30	.0	.0
84.44	1.2	.2
84.58	2.4	.6
84.73	3.7	1.1
84.87	5.0	1.8
85.01	6.4	2.6
85.15	7.9	3.5
85.29	9.4	4.7
85.44	11.7	5.2
85.58	14.1	6.9
85.72	16.7	8.8
85.86	19.3	10.9
86.01	22.0	13.3
86.15	24.7	15.8
86.29	27.6	18.6
86.43	30.6	21.6

86.12 36.7 28.4
 86.86 40.1 31.8
 87.00 43.5 35.7

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
 L=600 SLP=0.0004

TRAVEL TIME TABLE
 REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.14	0.	1.0967
.28	1.	.7062
.43	1.	.5499
.57	2.	.4625
.71	3.	.4055
.85	4.	.3649
.99	5.	.3342
1.14	5.	.3778
1.28	7.	.3428
1.42	9.	.3157
1.56	11.	.2939
1.71	13.	.2760
1.85	15.	.2609
1.99	19.	.2479
2.13	22.	.2367
2.27	25.	.2268
2.42	28.	.2181
2.56	32.	.2102
2.70	36.	.2032

ROUTE ID=6 HYD=201
 INDI=2 DT= 0.08330

PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 18RATE = 189.53
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 162RATE = 184.77
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 163RATE = 182.26
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 164RATE = 179.39
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 165RATE = 176.23
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 166RATE = 172.87
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 167RATE = 169.37
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 168RATE = 165.77
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 169RATE = 162.11
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 170RATE = 158.43
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 171RATE = 154.74
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 172RATE = 151.08
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 173RATE = 147.44

PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 43.93 MM
 PEAK DISCHARGE RATE = 15.349 CMS

*-----
 * GET INFLOW TO POINT -6-
 *-----
 *-----
 * SUBAREA 5C
 *-----

COMPUTE URBHYD ID=1 HYD=102 DT=0.0833 DA=45.5 CKK=1.0
 YIMP=0.30 TIMP=0.30 NI=36 FO=76.12 FC=13.2 DCAY=4.14
 F/DD=0.0 DPSP=1.57 DPSP=4.67 STI=0.0 STP=0.0
 SLI=1 LBI=550 MNI=0.013
 SLP=1 LSP=550 MNP=0.25

-1
 UNIT PEAK = .175 CMS
 PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
 STORAGE COEFF. SC = 6.91 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .175 CMS


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*****
**                                     **
**           M I C R O H Y M D --- 3   **
**                                     **
**           ( P . C . O T T H Y M D ) **
**                                     **
**           V E R S I O N 2.0+         **
**                                     **
**                                     **
**           ADAPTED FOR MICROCOMPUTER BY **
**                                     **
**           ANDREW BRODIE ASSOCIATES INC. **
**                                     **
**                                     **
**           **ANDREW BRODIE & ASSOCIATES INC **
**                                     **
*****
THE METRIC UNITS OPTION HAS BEEN SPECIFIED

```

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START                RAINFALL BEGINS AT 0.0 HRS
* COMMENTS
* RUISSEAU DES FEES
* 5 STROM
* POST-DEV COND.ALTERNATIVE -GAMA- R E V I S E D
* DT=0.0833 NI=36
* FILE NAME FEES5F.DT8

```

```

-----
* GET INFLOW TO THE POINT -A-
-----
* SUBAREA 1
-----

```

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COMPUTE NASHYD      ID=1 HYD=101 DT=0.0833 H DA=156.64 HECT AA=0.0 AB=0.0
                   CN=68 IA=2.5 MM N=3 TP=1.57 H NI=36
                   4.23 4.23 5.27 5.27 7.07 7.07 11.52 11.52 45.05 45.05
                   72.96 72.96 62.52 62.52 19.19 19.19 12.59 12.59 9.5 9.5
                   7.67 7.67 6.46 6.46 5.59 5.59 4.94 4.94 4.44 4.44
                   4.03 4.03 3.7 3.7 3.42 3.42

```

```

SHAPE CONSTANT, N = 3.00
UNIT PEAK = 3.81 CMS

```

```

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = 1.652 CMS RUNOFF VOLUME = 12.71 MM TIME TO PEAK = 2.999 HRS
TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .26

```

```

PRINT HYD          ID=1 1
                   HYDROGRAPH FROM AREA 101

```

```

RUNOFF VOLUME = 12.71 MM
PEAK DISCHARGE RATE = 1.652 CMS

```

```

-----
* SUBAREA 2A
-----

```

```

COMPUTE URBHYD     ID=2 HYD=102 DT=0.0833 DA=299.12 CKK=1.0
                   XIMP=0.36 TIMP=0.36 NI=36 FO=76.12 FC=13.2 DCAY=4.14
                   F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
                   SLI=1 L6I=1235 MNI=0.013
                   SLP=1 LGP=1235 MNP=0.25
                   -1

```

```

UNIT PEAK = .108 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 13.10 MINS

```

```

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

```

```

UNIT PEAK = .017 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 96.49 MINS

```

```

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

```

```

TOTAL RAINFALL = 48.34 MM

```

```

PEAK DISCHARGE = 20.111 CMS RUNOFF VOLUME = 23.94 MM TIME TO PEAK = 1.166 HRS

```

```

RUNOFF VOL. COEFFICIENT = .50

```

ADD HYD ID=4 HYD=412 IDI=1 IDII=2
 PEAK FLOW = 20.238 CMS RUNOFF VOLUME = 20.08 MM TIME TO PEAK= 1.17 HOURS
 ADD HYD ID=4 HYD NO=412 ID I=1 ID II=2

INFLOW TO THE POINT -A-

PRINT HYD ID=4 1

HYDROGRAPH FROM AREA 412

RUNOFF VOLUME = 20.08 MM
 PEAK DISCHARGE RATE = 20.238 CMS

ROUTING FROM THE POINT A TO POINT B

COMPUTE RATING CURVEID=1 VSN=1 NSEG=3 NINEL=0.0
 MAXEL=2.5
 CHSLP=0.0035
 FPSLP=0.0035
 N=0.03 DIST=9.5 N=-0.02 DIST=16.5 N=0.03 DIST=26
 0 2.5 4.5 1.0
 9.5 1.0 11.5 0.0
 14.5 0.0 16.5 1.0
 21.5 1.0 26.0 2.5
 126 102.40 226 102.98

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
.00	.0	.0
.13	.4	.3
.26	.9	1.0
.39	1.5	2.0
.53	2.1	3.4
.66	2.8	5.1
.79	3.6	7.2
.92	4.5	9.7
1.05	5.9	12.9
1.18	8.2	17.8
1.32	10.7	23.8
1.45	13.2	30.8
1.58	15.8	38.9
1.71	18.6	47.8
1.84	21.4	57.7
1.97	24.4	68.4
2.11	27.5	80.1
2.24	30.6	92.8
2.37	33.9	106.2
2.50	37.2	120.7

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
 L=750 SLP=0.0035

TRAVEL TIME TABLE REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.2900
.26	1.	.1920
.39	2.	.1525
.53	3.	.1301
.66	5.	.1152
.79	7.	.1044
.92	10.	.0962
1.05	13.	.0954
1.18	18.	.0964
1.32	24.	.0933
1.45	31.	.0892
1.58	39.	.0850
1.71	48.	.0810
1.84	58.	.0775
1.97	68.	.0743
2.11	80.	.0714
2.24	93.	.0688
2.37	106.	.0664
2.50	121.	.0643

ROUTE ID=6 HYD=201
 INDI=4 DT= 0.08330
 PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 20.08 MM
 PEAK DISCHARGE RATE = 18.029 CMS

```

-----
* GET INFLOW TO POINT -B-
-----
*
* SUBAREA 4A
-----

```

```

COMPUTE DRBHYD ID=2 HYD=102 DT=0.0833 DA=89.43 CRK=1.0
XIMP=0.75 TIMP=0.75 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LGI=810 MNI=0.013
SLP=1 LGP=810 MNP=0.25
-1

```

```

UNIT PEAK = .192 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 10.17 MINS

```

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

```

UNIT PEAK = .022 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 74.91 MINS

```

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 11.741 CMS RUNOFF VOLUME = 38.54 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .80

```

ADD HYD ID=3 HYD=342 IDI=6 IDII=2
PEAK FLOW = 29.585 CMS RUNOFF VOLUME = 23.11 MM TIME TO PEAK= 1.17 HOURS
ADD HYD ID=3 HYD NO=342 ID I=6 ID II=2

```

```

-----
* INFLOW TO THE POINT -B-
-----
*
PRINT HYD ID=3 1

```

HYDROGRAPH FROM AREA 342

```

RUNOFF VOLUME = 23.11 MM
PEAK DISCHARGE RATE = 29.585 CMS

```

```

-----
* ROUTING FROM THE POINT B TO POINT C
-----
*
COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=1300 SLP=0.0043

```

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.5027
.26	1.	.3327
.39	2.	.2643
.53	3.	.2254
.66	5.	.1997
.79	7.	.1810
.92	10.	.1667
1.05	13.	.1654
1.18	16.	.1672
1.32	24.	.1618
1.45	31.	.1546
1.58	39.	.1473
1.71	48.	.1405
1.84	58.	.1343
1.97	68.	.1287
2.11	80.	.1237
2.24	93.	.1192
2.37	106.	.1151
2.50	121.	.1114

```

ROUTE ID=6 HYD=201
INDI=3 DT= 0.08330
PRINT HYD ID=6 1

```

HYDROGRAPH FROM AREA 201

```

RUNOFF VOLUME = 23.11 MM
PEAK DISCHARGE RATE = 25.272 CMS

```

```

-----
* GET INFLOW TO POINT -C-
-----
*

```

* SUBAREA 3A

COMPUTE NASHYD ID=1 HYD=103 DT=0.0833 DA=98.36 HECT AA=0.0 AB=0.0
CN=83 IA=2.5 MM N=3 TP=1.17 H NI=36

SHAPE CONSTANT, N¹ = 3.00
UNIT PEAK = 3.21 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = 1.288 CMS RUNOFF VOLUME = 12.71 MM TIME TO PEAK = 2.499 HRS
TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .26

* SUBAREA 2B

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=23.23 CKK=1.0
XIMP=0.36 TIMP=0.36 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 L61=395 MNI=0.013
SLP=1 L6P=395 MNP=0.25

-1
UNIT PEAK = .180 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 6.61 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .033 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 48.89 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 1.880 CMS RUNOFF VOLUME = 23.95 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .50

ADD HYD ID=3 HYD=312 IDI=1 IDII=2
PEAK FLOW = 2.048 CMS RUNOFF VOLUME = 14.05 MM TIME TO PEAK= 1.17 HOURS

0 ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2
ADD HYD ID=1 HYD=163 IDI=6 IDII=3
0 PEAK FLOW = 26.834 CMS RUNOFF VOLUME = 21.60 MM TIME TO PEAK= 1.25 HOURS
ADD HYD ID=1 HYD NO=163 ID I=6 ID II=3

* SUBAREA 4B

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=191 CKK=1.0
XIMP=0.75 TIMP=0.75 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 L61=1128 MNI=0.013
SLP=1 L6P=1128 MNP=0.25

-1
UNIT PEAK = .113 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 12.40 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .018 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 91.38 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 24.005 CMS RUNOFF VOLUME = 38.54 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .80

ADD HYD ID=3 HYD=312 IDI=1 IDII=2
0 PEAK FLOW = 49.177 CMS RUNOFF VOLUME = 25.37 MM TIME TO PEAK= 1.17 HOURS
ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2

* INFLOW TO POINT -C-

0 PRINT HYD ID=3 1 HYDROGRAPH FROM AREA 312

0 RUNOFF VOLUME = 25.37 MM
0 PEAK DISCHARGE RATE = 49.177 CMS

* ROUTING FROM THE POINT C TO POINT D

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=750 SLP=0.008

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.2900
.26	1.	.1320
.39	2.	.1525
.53	3.	.1301
.66	5.	.1152
.79	7.	.1044
.92	10.	.0962
1.05	13.	.0954
1.18	18.	.0964
1.32	24.	.0933
1.45	31.	.0892
1.58	39.	.0850
1.71	48.	.0810
1.84	58.	.0775
1.97	68.	.0743
2.11	80.	.0714
2.24	93.	.0688
2.37	106.	.0664
2.50	121.	.0643

ROUTE ID=6 HYD=201
INDI=3 DT= 0.08330
PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 25.37 MM
PEAK DISCHARGE RATE = 46.767 CMS

*-----
* GET INFLOW TO POINT -D- (CMS * POND)
*-----
* SUBAREA 3B
*-----

COMPUTE NASHYD ID=1 HYD=103 DT=0.0833 H DA=95.17 HECT AA=0.0 AB=0.0
CN=68 IA=2.5 MM N=3 TP=1.50 W NI=36
-1
SHAPE CONSTANT, N = 3.00
UNIT PEAK = 2.42 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
PEAK DISCHARGE = 1.038 CMS RUNOFF VOLUME = 12.71 MM TIME TO PEAK = 2.916 HRS
TOTAL RAINFALL = 48.34 MM RUNOFF VOL. COEFFICIENT = .26

*-----
* SUBAREA 4C
*-----

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=77.71 CCK=1.0
XIMP=0.45 TIMP=0.45 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LGI=719 MNI=0.013
SLP=1 LSP=719 MNP=0.25
-1

UNIT PEAK = .139 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 9.47 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .024 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 69.74 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 6.824 CMS RUNOFF VOLUME = 27.31 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .57

ADD HYD ID=3 HYD=216 IDI=1 IDII=2
PEAK FLOW = 6.911 CMS RUNOFF VOLUME = .19.27 MM TIME TO PEAK= 1.17 HOURS
ADD HYD ID=3 HYD NO=216 ID I=1 ID II=2
ADD HYD ID=1 HYD=216 IDI=6 IDII=3
PEAK FLOW = 51.997 CMS RUNOFF VOLUME = 24.35 MM TIME TO PEAK= 1.25 HOURS
ADD HYD ID=1 HYD NO=216 ID I=6 ID II=3

*
PRINT HYD ID=1 1

HYDROGRAPH FROM AREA 216

RUNOFF VOLUME = 24.35 MM
PEAK DISCHARGE RATE = 51.997 CMS

ROUTE RESERVOIR ID=5 500 1
DISCHARGE STORAGE
0.0 0.0
3.0 4.2
6.2 7.7
9.0 23.1
13.0 29.56

PEAK DISCHARGE = 7.6418 CMS RUNOFF VOLUME= 24.2581 MM

*
PRINT HYD ID=5 1

HYDROGRAPH FROM AREA 500

RUNOFF VOLUME = 24.26 MM
PEAK DISCHARGE RATE = 7.642 CMS

*-----
* OUTFLOW FROM S W M POND (POINT -D-)
*-----

* ROUTING FROM THE POINT D TO POINT E
*-----

* ROUTING - X SECTION #2
*-----

COMPUTE RATING CURVEID=1 VSN=1 NSEG=1 NINEL=90.58
MAXEL=92.84
CHSLP=0.0041
FPSLP=0.0041

N=0.03 DIST=18
0.0 92.84 1.0 92.84
2.0 92.24 4.0 92.24
7.4 90.96 8.0 90.58
10 90.58 10.4 91.28
14 92.32 16 92.32
17 92.84 18 92.84

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
90.58	.0	.0
90.70	.3	.1
90.82	.5	.4
90.94	.9	.8
91.06	1.2	1.2
91.17	1.6	1.8
91.29	2.0	2.6
91.41	2.5	3.3
91.53	3.1	4.3
91.65	3.8	5.6
91.77	4.6	7.0
91.89	5.5	8.8
92.01	6.4	10.8
92.13	7.4	13.1
92.25	8.6	14.1
92.36	10.1	16.3
92.48	11.8	20.8
92.60	13.6	25.8
92.72	15.4	31.2
92.84	17.3	34.4

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=1350 SLP=0.0041

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.12	0.	.7780
.24	0.	.5181
.36	1.	.4140
.48	1.	.3606
.59	2.	.3245
.71	3.	.2987
.83	3.	.2856
.95	4.	.2716
1.07	6.	.2579

PRINT HYD ID=1 1

HYDROGRAPH FROM AREA 151

RUNOFF VOLUME = 24.59 MM
PEAK DISCHARGE RATE = 12.573 CMS

ROUTING FROM THE POINT F TO POINT G

ARTIFICIAL CHANNEL

COMPUTE RATING CURVEID=1 VSN=1 NSEG=1 NINEL=84.30
MAXEL=87.00
CHSLP=0.0004
FPSLP=0.0004

N=0.035 DIST=24.
0.0 87.00 4.0 85.3
6.5 85.3 8. 84.3
16.0 84.3 17.5 85.3
20.0 85.3 24.0 87.00

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
84.30	.0	.0
84.44	1.2	.2
84.58	2.4	.6
84.73	3.7	1.1
84.87	5.0	1.8
85.01	6.4	2.6
85.15	7.9	3.6
85.29	9.4	4.7
85.44	11.7	5.2
85.58	14.1	6.9
85.72	16.7	8.8
85.86	19.3	10.9
86.01	22.0	13.3
86.15	24.7	15.8
86.29	27.6	18.6
86.43	30.6	21.6
86.57	33.7	24.8
86.72	36.9	28.2
86.86	40.1	31.8
87.00	43.5	35.7

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=600 SLP=0.0004

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.14	0.	1.0967
.28	1.	.7062
.43	1.	.5499
.57	2.	.4625
.71	3.	.4055
.85	4.	.3649
.99	5.	.3342
1.14	5.	.3175
1.28	7.	.3428
1.42	9.	.3157
1.56	11.	.2939
1.71	13.	.2760
1.85	16.	.2609
1.99	19.	.2479
2.13	22.	.2367
2.27	25.	.2268
2.42	28.	.2181
2.56	32.	.2102
2.70	36.	.2032

ROUTE ID=6 HYD=201
INDI=2 DT= 0.08330

PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 108RATE = 185.20
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 109RATE = 182.82
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 110RATE = 180.09
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 111RATE = 177.09
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 112RATE = 173.89
 PROBLEM FAILED TO CONVERGE AFTER10 ITERATIONS. CONVERGENCE WAS FORCED.

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 114 RATE = 167.06
PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 115 RATE = 163.50
PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 116 RATE = 159.89
PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 117 RATE = 156.25
PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 118 RATE = 152.64
PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
OUTFLOW NUMBER = 119 RATE = 149.05

0 PRINT HYD ID=6 1 HYDROGRAPH FROM AREA 201

0 RUNOFF VOLUME = 24.55 MM
PEAK DISCHARGE RATE = 9.214 CMS

*-----
* GET INFLOW TO POINT -6-
*-----

* SUBAREA 50
*-----

COMPUTE URBHYD ID=1 HYD=102 DT=0.0833 DA=45.5 CCK=1.0
XIMP=0.30 TIMP=0.30 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LBI=550 MNI=0.013
SLP=1 LBP=550 MNP=0.25

-1
UNIT PEAK = .157 CMS
PEAK INTENSITY(RAIN EXCESS) = 72.96 MM/HR
STORAGE COEFF. SC = 8.06 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .027 CMS
PEAK INTENSITY(RAIN EXCESS) = 41.75 MM/HR
STORAGE COEFF. SC = 59.39 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 48.34 MM

PEAK DISCHARGE = 3.109 CMS RUNOFF VOLUME = 21.70 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .45

0 ADD HYD ID=2 HYD=261 ID1=1 ID11=6
PEAK FLOW = 11.794 CMS RUNOFF VOLUME = 24.44 MM TIME TO PEAK = 1.17 HOURS
0 ADD HYD ID=2 HYD NO=261 ID I=1 ID II=6

*-----
* TOTAL OUTLET FROM SIDE POINT -6-
*-----

0 PRINT HYD ID=2 1 HYDROGRAPH FROM AREA 261

0 RUNOFF VOLUME = 24.44 MM
PEAK DISCHARGE RATE = 11.794 CMS

*-----
FINISH

RUNOFF VOLUME = 25.71 MM
 PEAK DISCHARGE RATE = 1.122 CMS

 * SUBAREA 2A

COMPUTE URSHYD ID=2 HYD=102 DT=0.0833 DA=299.12 CKK=1.0
 XIMP=0.36 TIMP=0.36 NI=36 FO=76.12 FC=13.2 DCAY=4.14
 F/DO=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
 SLI=1 LGI=1235 MNI=0.013
 SLP=1 LGP=1235 MNP=0.25

-1
 UNIT PEAK = .122 CMS
 PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
 STORAGE COEFF. SC = 11.03 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .022 CMS
 PEAK INTENSITY(RAIN EXCESS) = 31.48 MM/HR
 STORAGE COEFF. SC = 73.85 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 38.319 CMS RUNOFF VOLUME = 45.90 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .64

ADD HYD ID=4 HYD=412 IDI=1 IDII=2
 PEAK FLOW = 38.626 CMS RUNOFF VOLUME = 38.96 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=4 HYD NO=412 ID I=1 ID II=2

 * INFLOW TO THE POINT -A-

PRINT HYD ID=4 1

HYDROGRAPH FROM AREA 412

RUNOFF VOLUME = 38.97 MM
 PEAK DISCHARGE RATE = 38.626 CMS

 * ROUTING FROM THE POINT A TO POINT B

COMPUTE RATING CURVEID=1 VSN=1 NSEG=3 NINEL=0.0
 MAXEL=2.5
 CHSLP=0.0035
 FPSLP=0.0035
 N=0.03 DIST=9.5 N=-0.02 DIST=16.5 N=0.03 DIST=26
 0 2.5 4.5 1.0
 9.5 1.0 11.5 2.0
 14.5 0.0 16.5 1.0
 21.5 1.0 26.0 2.5
 126 102.40 226 102.98

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
.00	.0	.0
.13	.4	.3
.26	.9	1.0
.39	1.5	2.0
.53	2.1	3.4
.66	2.8	5.1
.79	3.6	7.2
.92	4.5	9.7
1.05	5.9	12.9
1.18	8.2	17.8
1.32	10.7	23.8
1.45	13.2	30.8
1.58	15.8	39.9
1.71	18.6	47.8
1.84	21.4	57.7
1.97	24.4	68.4
2.11	27.5	80.1
2.24	30.6	92.8
2.37	33.9	106.3
2.50	37.2	120.7

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=750 SLP=0.0035

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.2900
.26	1.	.1920
.39	2.	.1525
.53	3.	.1301
.66	5.	.1152
.79	7.	.1044
.92	10.	.0962
1.05	13.	.0954
1.18	18.	.0964
1.32	24.	.0933
1.45	31.	.0892
1.58	39.	.0850
1.71	48.	.0810
1.84	58.	.0775
1.97	68.	.0743
2.11	80.	.0714
2.24	93.	.0688
2.37	106.	.0664
2.50	121.	.0643

ROUTE ID=6 HYD=201
INDI=4 DT= 0.08330
PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 38.97 MM
PEAK DISCHARGE RATE = 35.115 CMS

* SUBAREA 4A

COMPUTE URBYHD ID=2 HYD=102 DT=0.0033 DA=89.43 CKK=1.0
KIMP=0.75 TIMP=0.75 NI=36 FO=76.12 FC=13.2 DCAY=4.14
F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
SLI=1 LGI=810 MNI=0.013
SLP=1 LSP=810 MNP=0.25

-1

UNIT PEAK = .148 CMS
PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
STORAGE COEFF. SC = 8.72 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .028 CMS
PEAK INTENSITY(RAIN EXCESS) = 81.48 MM/HR
STORAGE COEFF. SC = 57.34 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 19.604 CMS RUNOFF VOLUME = 61.71 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .85

ADD HYD ID=3 HYD=342 IDI=6 IDII=2
PEAK FLOW = 54.719 CMS RUNOFF VOLUME = 42.69 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=3 HYD NO=342 ID I=6 ID II=2

* INFLOW TO THE POINT -B-

PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 342

RUNOFF VOLUME = 42.70 MM
PEAK DISCHARGE RATE = 54.719 CMS

* ROUTING FROM THE POINT B TO POINT C

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=1300 SLP=0.0043

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.5027
.26	1.	.3327
.39	2.	.2643
.53	3.	.2254
.66	5.	.1997
.79	7.	.1810
.92	10.	.1667
1.05	13.	.1654
1.18	18.	.1672

1.45	31.	.1546
1.53	39.	.1473
1.71	48.	.1405
1.84	58.	.1343
1.97	68.	.1287
2.11	80.	.1237
2.24	93.	.1192
2.37	106.	.1151
2.50	121.	.1114

ROUTE ID=6 HYD=201
 INDI=3 DT= 0.08330
 PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 42.70 MM
 PEAK DISCHARGE RATE = 48.297 CMS

*-----
 * GET INFLOW TO POINT -C-
 *-----

* SUBAREA 3A
 *-----

COMPUTE NASHYD ID=1 HYD=103 DT=0.0833 H DA=98.38 HECT AA=0.0 AB=0.0
 CN=68 IA=2.5 MM N=3 TP=1.17 H NI=36

-1

SHAPE CONSTANT, N = 3.00
 UNIT PEAK = 3.21 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
 PEAK DISCHARGE = 2.719 CMS RUNOFF VOLUME = 25.71 MM TIME TO PEAK = 2.416 HRS
 TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .36

* SUBAREA 2B
 *-----

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=23.23 CKK=1.0
 XIMP=0.36 TIMP=0.36 NI=36 F0=76.12 FC=13.2 DCAY=4.14
 F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
 SLI=1 LGI=395 MNI=0.013
 SLP=1 LGP=395 MNP=0.25

-1

UNIT PEAK = .199 CMS
 PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
 STORAGE COEFF. SC = 5.67 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .043 CMS
 PEAK INTENSITY(RAIN EXCESS) = 81.48 MM/HR
 STORAGE COEFF. SC = 37.26 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 3.721 CMS RUNOFF VOLUME = 45.92 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .64

ADD HYD ID=3 HYD=312 IDI=1 IDII=2
 PEAK FLOW = 4.124 CMS RUNOFF VOLUME = 29.57 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2
 ADD HYD ID=1 HYD=163 IDI=6 IDII=3
 PEAK FLOW = 51.591 CMS RUNOFF VOLUME = 40.30 MM TIME TO PEAK= 1.25 HOURS

ADD HYD ID=1 HYD NO=163 ID I=6 ID II=3

*-----
 * SUBAREA 4B
 *-----

COMPUTE URSHYD ID=2 HYD=102 DT=0.0833 DA=191 CKK=1.0
 XIMP=0.75 TIMP=0.75 NI=36 FO=76.12 FC=13.2 DCAY=4.14
 F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
 SLI=1 LGI=1128 MNI=0.013
 SLP=1 LGP=1128 MNP=0.25

-1

UNIT PEAK = .127 CMS
 PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
 STORAGE COEFF. SC = 10.63 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .023 CMS
 PEAK INTENSITY(RAIN EXCESS) = 81.48 MM/HR
 STORAGE COEFF. SC = 69.94 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 11.99

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 40.276 CMS RUNOFF VOLUME = 61.70 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .85

ADD HYD ID=3 HYD=312 IDI=1 IDII=2
 PEAK FLOW = 89.047 CMS RUNOFF VOLUME = 45.07 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=3 HYD NO=312 ID I=1 ID II=2

*-----
 * INFLOW TO POINT -C-
 *-----

PRINT HYD ID=3 1

HYDROGRAPH FROM AREA 312

RUNOFF VOLUME = 45.07 MM
 PEAK DISCHARGE RATE = 89.047 CMS

*-----
 * ROUTING FROM THE POINT C TO POINT D
 *-----

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
 L=750 SLP=0.008

TRAVEL TIME TABLE
 REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.13	0.	.2900
.26	1.	.1920
.39	2.	.1525
--	-	----

.79	7.	.1044
.90	10.	.0962
1.05	13.	.0954
1.18	18.	.0964
1.32	24.	.0933
1.45	31.	.0892
1.58	39.	.0850
1.71	48.	.0810
1.84	58.	.0775
1.97	68.	.0743
2.11	80.	.0714
2.24	93.	.0688
2.37	106.	.0664
2.50	121.	.0643

ROUTE ID=6 HYD=201
 INDI=3 DT= 0.08330
 PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 45.07 MM
 PEAK DISCHARGE RATE = 85.277 CMS

 * GET INFLOW TO POINT -D- (S W M POND)

* SUBAREA 3B

COMPUTE NASHYD ID=1 HYD=103 DT=0.0833 H DA=95.17 HECT AA=0.0 AB=0.0
 CN=68 IA=2.5 MM N=3 TP=1.50 H NI=36
 -1
 SHAPE CONSTANT. N = 3.00
 UNIT PEAK = 2.42 CMS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00
 PEAK DISCHARGE = 2.157 CMS RUNOFF VOLUME = 25.71 MM TIME TO PEAK = 2.832 HRS
 TOTAL RAINFALL = 72.27 MM RUNOFF VOL. COEFFICIENT = .36

 * SUBAREA 4C

COMPUTE URBHYD ID=2 HYD=102 DT=0.0833 DA=77.71 CCK=1.0
 XIMP=0.45 TIMP=0.45 NI=36 FO=76.12 FC=13.2 DCAY=4.14
 F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
 SLI=1 LGI=719 MNI=0.013
 SLP=1 LGP=719 MNP=0.25
 -1

UNIT PEAK = .156 CMS
 PEAK INTENSITY(RAIN EXCESS) = 107.19 MM/HR
 STORAGE COEFF. SC = 8.12 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .030 CMS
 PEAK INTENSITY(RAIN EXCESS) = 81.48 MM/HR
 STORAGE COEFF. SC = 53.38 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 12.551 CMS RUNOFF VOLUME = 49.56 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .60

ADD HYD ID=3 HYD=216 IDI=1 IDII=2
PEAK FLOW = 12.760 CMS RUNOFF VOLUME = 36.43 MM TIME TO PEAK= 1.17 HOURS

ADD HYD ID=3 HYD NO=216 ID I=1 ID II=2
ADD HYD ID=1 HYD=216 IDI=6 IDII=3
PEAK FLOW = 95.043 CMS RUNOFF VOLUME = 43.62 MM TIME TO PEAK= 1.25 HOURS

ADD HYD ID=1 HYD NO=216 ID I=6 ID II=3

*-----
* INFLOW TO S W M POND
*-----

PRINT HYD ID=1 1

HYDROGRAPH FROM AREA 216

RUNOFF VOLUME = 43.62 MM
PEAK DISCHARGE RATE = 95.043 CMS

ROUTE RESERVOIR	ID=5 500 1	DISCHARGE	STORAGE
		0.0	0.00
		3.0	4.20
		6.2	7.70
		9.0	23.10
		13.0	29.56

RAGE-DISCHARGE TABLE EXCEEDED.

PEAK DISCHARGE = 13.0348 CMS RUNOFF VOLUME= 43.3402 MM

PRINT HYD ID=5 1

HYDROGRAPH FROM AREA 500

RUNOFF VOLUME = 43.34 MM
PEAK DISCHARGE RATE = 13.035 CMS

*-----
* OUTFLOW FROM S W M POND (POINT -D-)
*-----
* ROUTING FROM THE POINT D TO POINT E
*-----
* ROUTING - X SECTION #2
*-----

COMPUTE RATING CURVEID=1 VSN=1 NSEG=1 NINEL=90.58
MAXEL=92.84
CHSLP=0.0041
FPSLP=0.0041

N=0.03	DIST=18		
0.0	92.84	1.0	92.84
2.0	92.24	4.0	92.24
7.4	90.96	8.0	90.58
10	90.58	10.4	91.28
14	92.32	16	92.32
17	90.00	18	90.00

RATING CURVE VALLEY SECTION 1.0

WATER SURFACE ELEV	FLOW AREA SQ METRES	FLOW RATE CMS
90.58	.0	.0
90.70	.3	.1
90.82	.5	.4
90.94	.9	.8
91.06	1.2	1.2
91.17	1.6	1.8
91.29	2.0	2.6
91.41	2.5	3.3
91.53	3.1	4.3
91.65	3.8	5.6
91.77	4.6	7.0
91.89	5.5	8.8
92.01	6.4	10.8
92.13	7.4	13.1
92.25	8.6	14.1
92.36	10.1	16.3
92.48	11.8	20.8
92.60	13.6	25.8
92.72	15.4	31.2
92.84	17.3	34.4

COMPUTE TRAVEL TIME ID=6 REACH=1 NVS=1
L=1350 SLP=0.0041

TRAVEL TIME TABLE
REACH 1.0

WATER DEPTH METRES	FLOW RATE CMS	TRAVEL TIME HRS
.12	0.	.7780
.24	0.	.5181
.36	1.	.4140
.48	1.	.3606
.59	2.	.3245
.71	3.	.2987
.83	3.	.2856
.95	4.	.2716
1.07	6.	.2579
1.19	7.	.2450
1.31	9.	.2331
1.43	11.	.2223
1.55	13.	.2123
1.67	14.	.2278
1.78	16.	.2313
1.90	21.	.2126
2.02	26.	.1977
2.14	31.	.1853
2.26	34.	.1883

ROUTE ID=6 HYD=201
INDI=5 DT= 0.08330
PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 43.29 MM
PEAK DISCHARGE RATE = 12.993 CMS

PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 166 RATE = 168.68
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 167 RATE = 165.17
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 168 RATE = 161.56
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 169 RATE = 157.90
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 170 RATE = 154.23
 PROBLEM FAILED TO CONVERGE AFTER 10 ITERATIONS. CONVERGENCE WAS FORCED.
 OUTFLOW NUMBER = 171 RATE = 150.58

PRINT HYD ID=6 1

HYDROGRAPH FROM AREA 201

RUNOFF VOLUME = 43.92 MM
 PEAK DISCHARGE RATE = 18.140 CMS

*-----
 * GET INFLOW TO POINT -G-
 *-----
 *-----
 * SUBAREA 5C
 *-----

COMPUTE URBHYD ID=1 HYD=102 DT=0.0833 DA=45.5 CKK=1.0
 XIMP=0.30 TIMP=0.30 NI=36 FO=76.12 FC=13.2 DCAY=4.14
 F/DD=0.0 DPSI=1.57 DPSP=4.67 STI=0.0 STP=0.0
 SLI=1 LGI=550 MNI=0.013
 SLP=1 LGP=550 MNP=0.05

-1
 UNIT PEAK = .175 CMS
 PEAK INTENSITY (RAIN EXCESS) = 107.19 MM/HR
 STORAGE COEFF. SC = 6.91 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

UNIT PEAK = .035 CMS
 PEAK INTENSITY (RAIN EXCESS) = 81.48 MM/HR
 STORAGE COEFF. SC = 45.45 MINS

SUM OF THE UNIT HYDROGRAPH CO-ORDINATES = 12.00

TOTAL RAINFALL = 72.27 MM

PEAK DISCHARGE = 6.339 CMS RUNOFF VOLUME = 43.49 MM TIME TO PEAK = 1.166 HRS

RUNOFF VOLUMETRIC COEFFICIENT = .60

ADD HYD ID=2 HYD=261 IDI=1 IDII=6
 PEAK FLOW = 24.005 CMS RUNOFF VOLUME = 43.90 MM TIME TO PEAK = 1.17 HOURS

ADD HYD ID=2 HYD NO=261 ID I=1 ID II=6

*-----
 * TOTAL OUTLET FROM SIDE POINT -G-
 *-----

PRINT HYD ID=2 1

HYDROGRAPH FROM AREA 261

RUNOFF VOLUME = 43.90 MM
 PEAK DISCHARGE RATE = 24.005 CMS

